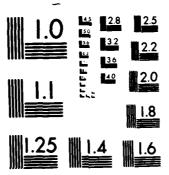
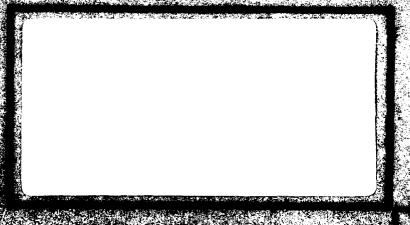
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EXPERIMENTAL TESTING OF FLYING QUALITIES THEORIES

Thesis

Nathan H. Krys AFIT/GE/EE/82D-43 Captain USAF

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EXPERIMENTAL TESTING OF FLYING QUALITIES THEORIES

THESIS

Presented to the Faculty of the School of Engineering
of the Air Force Institute of Technology
Air University

In Partial Fulfillment of the Requirements for the Degree of

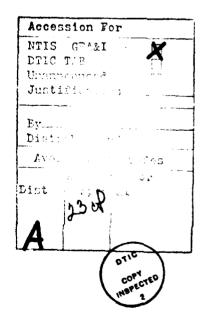
Master of Science

by

Nathan Krys Capt USAF

Graduate Electrical Engineering

December 1982



Approved for public release; distribution unlimited

Preface

During my second quarter at the Air Force Institute of Technology, I was fortunate to hear Mr. Ron Anderson lecture on the problems with man-machine interface and how they affected flying qualities. When this thesis topic was proposed, I saw an opportunity to gain practical knowledge in an area encountered briefly before but never expanded on and thus chose this topic.

My thanks to Mr. R.O. Anderson who, as my thesis advisor and sponsor, gave me his valuable guidance and advice. My thanks to Mr. Tom Cord for his unending assistance and encouragement. I also thank Mr. Joe Marous and Mr. Mike Dammarell for their time and expertise in setting up the experimental simulator. In addition, thanks to Suzanne Weber for typing this thesis.

Finally, a special thank you for my wife and children. My wife, Leslie, who had the patience of Job and supported me during the trying times. My children, Caryn and Michael, both have shown an unusual amount of maturity and understanding during these difficult 18 months.

Nathan H. Krys

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LIST OF SYMBOLS

e^{-τS} time delay (sec) stick force in roll axis (1b) Fas stick gain ((deg/sec²)/lb) K .roll rate (deg/sec) La Place operator s stick deflection (in) time delay (sec) bank angle (deg) bank angle command (deg) bank angle error (deg), $\Phi_e = \Phi_c - \Phi$ roll rate (deg/sec) pitch angle (deg) short period natural frequency (rad/sec) ^wsp short period damping, ratio ξsp

List of Abbreviations

deg degrees

Eq equation

fwd forward

in inches

lb pounds

PR pilot rating

pot potentiometer

rad radians

Ref reference

RMS root-mean-square

sec seconds

TOT time on target

vs versus

Abstract

An analog computer simulation was used to model the roll dynamics of the generic aircraft which had been evaluated on the variable stability NT-33A arroraft. Sum of sine waves and random step functions were used as the two different command signals. The purpose of this study was to determine what effect the nature of the command signal had on the pilot rating of the task simulation.

The experiments consisted of fourteen different tests for each command signal. Five pilots, with varied flying experience, were instructed to follow the command signal in a pursuit flying task. The system time delay was varied from 0.1 to 0.8 seconds. The highest frequency component of the input signal was 2.54 radians/second. The subjects used a control stick while looking at an oscilloscope displaying the command signal and the subjects's response. RMS error, time on target, and the Cooper-Harper rating scale were used as performance measures.

The experiments showed that the subjects considered the sum of sine waves task closer to an actual flying task. In addition, as the time delay was decreased, the subjects preferred K/s-like dynamics.

EXPERIMENTAL TESTING OF FLYING QUALITIES THEORIES

I. Introduction

Background

The increasingly complex control systems of modern fighter aircraft have resulted in closed-loop system dynamics substantially different from traditional flight dynamics. Because of these differences, it is nearly impossible to accurately predict pilot-aircraft performance and pilot rating for many of the aircraft/control systems now being tested or designed. The small data base on handling qualities of modern aircraft (or high-order systems) compounds the difficulty. Traditional aircraft flight dynamic characteristics for favorable pilot ratings on different levels of flying quality are contained in the old Military Specification, MIL-F-8785B. However, because the modern system dynamics which increase the aircraft capabilities and add to its complexity, the criteria in that Military Specification are not adequate to evaluate or predict the the flying qualities of modern aircraft/control systems (Ref 2). This situation provided the motivation for the simulations reported in this thesis, as well as the revision to the Specification, MIL-F-8785C (Ref 1).

Current aircraft modeling concepts can shed some

light on predicting the flight qualities of new aircraft by man-in-the-loop simulations. One can place a pilot in a system simulation programmed with the proper aircraft equations of motion and control systems dynamics where the pilot-aircraft performance can be observed.

Two, of many, previous studies were done for the Air Force Wright Aeronautical Laboratories/Flight Dynamics Laboratory (AFWAL/FDL) by the Calspan Advanced Technology Center using the USAF/Calspan variable stability NT-33A aircraft. The NT-33A is a test bed used to study the effects of different control system dynamics (Refs 2; 3).

Up until the recent NT-33A studies (Refs 3; 5), the prevailing theory was that K/s-like dynamics are the ideal transfer function. Earlier studies with the NT-33A suggested similar conclusions. However, very little data were available to reach a definite conclusion. The origin of using ideal dynamics represented by the simple transfer function K/s was obtained during ground-based compensatory tracking tasks using a sum of sine waves signal for the input. A compensatory tracking task is one where the subject sees only the system error and tries to correct this error. The recent NT-33A experiments, however, used a pursuit task in an airborne flight with step inputs. A pursuit task shows both command signal and aircraft position, the difference between the two is the error. The purpose of this thesis is to use a ground-based experiment to evaluate the differences in experimental conditions.

The Air Force Wright Aeronautical Laboratories, (AFWAL) Wright-Patterson AFB, is interested in this research for possible application to future specifications.

Problem

AFWAL desires the simulation of the dynamics used in the NT-33A duplicated in the laboratory and a comparison of these ground results with the actual flight data. The specific tasks required are:

- 1. Determine the effect that the type of tracking command (random vs. step) has on the pilot rating during a roll tracking task with various roll time constants.
- Determine the effect of stick sensitivity (gain) on pilot rating for these same cases.
- 3. Develop a data base of simplified low order equivalent system results that can be used to predict the handling qualities for high order models in the pitch axis.

Scope

The experiment is concerned only with studying the flying qualities of the dynamics used in the NT-33A aircraft as simulated on the Electronic Associates Incorporated (EAI) 2000 Analog Computer. The roll task has two different inputs. The first test examines the roll task with a sum of sine waves input. The other test uses a random square wave

input. The pitch task uses only the sum of sine waves as an input.

Three performance measures are used. The Cooper-Harper Pilot Opinion Rating Scale (Fig 1) is be the subjective performance measure, while RMS error and time on target are the objective performance measures. A performance measurement is an evaluation of how well a system operates (i.e., how well the output follows the input or how small the error can be maintained over a given period of time).

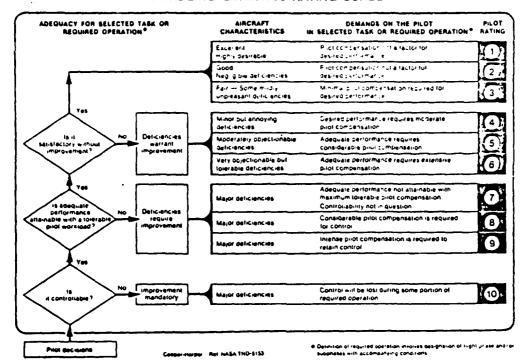
Assumptions

- 1. The Aeronautical Systems Division (ASD) EAI 2000 Analog computer will be a good representation of the dynamics simulated with the NT-33A.
- 2. The volunteer pilots will be a good representation of USAF "line" pilots.

Approach

The pitch (Ref 7) and roll (Refs 3; 5) equations were provided by AFWAL. Chapter II discusses the experimental approach and how the equations were implemented on the EAI 2000 Analog computer. Chapter III presents the results, problems encountered during the simulation, and observations. Chapter IV presents conclusions and further recommendations resulting from this study. The appendices contain additional pertinent information and tabulated results.

HANDLING QUALITIES RATING SCALE



DEFINITIONS FROM TN-D-5153

COMPENSATION

The measure of additional pilot effort and attention required to maintain a given level of performance in the face of deficient vehicle characteristics.

HANDLING QUALITIES

Those qualities or characteristics of an aircraft that govern the ease and precision with which a pilot is able to perform the tasks required in support of an aircraft role.

MISSION

The composite of pilot-vehicle functions that must be performed to fulfill operational requirements. May be specified for a role, complete flight, flight phase, or flight subphase.

PERFORMANCE

The precision of control with respect to aircraft movement that a pilot is able to achieve in performing a task. (Pilot-vehicle performance is a measure of handling performance. Pilot performance is a measure of the manner or efficiency with which a pilot moves the principal controls in performing a task.)

ROLE

The function or purpose that defines the primary use of an aircraft

TASK

The actual work assigned a pilot to be performed in completion of or as representative of a designated flight segment.

WORKLOAD

The integrated physical and mental effort required to perform a specified piloting task.

Fig 1. Cooper-Harper Pilot Rating Scale (Ref 3)

II. Experimental Approach

General

This thesis documents the experimental study of the dynamics of the roll and pitch axes of conventional aircraft (Fig 2). The roll task will have two alternate inputs, a sum of sine waves and a random step function. The pitch task will deal only with the sum of sine waves input. All experiments took place in Building 676, the Aeronautical Systems Division (ASD) computer center. The roll and pitch equations were simulated on the EAI 2000 analog computer. A control stick obtained from bench stock was used (Fig 3). The stick was free to move in both the pitch and roll axes. More detailed information on the stick is found in Appendix A. stick was used by the pilot to follow the command signal in a pursuit environment. Only one axis of the stick was used per task. The command and stick signals were displayed on a dual trace Tektronics oscilloscope, type 454 (Fig 4). flying W represents the pilot's simulated aircraft. pilots were instructed to maintain minimum error between the command signal and the flying W (Fig 5).

Experimental Setup

The simulation was performed on the EAI 2000 analog computer. Figure 6 shows a simplified block diagram of the system. The analog circuitry of the system (see Appendix B)

was installed on the EAI 2000 in the normal fashion with output displayed on the oscilloscope. The pilot was instructed to minimize error by moving the control stick in the proper direction. All runs were timed for 90 seconds. The RMS error and time on target were monitored and kept on MODCOMP Classic IV hook-up.

Simulator

Figure 7 shows the simulator setup for this experiment. It consists of a flat chair (no wheels), the stick, and a dual trace oscilloscope. The stick polarity was set similar to an aircraft stick. Force applied away from the subject caused the W to move down and vice versa. Since the simulation was flown one axis at a time, it would not be possible to perform roll and pitch motion at the same time. For each task the pilot was given several practice runs until he felt comfortable with the task and apparatus. Distance between pilot and scope varied with the pilot concerned. On the average, the distance was two feet from the head of the pilot to the oscilloscope. All the pilots used the stick as a center stick.

Aircraft Equations

The roll equation used is the same used by Monagan (Ref 3). The pitch equation came from NASA contractor report CR-2144 (Ref 7). The equations are shown below.

Roll equation:

$$\frac{\Phi}{F_{AS}} = \frac{K}{s(s+1/\tau_R)} \tag{1}$$

Pitch equation:

$$\frac{\theta}{F_{AS}} = \frac{K}{s} \left[\frac{s + \frac{1}{\tau}}{\frac{s^2}{\omega_{sp}^2} + 2 \frac{\xi_{sp}}{\omega_{sp}}} \right] e^{-\tau s}$$
 (2)

Pade's approximation for $e^{-\tau S}$ was used in the pitch simulation. All analog circuit drawings appear in Appendix B.

Pade's approximation:

$$e^{-\tau S} = \frac{2 - \tau S}{2 + \tau S} \tag{3}$$

Command Signals

The sum of sine waves command signal is similar to the one used in AFFDL-TR-65-15. This experiment uses six different sine waves because of equipment limitations. The frequency components for the sine wave are shown in Table 1. Each sine wave had a peak voltage of one volt to ensure the command signal would not go off the face of the scope (6 volts). This signal was used for roll and pitch.

The random step function used the sum of sine wave signal as both a trigger to start the random appearing step and set the value for the step voltage. A more detailed explanation of both circuits appears in Appendix B.

TABLE 1
Sum of Sine Waves
(Ref 4)

ω _n
0.262/rad/sec
0.393
0.969 1.49 2.54

Presentation of Task

During a tracking task the pilot is aware of two parameters, his position and the target's position. A difference between the two positions is an error. The pilot task is to minimize the error. In this simulation, the command signal is a horizontal line on the scope. The command signal in the pitch axis moves up or down and will not go off the face of the scope. For the roll task, the command signal rotated 34 degrees left or right on the scope because of equipment limitations. A typical presentation of both tasks is shown in Fig 4. To correct the pitch error displayed, the pilot must pull back or push forward on the stick, causing the W to rise or fall and follow the command signal. To correct the roll error, the pilot must push the stick toward the left or right, which will make the W rotate in the direction of the command signal.

During the first roll tests, pilots were confused as to which signal was which when the W and command signals were superimposed. To eliminate this confusion, the signals were separated by two divisions on the scope face. This confusion did not occur in the pitch task.

A normal run began with the command and W lines horizontal on the scope face, with no initial conditions. The pilots were instructed to keep the error at zero for 90 percent of the time for as long as possible. When the pilot was ready, the computer operator started the command signal. Then the pilot began tracking his target. The data variables monitored were command signal, stick output (6), error, pitch or roll rate, RMS error and time on target. RMS error and time on target were read on a digital printout, while the other signals were on a strip chart. Each run was 90 seconds long. Figure 7 shows a typical strip chart recording for the experiment.

The Gathering of Data

Once the position of the stick and scope were adjusted for the comfort of the pilot, a training period began. A training period consisted of as many runs as the pilot wished, usually three to five runs. This allowed for further adjustment of the stick, scope and chair, as well as familiarity with the task involved. The testing began when the pilot was ready.

The roll task consisted of fourteen runs. These runs were made up of four sets of three runs and one set of two runs. During each set of runs, τ_R would remain the same and stick gain would vary. For the last run of each set, the

subject was asked if the task could be improved. If so, which run was preferred. Should the stick act more like task A, task B, or someplace in between? The subject would then fly a 45-second test run. This allowed him to judge if the stick characteristics were improved. This testing procedure continued until optimum performance of the system was reached. Then the subject would fly the new system for a recorded 90 seconds.

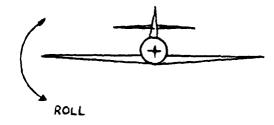
At no time did the subject know what parameter had changed. He only knew the stick would handle differently, and his preference was used to improve the system. After completing each run, the subject was asked for comments and a Cooper-Harper rating for the task. He was reminded not to rate himself, but the task.

To present the tasks in a random fashion, all subjects were started on a different set of tasks. For instance, SF began the roll task with sum of sine waves test one and ended with test fourteen. DS started with sum of sine waves test four and ended with test three. This allowed for a randomized test. Table 2 lists the parameters tested (Ref 3). However, these parameters were not actually tested due to an error. The details are discussed in Chapter III.

The pitch task was cancelled due to problems with the simulation. The details are also discussed in Chapter III.

TABLE 2
Parameters and Values
(Ref 3)

Variable	Tested Parameter
[₹] R	.1, .15, .25, .45, .8 sec
P _{SS} F _{AS}	10, 25 Set by Pilot (deg/sec)/lb



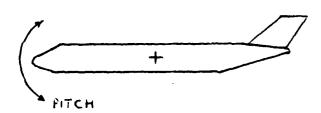
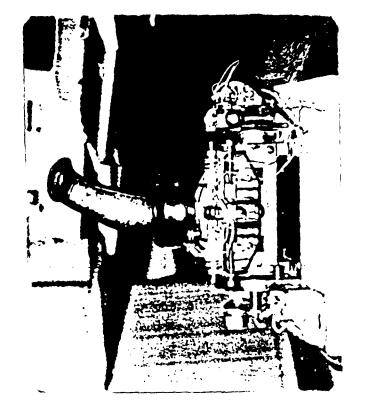


Fig 2. Pitch and Roll Axes



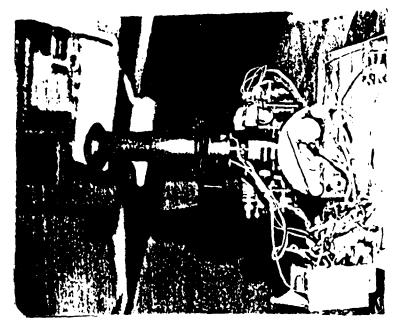


Fig 3. Front and Side of Stick

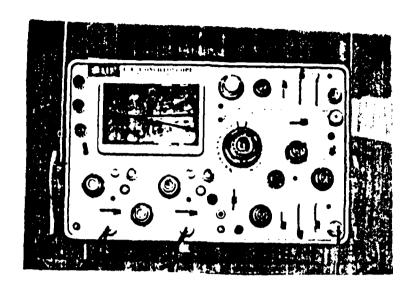


Fig 4. Oscilloscope Display

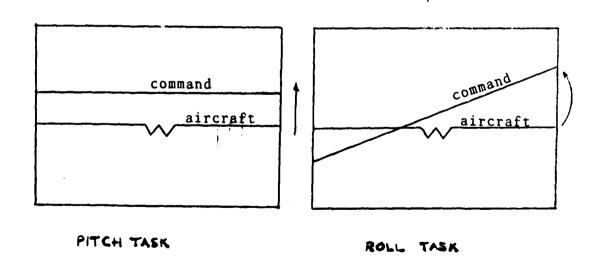


Fig 5. Task Displays 14

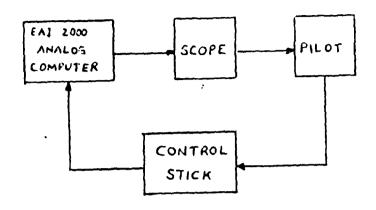


Fig 6. System Block Diagram

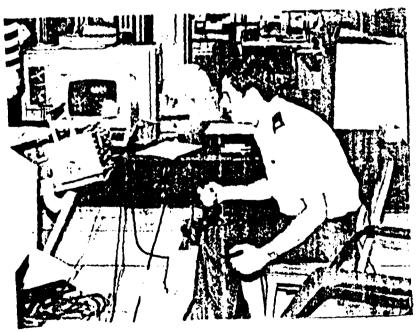
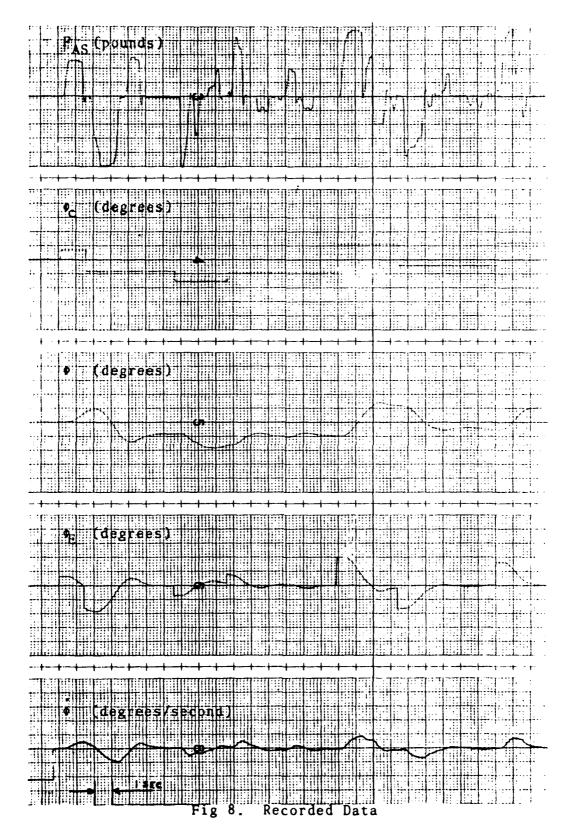


Fig 7. Simulator



4_

III. Experimental Results

This chapter contains the data from all the experimental runs with the five subjects. The problems, observations and results are also presented and discussed.

Pitch Task

The pitch task was never accomplished due to a stick "bobble" which appeared in the scope display during the initial tests. A bobble is a continued movement of the subject response (W) when no force is applied. The subjects noticed that the W on the scope would make a slight downward movement after the desired response was complete. This problem was later traced to the simulated pitch equation. The connections to the control stick were interchanged to allow the pitch axis to be connected to the roll equation and vice versa. After the connections were made, the pitch display had no bobble but the roll did. This procedure eliminated the control stick as the problem, leaving the simulation equation as the source of the bobble.

As a result, the roll tests were continued while nitempting to solve the problem with the pitch equation. This problem was very disturbing since the equation is an actual description for the T-33 pitch dynamics. The problem was never rectified, and we still do not know why the bobble is present. To continue the research, other equations recom-

mended by AFWAL were simulated. The second equation is shown below:

$$\frac{\theta}{\delta} = \frac{K(s + \frac{1}{\tau})}{s(\frac{s^2}{\omega^2} + 2\frac{\xi}{\omega}s + 1)}$$
 (4)

Although this equation is very similar to the original equation, this simulation was not stable. Recently another much simpler equation was simulated on the EAI 2000, and no bobble or instability problems occurred. The simpler equation is shown below:

$$\frac{\phi}{\delta} = \frac{Ke^{-\tau S}}{s(s + \frac{1}{\tau_R})} \tag{5}$$

Due to the coordination needed for ASD employees to be present during test runs, conflicts with subject pilots' schedules and the small amount of time left for further research, this last equation was not pursued any further. It was decided to document what had happened and recommend that the last equation be used for further research. The schematic diagram for Eq (5) is found in Appendix F.

If the pitch equation had no problems, the data would have been used to start a data base for low-order equivalent system results to aid in predicting the handling qualities of high-order systems.

Roll Task

Table 2 (Chapter II) shows the original values for the proposed test parameters. These parameters were not tested due to a factor not accounted for in the roll simulation. Therefore the values shown in Table 3 were tested. To switch from one test to another in the simulation, one potentiometer was used to set the value for K. Typing in the value for time delay on the CRT set the value for τ_R . After the results were examined in detail, it was discovered the K potentiometer included a τ_R factor which was not accounted for. This unaccounted factor changed all the values for K and $P_{\text{SS}}/F_{\text{AS}}$ values. Table 3 shows the actual parameters tested.

TABLE 3
Actual Tested Values

r sec	K deg/sec²	P _{SS} /F _{AS} deg/sec
0.1	1b 1000.00	166.66
0.15 0.15	1111.11	66.66 66.66
0.25	400.00 160.00	100.00 40.00
0.45 0.45	49.38 123.42	22.22 55.54
0.8	15.63 39.10	12.50 31.28
Note: Koptimum	was set by the subje	ct (see Tables 4 and 5)

A summary of the results in tabulated form is found in Tables 4 and 5. The tables show the 14 different tasks, pilot ratings, time on target (TOT), RMS error, and the

TABLE 4

Random Step Summary

) v:	Subjects	} }	} }			
PR	SF	RMS PR TOT	PR	TOT	RMS	7 A	RMS PR TOT	RMS PR TOT	RL	RMS PR	MK TOT	RMS
Test 6	1 t=. 70.57		=49 6	73.98	13.4	7	78.56	13.4 3	74.5	45 K=49.38 18.5 6 73.98 13.4 7 78.56 13.4 3 74.51 19.4 4 83.4 12.5	83.4	12.5
Test 8	2 t=. 75.21		=123.	45 K=123.42 16.8 4 80.86 14.1 3	14.1	m	79.70	79.70 14.9 2	80.1	80.18 14.2 4.5 79.50 14.3	79.50	14.3
Test 7	t 3 r=.45 Kopt =88.88 77.43 19.4	.45 38.88 19.4	2.5	45 8.88 K _{opt} =155.55 19.4 2.5 77.68 16.8	55.55 16.8		K=123.42 NO IMPRO	K=123.42 NO IMPROVEMENT		K _{opt} =444.44 80.12 14.2 4	K _{opt} =4444 78.77 14.9	1444
Test 7	4 t=. 77.43	.25 K	= 4 00	.25 K=400 16.7 4 73.40 16.6 2	16.6	7	83.1	83.1 15.0 3	76.8	76.87 16.1 3	82.0 11.9	11.9
Test 2.5	5 τ= 80.15	.25 K [±] 15.2	=160 2	.25 K=160 15.2 2 73.42 18.4 3	18.4	۳۸	78.9	78.9 14.9 2	76.4	76.43 17.5 3	82.77 12.1	12.1
Test	t 6 r=.25 Kopt=140 79.50 15.0	.25 !40 15.6	1.5	25 40 K _{opt} =240 15.6 1.5 73.96 14.7 2	40 14.7		K _{opt} =3 82.23	K _{opt} =360 82.23 13.6 2		K _{opt} =208 81.07 15.9 3	K _{opt} =500 80.7 11.8	500 11.8
Test 7	7 t=. 70.56	.8 K= 18.5	15.63 5.5	5 66.16	16.8	7.5	66.20	8 K=15.63 18.5 5.5 66.16 16.8 7.5 66.20 22.9 4		69.23 18.1 4	72.1 17.4	17.4
NOTE	Kopt	equal	to 1	equal to pilot optimum gain	ptimu	m ga	in					

TABLE 4, continued

						รั	Subjects							
PR	SF TOT	MM RMS PR TOT	PR		RMS	PR	DS PR TOT	RMS PR TOT	PR		RMS PR		MK TOT	RMS
Test 8.5	8 T=.8 70.52	.8 K=39.1 19.0 S	39.1 5	63.02 21.6 7 77.43 17.3 4	21.6	7	77.43	17.3	4	74.22 16.8	16.8		74.4 18.2	18.2
Test 5	t 9 t=.8 Kopt=62.5 76.72 16.0	8 2.5 16.0 4	4	K _{opt} =100 K _{opt} =125 75.97 14.5 5.5 81.15 15.4 4	0 14.5	5.5	Kopt=1.8	25 15.4		K _{opt} =100 77.00 15.0	.00 15.0		K=15.63 NO IMPROVEMENT	3 EMENT
Test 2.5	10 r=.1 80.06 1	.15 ⁻ 1	K=111	15 K=1111.1 14.2 7 76.42 14.0 5.5 77.56 18.0 3	14.0	5.5	77.56	18.0	8	81.52 14.3 3	14.3	3	80.05 14.6	14.6
Test 5	11 t= 82.6	.15]	K=444 2.5	15 K=444.44 13.2 2.5 70.38	17.1 2	2	82.76 14.0 3	14.0	100	83.32 15.4 3	15.4	3	83.0 13.8	13.8
Test	12 t=.1 K _{opt} =833 82.52 1	.15 33.33 12.7 1	1	K _{opt} =533.33 77.71 16.8 1	3.33	7	K _{opt} =533.33 82.77 14.3 3	33.33 14.3	м	K _{opt} 500 83.56 12.8 3)0 12.8		K _{opt} =1333.33 80.72 14.4	33.33
Test 2	13 t= 84.45	.10]	K=100 5	10 K=1000 12.8 5 74.22 15.6 2	15.6	2	82.20 14.9 3	14.9	23	83.74 13.1 3	13.1	8	83.20 11.7	11.7
Test 3	14 t=.1 Kopt=750 84.24 1	.10 50 11.8 1		K _{opt} =850 K _{opt} =600 78.60 13.9 1.5 82.85 13.1 2	0 13.9	1.5	Kopt=6 82.85	00 13.1	2	K _{opt} =7 83.40	750	2.5	K _{opt} =750 K _{op} =750 83.40 13.1 2.5 85.31 11.7	0
NOTE:	Kopt	ļΘ	l to	qual to pilot optimum gain	ptimu	B &	ain							

TABLE 5 Sum of Sine Waves Summary

						Sı	Subjects						
PR	SF	RMS	RMS PR TOT	TOT	DS RMS PR TOT	PR	DS TOT	RMS PR TOT	PR		RMS PR	TOT	RMS
Test 5	1 t= 41.97	18.	K=49 3 6	15 K=49.38 18.3 6 68.42 12.4 4	12.4	1	73.16 10.9 6	10.9	9	60.13	60.13 13.5 6	52.82 15.0	15.0
Test 3	2 t≡. 49.58	.45 l	K=123.	5 K=123.42 15.3 4 80.07 10.7 3	10.7	м	82.17 10.5 5	10.5	2	72.88	72.88 11.5 4.5 60.94 13.7	60.94	13.7
Test	3 t= Kopt= 54.82	`. =		Kopt=277.77 Kopt=333.33 87.37 10.1 2.5 84.84 10.9 4	10.1	2.5	Kopt=3 84.84	33.33 10.9		K _{opt} =2 66.81	K _{opt} =277.77 66.81 11.6 5	K _{opt} 388.88 67.88 11.4	8.88
Test 1.5	4 t=.	.25	25 K=400 11.5 4	87.31 9.9 2	9.9 2		84.67 9.6 4	9.6 4		69.73	69.73 11.7 3	73.90 11.1	11.1
Test 7	5 t=.	25 1	K=160 3 5.5	:5 K=160 20.3 5.5 86.92 10.3 2.5 79.92 10.2 4	10.3	2.5	79.92	10.2	4	70.65	70.65 11.2 4.	72.42 12.3	12.3
Test	6 TE. Kopt 56.59	.25 320 15.7	7 1.5	K _{opt} =600 15.7 1.5 88.79 10.0 2)0 10.0	2	K _{opt} =320 83.76 9.8 3	20 9.8 3		K _{opt} =6 77.00	K _{opt} =600 77.00 10.9 3	K _{opt} =800 84.71 11.2	00 11.2
Test 8	7 t=. 29.40	.8 K= 27.]	=15.63 1 8	K=15.63 27.1 8 75.25 11.7 7.5 50.16 17.2 7	11.7	7.5	50.16	17.2	7	53.94	53.94 16.1 7.5 39.25 19.8	39.25	19.8
NOTE	Kopt	1	al to	equal to pilot optimum gain	optimu	1m 86	ain						

TABLE 5, continued

						S	ubjects						
PR	SF TOT	MM RMS PR TOT	PR	TOT	RMS	ď	PR TOT	RMS PR TOT	PR	RL TOT	RMS PR	MK TOT	RMS
Test 7	8 TE.	8 K=39.	39.T 5.5	K=39.1 23.4 5.5 83.82 10.6 7	10.6	7	50.34 15.0 7	15.0	7	55.72	55.72 14.5 7	43.93 18.3	18.3
Test	9 t= Kopt= 50.32	.8 237.5 16.9 3		K _{opt} =143.75 87.44 10.0 4	10.0	4	K _{opt} =225 74.92 10.7 6	25 10.7	9	Kopt=] 58.32	K _{opt} =156.25 K _{opt} =225 58.32 13.8 4.5 54.41 13.9	Kopt = 54.41	13.9
Test 1	10 T= 66.56	.15 1 15.4	K=111 4	15 K*1111.1 15.4 4 79.43 12.0 4	12.0	4	85.41 9.6 5	9.6		72.57	72.57 11.8 3	67.50 9.6	9.6
Test 4	11 T= 62.38	15 1	K=444 2.5	15 K=444.44 13.9 2.5 85.65	10.4 3	3	83.80 9.8 6	9.86		70.30	70.30 12.0 3	70.83 11.3	11.3
Test 1	12 T= Kopt=6 72.65	T=.15 =666.66 15 13.0 2	2	K _{opt} =833.33 85.97 10.2 2	33.33 10.2		K _{opt} =833.33 87.36 9.5 3	33.33 9.5 3		Kopt=883.10	K _{opt} =833.33 83.10 10.3 2	K _{opt} =900 73.23 11.2	300
Test 3	13 t= 70.01	•	K=100)0 91.10	9.8 1	.5	10 K=1000 14.5 4 91.10 9.8 1.5 88.95 9.4 4	9.4 4		77.17	77.17 10.9 2.5 86.95 10.3	86.95	10.3
Test	14 t=.1 Kopt=750 74.41 1	.10 50 11.0 1		K _{opt} =1; 91.32	250 9.6 N	1 0	K _{opt} =1250 K=1000 91.32 9.6 NO IMPROVEMENT 2	ENT 2		K _{opt} =1500 82.10 10.5	K _{opt} =1500 K _{opt} =2000 82.10 10.5 2.5 87.51 10.0	Kopt 87.51	=2000 10.0
NOTE:	Kopt	1	to T	equal to pilot optimum gain	optimo	8 =	ain						

optimum gain (K) values for the two different inputs. Please note, P_{SS}/F_{AS} values above 75 are not attainable with real aircraft. Since the error was not discovered until after the data were taken, all the data and parameters are displayed to establish trends within the data.

All the pilots agreed that the sum of sine waves task appeared to act more like an airplane flying task when compared to the step function input. Several pilots commented that the step function input task was superficial and did not "act like an airplane." Furthermore, the random step task was easy, and they knew more than enough time was available to minimize the error between signals. More information regarding pilot experience is found in Appendix D. Pilot comment data is found in Appendix E.

Time on Target

Figures 9 through 16 show the pilot rating versus time on target data for the two different inputs. The random step data do not show any apparent consistent trends. It is suspected the subjects were not sensitive to this measure except where the time delay was high ($\tau = 0.8$). The sum of sine waves data, on the other hand, show definite trends. All the tests (except $\tau = 0.1$) show that all the pilots gave low ratings for high time on target results. The subjects were better able to evaluate the dynamics for the sum of sine waves task and were certainly more consistent with each other. The high ratings (poor performance) reflected direct-

ly the degree of pilot compensation and workload needed to minimize the error for each task. In comparison, the sum of sine waves data shows more sensitivity and the subjects were better able to judge their task, since high time on target tasks received low ratings. Probably the degree of pilot compensation and workload account for the higher ratings for the square wave task. In addition, there was more consistency in pilot ratings between the sum of sine waves task as compared to the step function.

RMS Error

RMS error for the two different inputs. Again, the data show inconsistencies for the random step data and definite trends for the sum of sine waves data. The subjects appear to be more sensitive to RMS error data due to the data lines not being as steep as the time on target data.

The high pilot ratings for high RMS error and vice versa seem reasonable. The data for the random step show the subjects were more sensitive to this measure, but they were not consistent (except where τ = 0.8). In comparison, the sum of sine waves data show a definite agreement among the ratings and lower ratings were given for lower RMS error. Again, the high ratings are a measure of how much pilot compensation is necessary to manage the workload.

Time Delay (t)

Figure 22 is a composite for all the time delays

versus pilot ratings for those values of K that were chosen by the subjects. At the top of the graphs are the average optimized stick gains. As can be readily seen, there is very little difference between the two different inputs. However, it is interesting to note that the subjects preferred higher gains for lower time delays and higher gains were preferred for the sum of sine waves task when compared to the step function. This figure clearly shows K/s-like dynamics were preferred for both inputs.

Stick Gain (K)

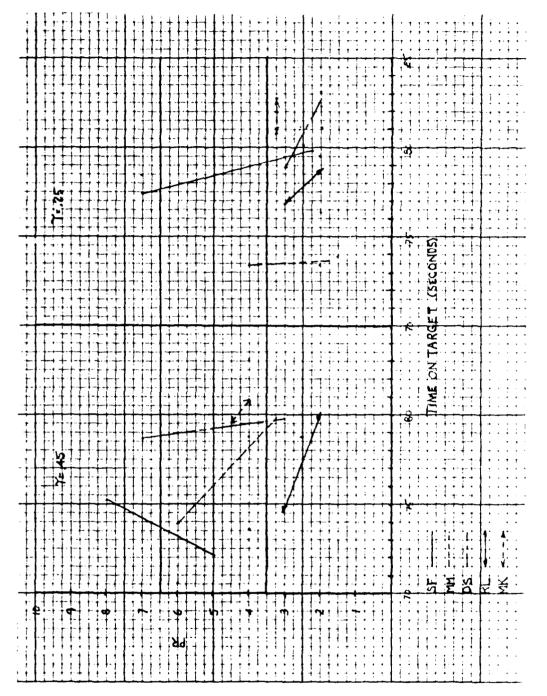
Figures 23 through 29 show stick gain versus pilot The higher the gain, the more sensitive the stick reacts to stick input. For the step input, the inconsistencies continue and no trends are shown. For the sum of sine waves, however, a definite trend is shown. First, the subjects were most sensitive to stick gain. In addition, the subjects were very consistent. The subjects generally gave the higher gains lower pilot ratings. When τ was equal to 0.15 (very responsive aircraft), an optimum gain was obtained between 600 and 900. This illustrates that after a certain point high pilot ratings were given, the gain reached a point where the simulation was just too responsive. This is why no straight trends lines appear in Fig 28. (Since this was a trend in itself, this author connected the points with straight lines to emphasize the agreements between all of the subjects for stick gain where $\tau = 0.15$.)

To correlate the runs, mean RMS error and time on target were graphed in Figs 30 and 31. It was expected that simulation resulting in a low RMS error and high time on target would reflect "good" flying qualities and "low" pilot ratings. For the random step this was not the case (Fig 30). In fact, this result agrees with Monagan (Ref 3). There was no apparent correspondence between time on target, RMS error and pilot rating. For the sum of sine waves, on the other hand, Fig 31 shows a definite correlation between the three different levels of flight characteristics. This figure definitely shows "poor" flying qualities tend to be associated with higher RMS errors and with low time on target. Arcs are shown between what might be considered the three different levels of flying qualities. This agrees with Onstott (Ref 12). Onstott concluded that a pilot will tolerate more sluggish response in a given flying level if the resulting time on target is good.

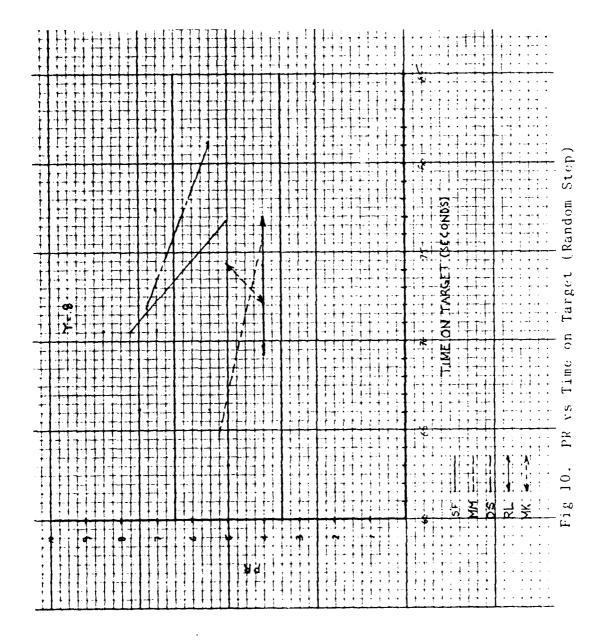
Figures 32 and 33 compare stick gain versus time delay with the flying quality level shown. All that can be deduced from these figures is that the subjects preferred low time delays with high gains. However, the data points to the extreme right should not be considered valid since these gains cannot be attained with real conventional aircraft. These points are displayed only to show trends. Note, as a decreased, the subjects preferred higher stick gains and the rating improved, indicating a preference for "K/s-like" systems. This data is in direct conflict with Chalk and

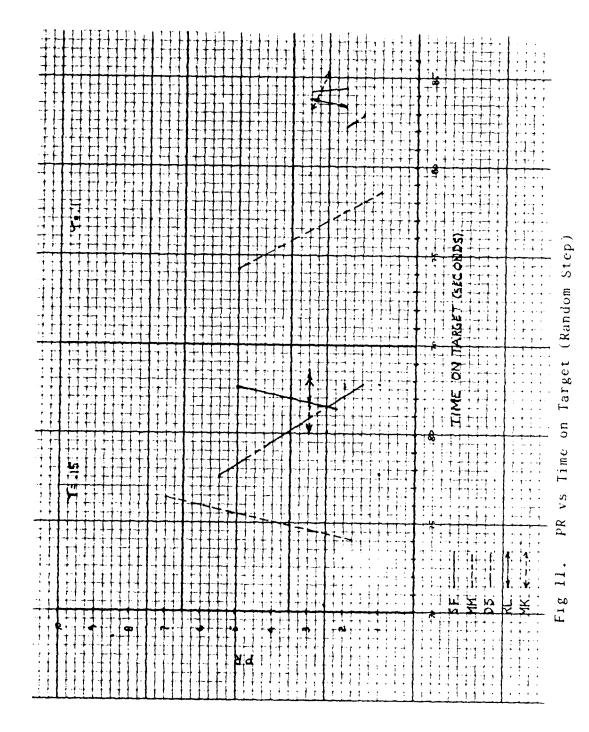
Monagan. However, the difference could be due to motion effects present in the NT-33 experiment and not here. Add this conflict to the extremely consistent data with the sum of sine waves command signal tests and a question arises. Namely, are random step function command signals useful in defining flight characteristics alone or should a variety of different command signals be used? The data seem to speak for themselves.

In summary, the experimental results show the subjects preferred K/s-like aircraft characteristics. Figure 21 clearly illustrates that as τ decreased, pilot ratings improved for the two different inputs. In addition, the above results certainly lead one—to question why the step signals were used. It might also be recommended that step functions not be used as the only inputs to define flying characteristics.



Hig 9. PR vs Time on Target (Random Step)





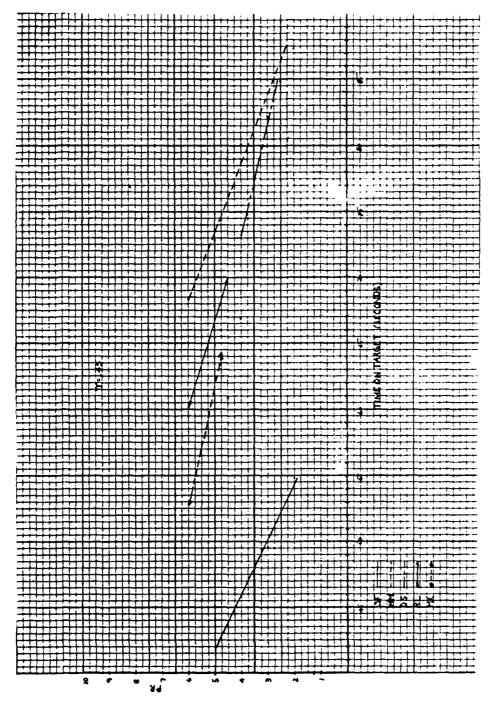


Fig 12. PR vs Time on Target (Sum of Sine Waves)

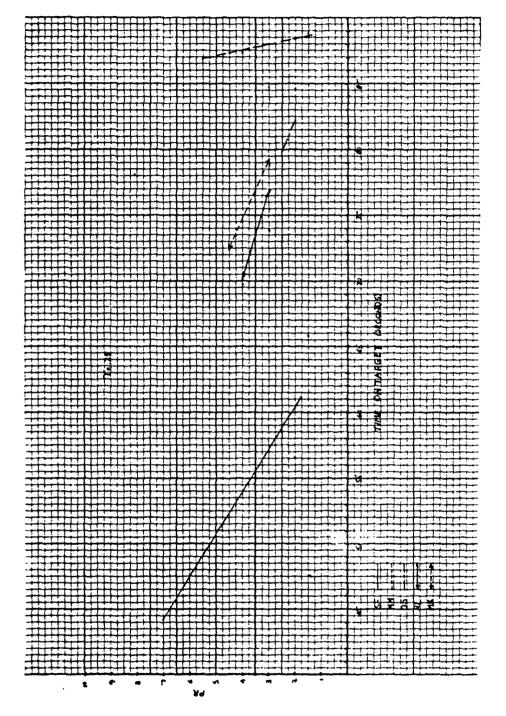
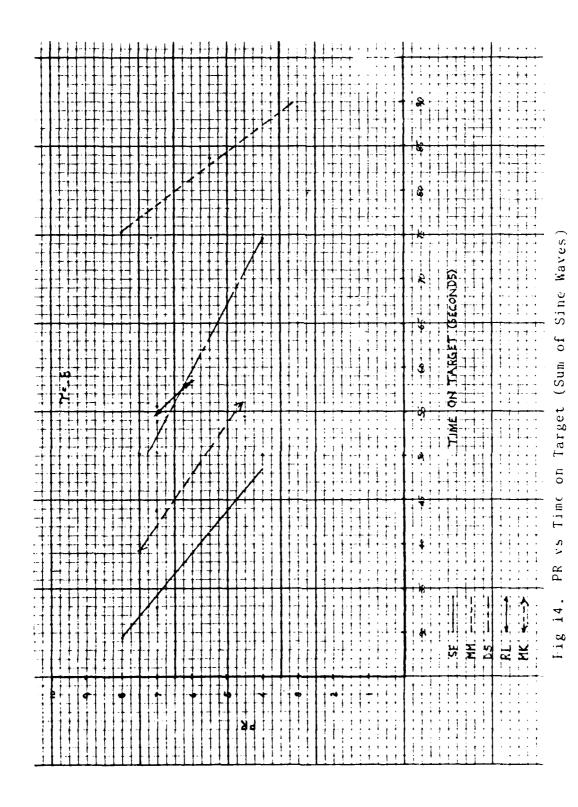


Fig 13. PR vs Time on Target (Sum of Sine Waves)



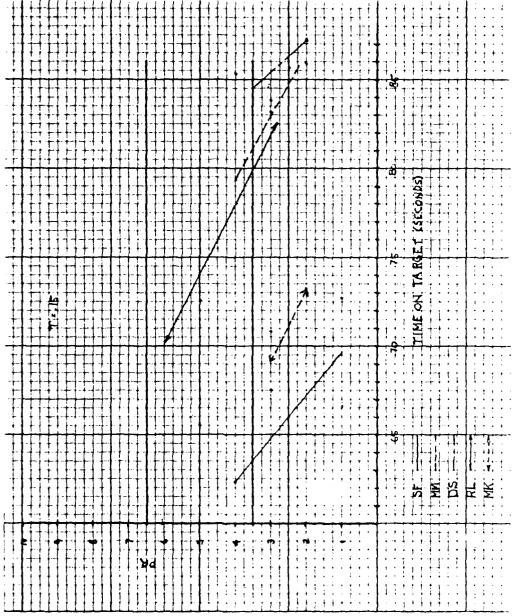
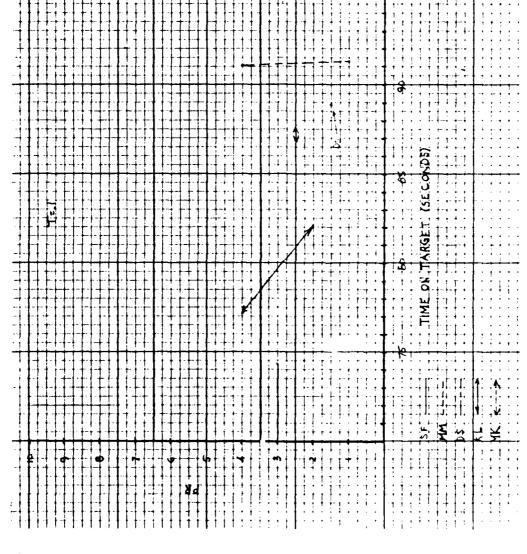
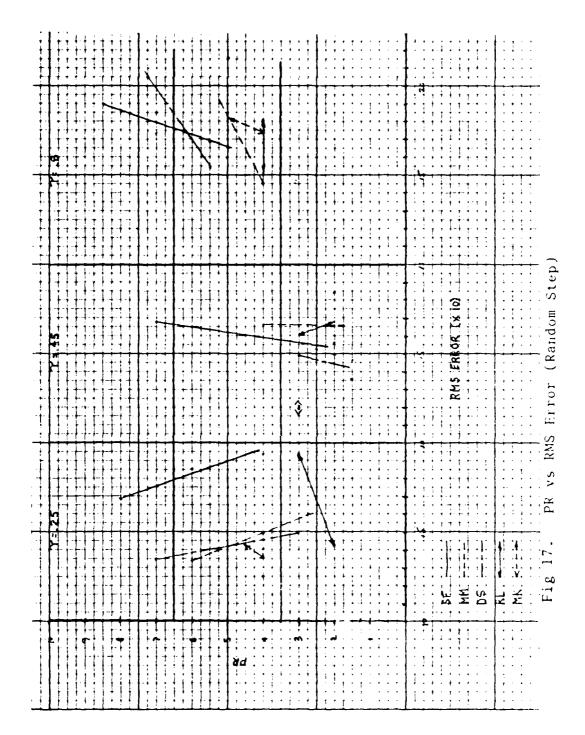
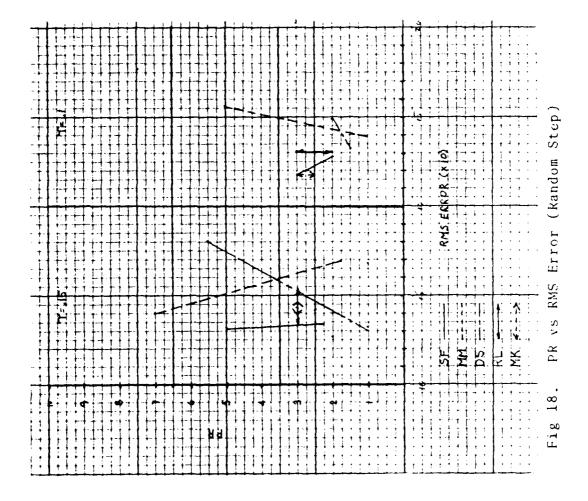


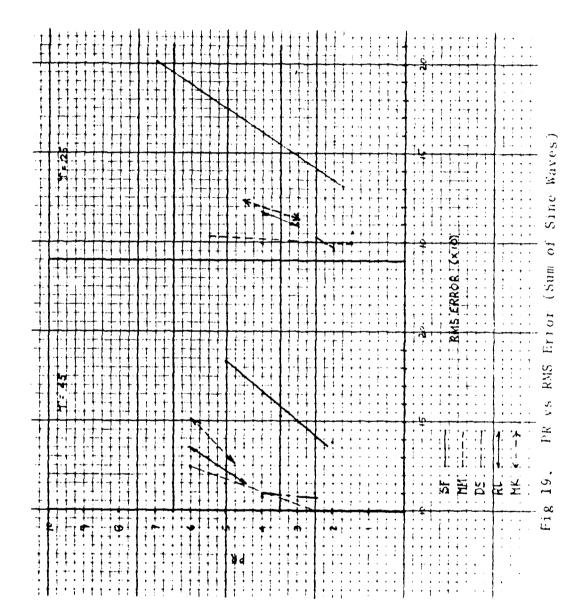
Fig 15. PR vs Time on Target (Sum of Sine Waves)

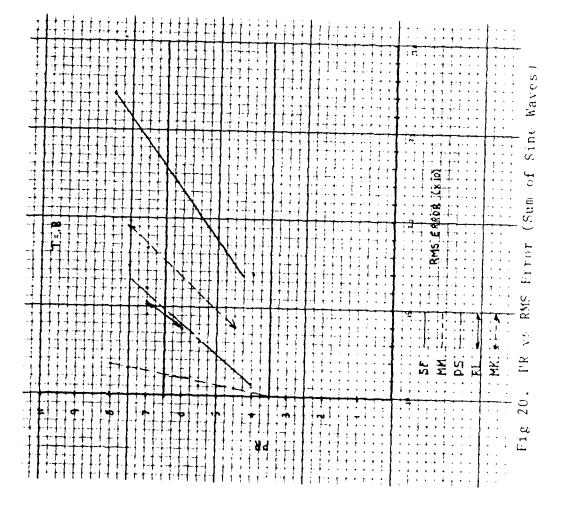


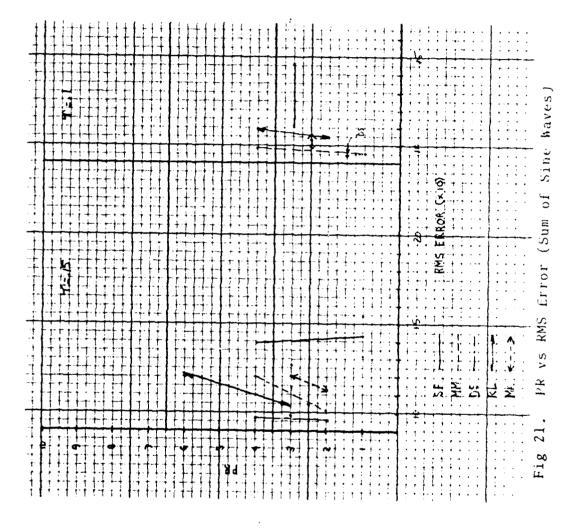
ig 16. PR vs Time on Target (Sum of Sine Waves)

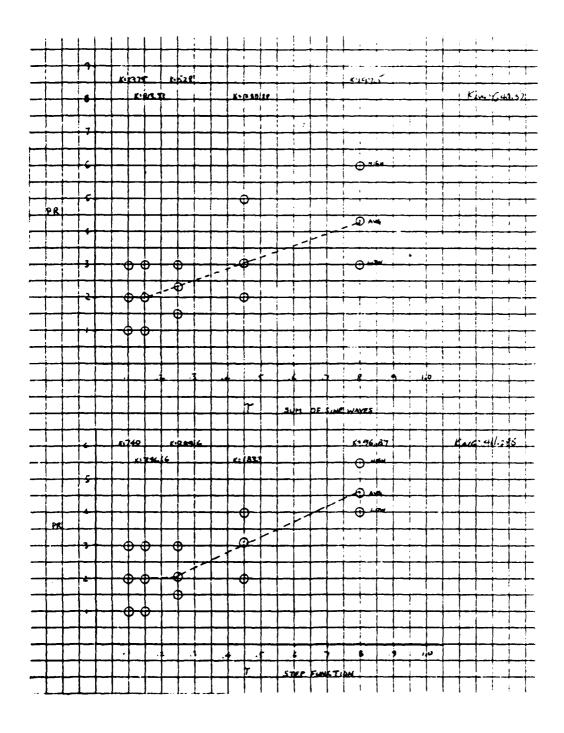






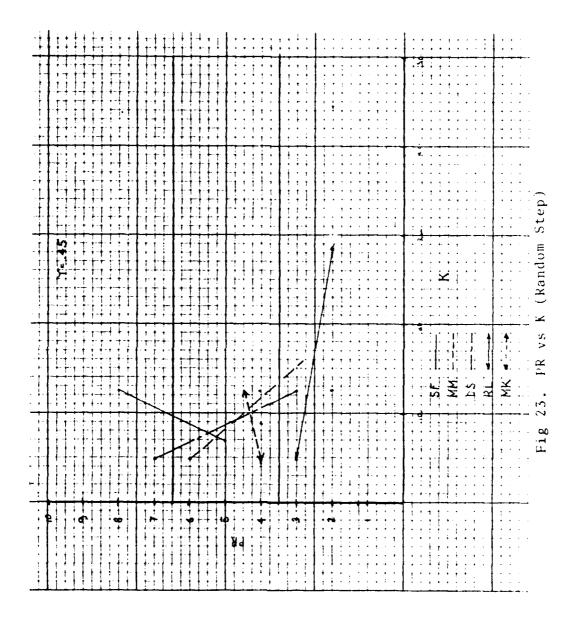


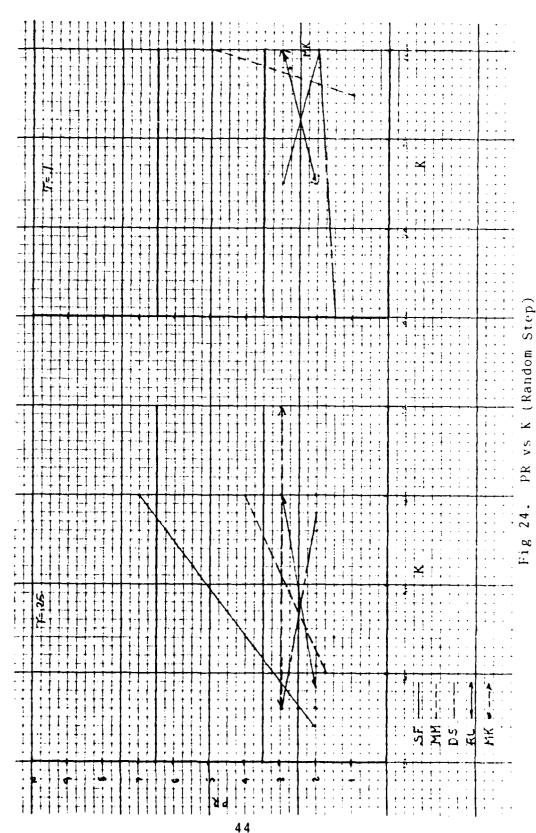




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Fig 22. Pilot Rating vs Time Delay





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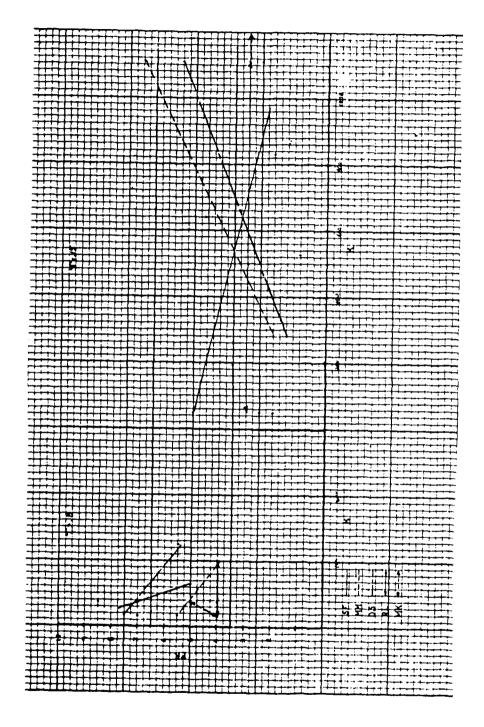


Fig 25. PR vs K (Random Step)

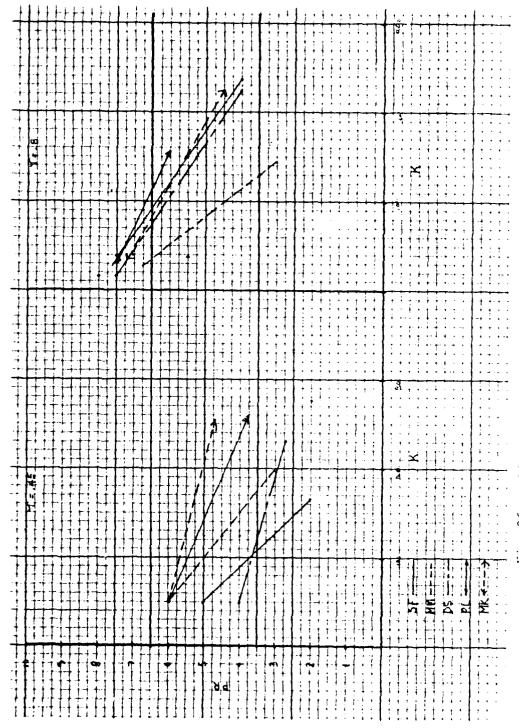


Fig 26. PR vs K (Sum of Sine Waves)

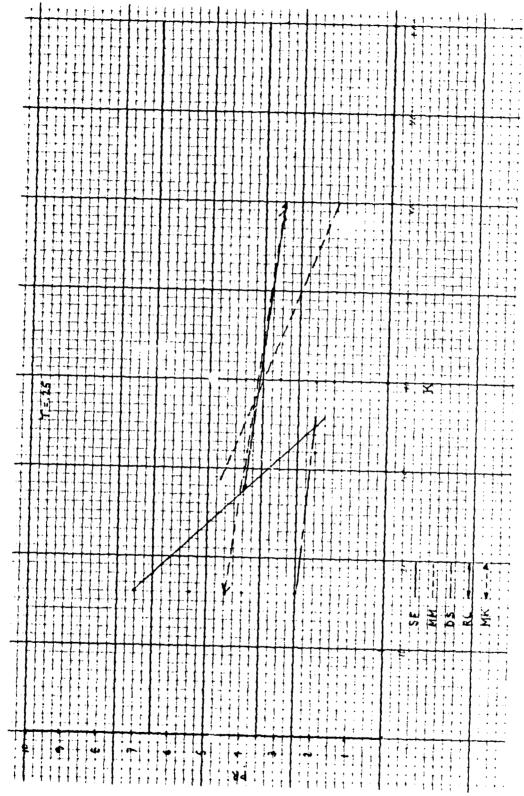


Fig 27. PR vs K (Sum of Sine Waves)

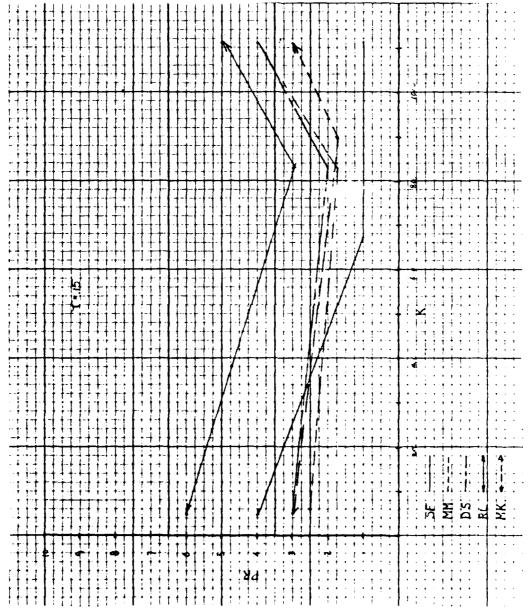


Fig 28. PR vs K (Sum of Sine Waves)

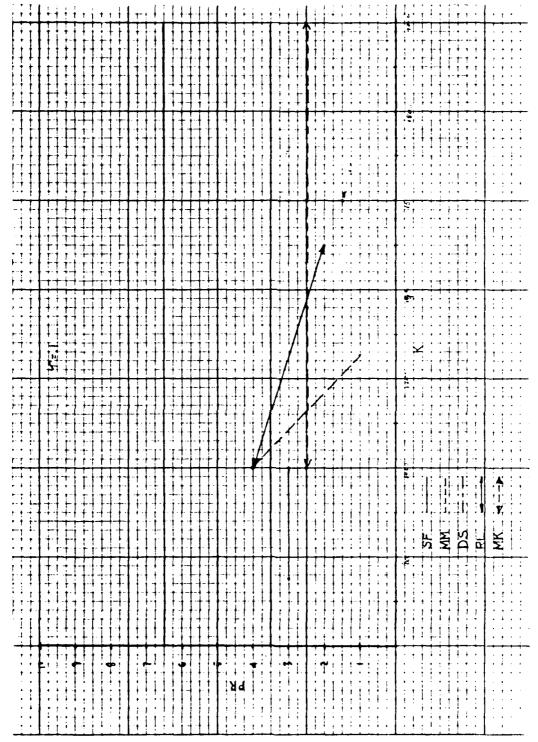


Fig 29. PR vs K (Sum of Sine Waves)

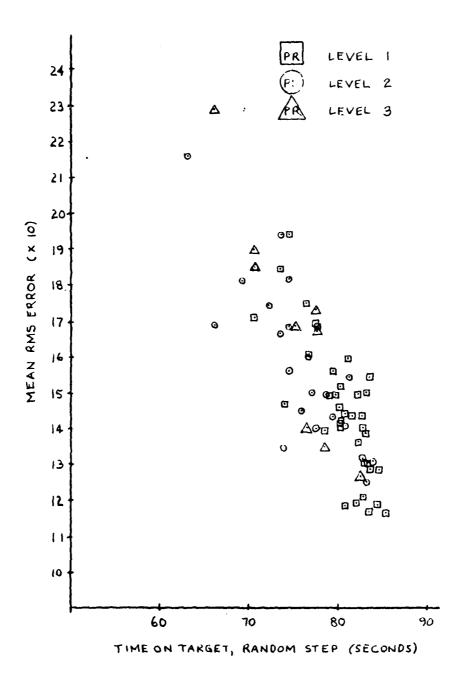
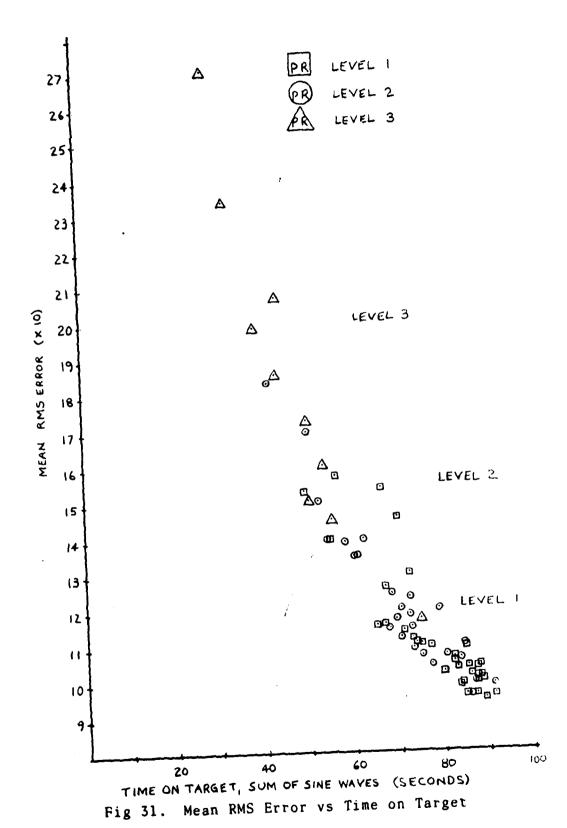


Fig 30. Mean RMS Error vs Time on Target



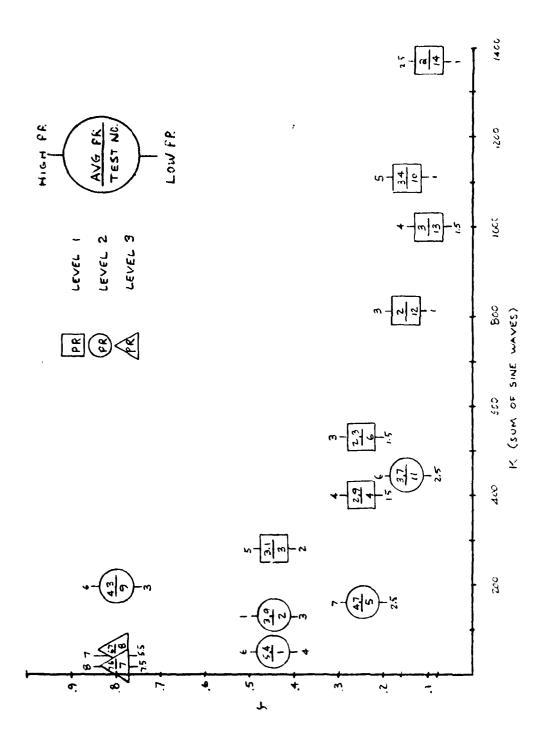


Fig 32. t vs K (Sum of Sine Waves)

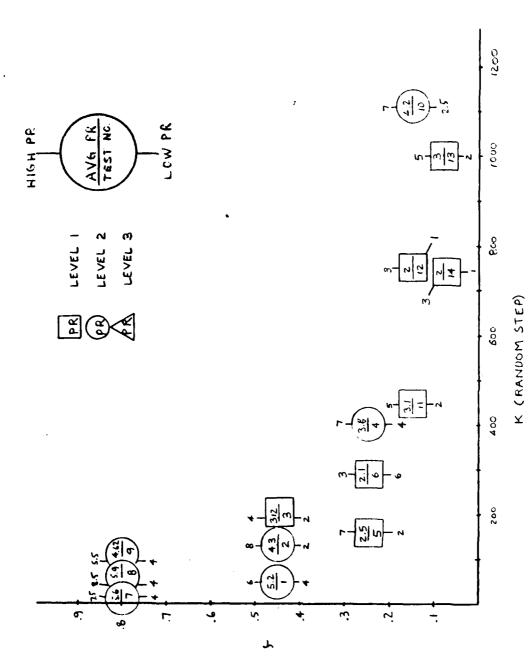


Fig 33, τ vs K (Random Step)

IV. Summary, Conclusions and Recommendations

The purposes of this thesis were to determine what effect the type of command input has on the pilot rating during a roll tracking task with various time constants, determine the effect of stick sensitivity on pilot rating for those same cases, and collect data on the pitch axis to compare with high order systems. Early in the study a problem (still not resolved) arose with the pitch simulation.Data collection continued with the roll axis simulation. After all the roll data were taken, an algebraic error was discovered in the roll simulation. An extra factor was not accounted for. This factor changed all of the stick gain results. However, the data were recalculated to account for the newly discovered factor; the revised data showed that some of the configurations tested are not attainable in today's normal aircraft. Instead of discarding the data, the results were used to show trends and form conclusions based on all the data. These trends are considered valid.

In short, all of the random step data were inconsistent. When all three performance measures were used, there were no correlations that could be definitely made between the data. For the sum of sine waves data, there are many signs of trends between performance measures and the data were consistent, even between different pilots. The

subjects continually gave low pilot ratings for high time on targets, low RMS errors, and high stick gains. In addition, subjects optimized their stick gains when time delay decreased. Finally, all the subjects preferred "K/s-like" dynamics as the time delay was decreased. This conclusion is in direct conflict with both Monagan and Chalk.

It should be remembered that Monagan and Chalk's studies were on an actual aircraft with motion. The current studies were performed on a fixed-base simulator. The obvious difference between the two are the effects of motion and actual flight. These factors cannot be accounted for in the simulator. Clearly further study with more pilots and a motion simulator is needed before assuming any definite conclusions. In addition, it is recommended that any future flight tests include sum of sine waves command signals, and the experimenters compare these test results with the other test data.

This thesis did bring out the fact that a sum of sine waves command signal (highest frequency 2.54 radians/sec) is preferred by subjects and does lead to K/s-like dynamics for time delay between 0.1 and 0.8 seconds as most desirable, at least when no motion is present. Thus, prevailing theories are still appropriate and one might question the conclusions of both Chalk and Monagan because of the inconsistencies associated with the step data. Furthermore, it is recommended that future inflight testing with the NT-33 include sum of sine waves command signals.

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APPENDIX A

CALIBRATION OF THE CONTRUL STICK

AND ROLL SIMULATION

As mentioned previously, a control stick obtained from bench stock was used in these experiments. However, there was no documentation on the control stick. This particular stick was used only because the pilots had no experience with a force stick, the only other stick available. The pilots wanted another feedback cue other than just the visible display on the scope, and a force stick could not accommodate the pilots since it did not move. The control vtick used was free to move plus or minus 25 degrees in the roll axis and plus or minus 20 degrees in the pitch axis. By judging the movement on the stick with the W on the scope, a pilot can gage his force necessary to follow the command signal. In addition, all pilots have had experience with a moveable control stick and none with a force stick, otherwise additional training would have been required.

Stick Calibration

The items used to calibrate the stick were assorted weights, string, tape, protractor grid, bearing and a needlepoint. The stick was secured to a table to insure no movement of the base. The string was attached to the center of the grip and placed over a bearing which was rigidly

attached to the table. The end of the cord had a loop to allow for the weights (Fig A-1). As weights were placed on the end of the string, the handle would deflect. A protractor grid was rigidly placed around the axis of movement and a needlepoint was attached to the same axis. As the handle deflected, a reading in degrees was made. This procedure was used for both axes. Tables A-1 and A-2 show the tabulated data, and Figs A-2 and A-3 show the graphed data.

TABLE A-1
Roll Axis

L	Left		ht	
Pounds	Degrees	Pounds	Degrees	
0.88	0.5	0.88	0.5	_
0.99	0.5	0.99	1.0	
1.10	0.5	1.10	1.5	ł
1.14	0.5	1.14	7.0	- 1
1.21	1.0	1.21	13.5	
1.32	2.0	1.32	25.0	
1.54	6.0			
1.64	20.0			- 1
1.66	25.0			

TABLE A-2
Pitch Axis

	Forward		Aft
Poun	ds Degree	es Pounds	Degrees
		1.32	0.5
1.5	4 0.5	1.54	0.5
1.6	5 0.5	1.65	0.5
1.7		1.76	0.5
1.9		1.98	1.0
2.2		2.20	3.5
2.3		2.31	7.5
2.4		2.42	13.5
2.6		2.64	19.0
2.6		2.68	20.0

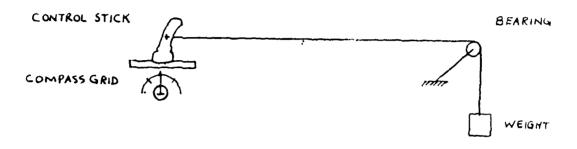


Fig A-la. Stick Calibration Setup

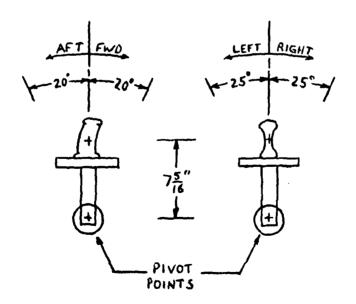


Fig A-1b. Stick Dimensions and Travel

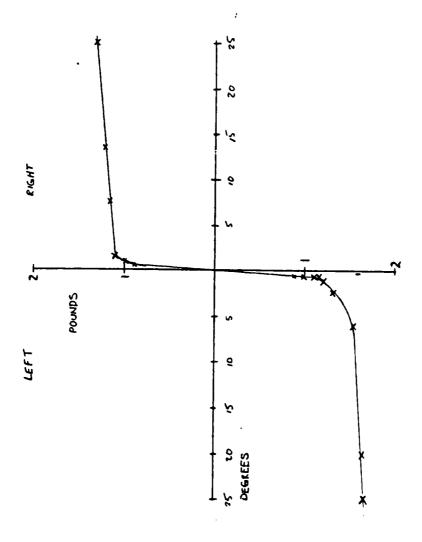
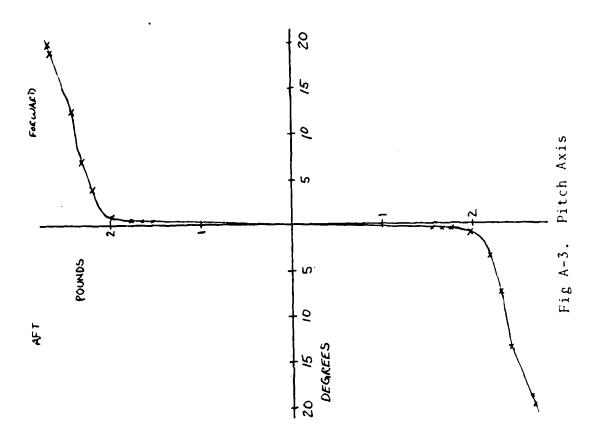


Fig A-2. Roll Axis



Stick Wiring

Since there were no wiring diagrams of the control stick, one was drawn up and is shown in Fig A-4.

Simulation Calibration

This calibration was actually used to verify that the same values of P_{SS}/F_{AS} in Monagan's paper were used for this thesis. This calibration led to the discovery that the experiments did not duplicate Monagan precisely. The potentiometer controlling the value of K had an extra τ factor which was not taken into account. The procedure for the calibration removed the control stick and replaced it with a signal of one volt for one second. This procedure was repeated for every different value of τ and K. The output of integrator 34 (Φ) was then measured with a digital voltmeter. Table A-3 shows the calculated and measured results for P_{SS}/F_{AS} .

	Calculated			Measured		
]	τ	K	P _{SS} /F _{AS}	Φ	P _{SS} /F _{AS}	
:	sec	deg/sec ²	deg/sec lb	deg	deg/sec lb	
	0.45	49.38	22.22	0.95	21.83	
	0.45 0.25	123.42 400.00	55.54 100.00	2.37 4.14	54.48 95.17	
•	0.25	160.00	40.00	1.70	39.08	
	0.80 0.80	15.63 39.10	12.50 31.28	0.54 1.34	12.41 30.80	
	0.15	1111.10	166.66	6.92	159.07	
1	0.15 0.10	444.44 1000.00	66.66 100.00	2.80 4.14	64.36 95.17	

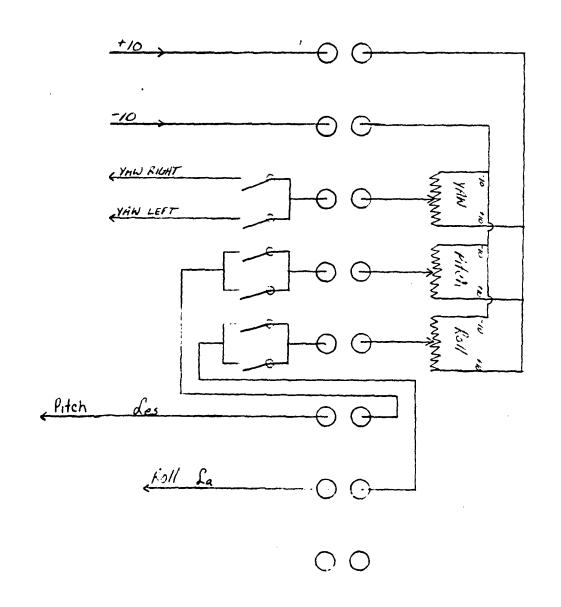


Fig A-4. Control Stick Wiring Diagram

The calculation for $R_{\rm SS}/F_{\rm AS}$ required several factors. The first value of .012 lb/deg was obtained from the stick calibration. The 7.83 deg/in was derived from the amount of stick radius moved per degree. The 2.16 v/in was obtained from Dammarell's calibration of the stick (Ref 11). Φ was measured from the output of integrator 34.

$$\frac{\text{deg}}{.012 \text{ lb}} = \frac{1 \text{ in}}{7.83 \text{ deg}} = \frac{2.16 \text{ v}}{\text{in}} = \frac{.95 \text{ deg/sec}}{\text{v}} = 21.83 \frac{\text{deg/sec}}{\text{lb}}$$

$$P_{SS}/F_{AS} = 21.83 \text{ (deg/sec)/lb}$$

The other measured values of P_{SS}/F_{AS} were calculated in a similar manner.

APPENDIX B SCHEMATIC DIAGRAMS

The EAI 2000 analog computer was used for all experiments. The pitch and roll equations, as well as the performance measures, were all programmed on one board. The descriptions are printed with the permission of Electronic Associates Incorporated of New Jersey (permission statement included). Before detailing each diagram, each individual component is described below. The schematic diagrams show the circuitry used to implement this experiment. The simulation was accomplished by the computer technician.

Oscilloscope Images

Figure B-1 is the circuit diagram for the generation of command, subject response and external trigger for the oscilloscope. Integrator zero produces the sawtooth signal (labeled X); it is connected directly to the external trigger of the oscilloscope. Signal X is also used to generate the W. The output of summer 52 is the W signal. Switch 3 allows either the subject pitch (amp 71) or roll (integrator 34) to control the W on the scope. Switch 7 allows either the sum of sine waves (switch 67) or the random step (switch 25) to control the command bar on the scope. Amplifiers 42, 45, 46, 47, and 51 make up the slopes for the W signal.

Pitch and Roll Equations

Figures B-2 and B-3 show the circuitry for the pitch and roll simulations. Since it would be too cumbersome to explain each connection in the drawings, the equations for each signal are shown as the output for the amplifiers. For continuity, summer 71 (Fig B-2) and integrator 34 (Fig B-3) are shown in Fig B-1.

Sum of Sine Waves

Figure B-4 illustrates the sum of sine waves input signal. The signal is made up of six different sine waves. The output of summer 67 is the total sum. Each sine wave has a peak voltage of one volt, therefore, the maximum peak signal is six volts. The output of track/store amp 6 is used for the generation of the random step function (Fig B-5). Switch 67 is shown in Fig B-1 for continuity.

Random Step

The random step function generator is shown in Fig B-5. Comparator 31 compares the sum of sine waves signal to one volt. The comparator inhibits signal changes of less than one volt and passes greater than one volt. Counter 26 counts down every 1.5 seconds. The track/store circuitry (o and 26) ensure a pulse change at least every two changes of flip flop 11. Therefore, the time between step changes is at least three seconds. Switch 25 is shown in Fig B-1 for continuity.

Evaluation Methods

Figure B-6 is the circuitry used to evaluate the RMS error and time on target. The output of summer 126 is the error signal and it is used by both the RMS error and time on target hardware. Comparator 35 compares the error with the margin of error. In pitch (pot 37) the margin of error is one division on the scope face. The margin of error for roll is 4 degrees (pot 33) in slope between command and subject response. The comparator inhibits signals greater than the margin of error. The increment for time on target is 0.1 volts/second. The time on target value is stored in analog to digital port number 3.

The error is fed as an RMS value into analog to digital port number 1. The circuit located in the lower left ensures an RMS error value is stored once each second.

The circuit in the lower right acts as a timed switch. It is activated when the test begins, runs for 91 seconds, then shuts off the input signal. The 91-second shutoff is needed to ensure that all the time on target and RMS data values have entered their respective analog to digital ports. The analog to digital ports keep track of the voltages and allows the digital program (Appendix C) to read and store their values.

Switching Diagram

Figure B-7 shows the switching wiring necessary for switching between the input signals and the roll and pitch

161 Millionic att Parkway, West Long Branch N.J. 07764 (201) 223-1100

August 9, 1982

Capt. Nathan Krys AFIT/EN Box 4237 Wright Patterson AFB Ohio 45433

Dear Capt. Krys:

This letter is authorizing your request to use parts of Chapter 4 from our EAI 2000 Analog Reference Book for your thesis.

If you have any additional requests, please do not hesitate to call me.

Sincerely yours,

William Hiplan

William Kaplan Product Manager

WK/ejb

4.2 COEFFICIENT UNIT

FUNCTION:

Continuous multiplication of an analog variable times a constant coefficient.

DESIGNATIONS:

DCA Digitally Controlled Attenuator or Digitally Set Coefficient Unit

POT Manually Set Coefficient Unit

SYMBOL:

As shown in Figure 4.1

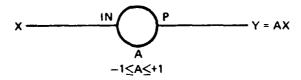


Figure 4.1 Coefficient Unit: Typical Programming Symbol

4.3 SUMMER

FUNCTION:

Continuous summation of several analog variables.

OPTIONS:

As an optional feature, the 4-input and the 7-input Summer can be equipped with a variable limiter. The limiter is described in Paragraph 4.14. Note that earlier versions of the EAI 2000 are not equipped with a 4-input Summer and its optional Limiter.

DESIGNATIONS:

SUM, 1

SYMBOL:

As shown in Figure 4.4

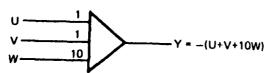


Figure 4.4 Summer: Typical Programming Symbol

4.4 INTEGRATOR

FUNCTION:

Continuous integration, with respect to time, of an analog variable.

OPTIONS:

As an optional feature, the Integrator can be equipped with a variable limiter. The limiter is described in Paragraph 4.14.

SYMBOL:

As shown in Figure 4.6.

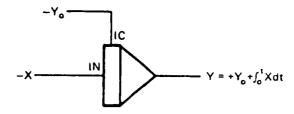


Figure 4.6 Integrator: Typical Programming Symbol

4.5 MULTIPLIER

FUNCTION:

Continuous multiplication of two analog variables.

DESIGNATIONS:

MUL

SYMBOL:

As shown in Figure 4.9.

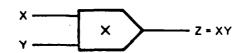


Figure 4.9 Multiplier: Typical Programming Symbol

4.7 SQUARE ROOT GENERATOR

FUNCTION:

Generate the Square Root of an analog variable.

DESIGNATION: V

SYMBOL:

As shown in Figure 4.13.

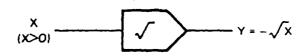


Figure 4.13 Square Root Generator: Programming Symbol

4.8 TRACK-STORE UNIT

FUNCTION:

Store an analog value.

OPTIONS:

As an optional feature, later versions of the TS/ Σ tray (Model Number 0.72.0051-1) contain a Limiter that is associated with the Track-Store Unit. The Limiter is described in Paragraph 4.14. The earlier versions (Model Number 0.72.0049) TS/ Σ tray does not have this option.

DESIGNATIONS: T/S

SYMBOL:

is shown in Figure 4.16.

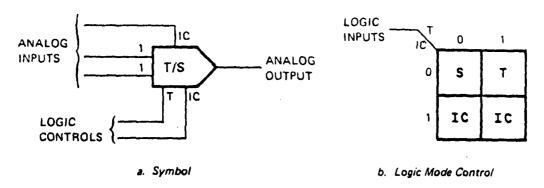


Figure 4.16 Track-Store Unit: Programming Symbol

4.9 SELECTOR SWITCH

FUNCTION:

Analog Signal Switching

DESIGNATION: SW

SYMBOL:

As shown in Figure 4.21.

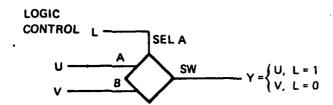


Figure 4.21 Selector Switch: Typical Programming Symbol

4.10 SINE GENERATOR

FUNCTION:

Generate the Sine of an analog variable.

'GNATION: SIN

SYMBOL:

As shown in Figure 4.23.

$$\begin{bmatrix} \frac{\theta}{\pi} \end{bmatrix} - \pi \le \theta \le + \pi$$
SIN
$$Y = \sin \theta$$

Figure 4.23 Sine Generator: Typical Programming Symbol

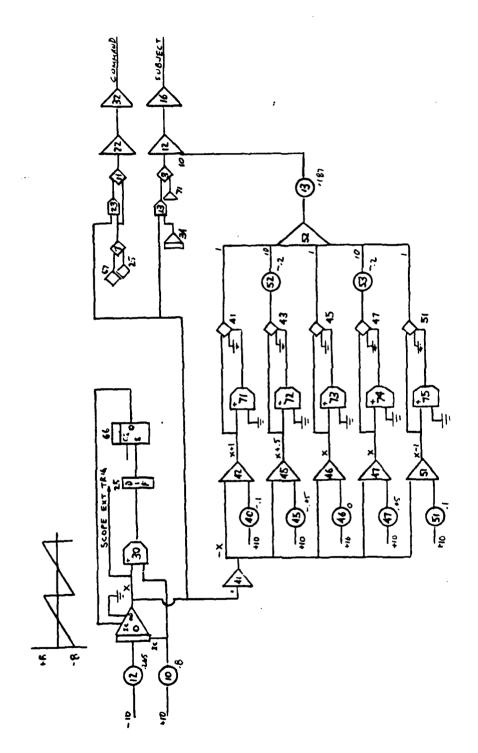


FIGURE [.] GENERATION OF COMMAND AND W SIGNALS

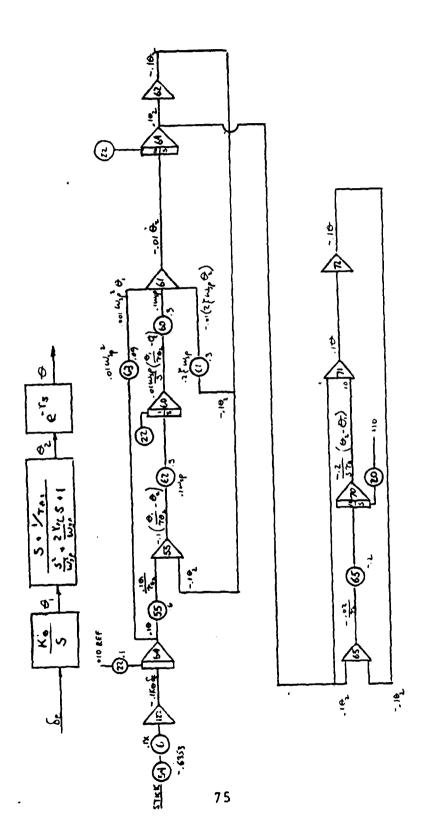


FIGURE B.2 PITCH SIMULATION

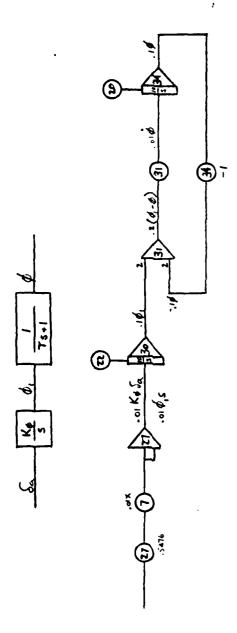


FIGURE 8-3 ROLL SIMULATION

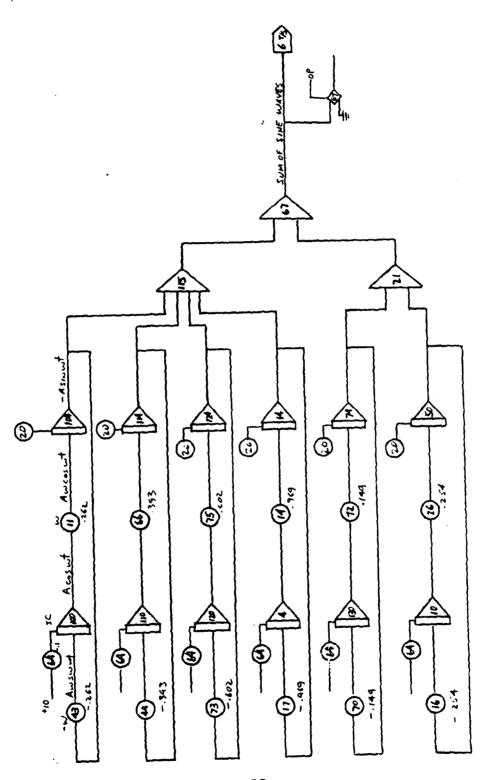


FIGURE BA GENERATION OF SUM OF SINE WAVES

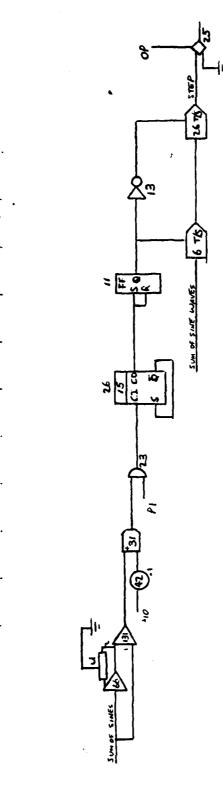


FIGURE B-S GENERATION OF RANDOM STEP FUNCTION

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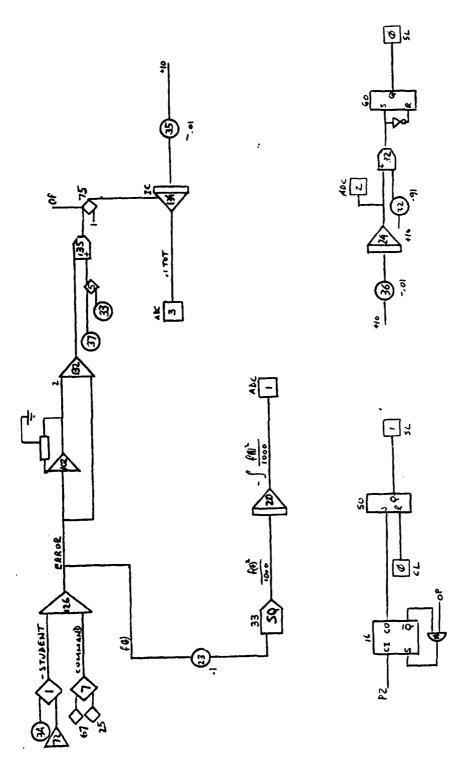


FIGURE 8-6 EVALUATION CIRCUITRY

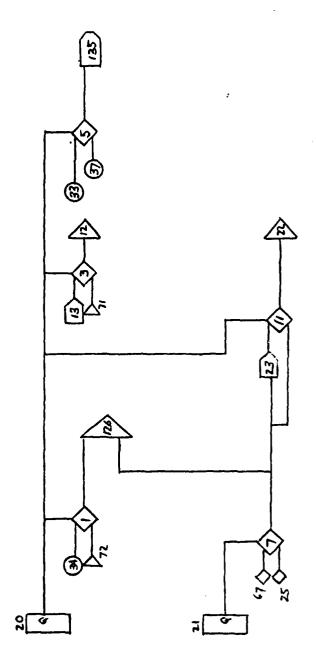


FIGURE B.7 SWITCHING INTERCONNECTIONS

APPENDIX C

PROGRAM USED TO INITIALIZE THE EAI 2000 ANALOG COMPUTER

The purpose of this program is to initialize the system on the EAI 2000 by setting specific values for all potentiometers, integrators and counters. It also changes potentiometers to show the change in variables for the different runs involved.

After the program begins the run, it monitors flip flops 50 and 60 (Appendix B, Fig B-6). If flip flop 60 is set high, the run has gone 91 seconds and the program stops the run. If 50 is high, the program samples and stores the values of analog to digital converters 1, 2, and 3 stores the values in an array and resets flip flop 50.

When the run has stopped (flip flop 60 - high), the program calculates the RMS mean error and time on target, then prints out the values.

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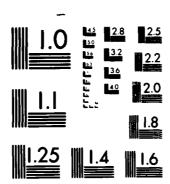
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CALCULATE K FOR ROLL AND PITCH
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                                                                                                                                 DE SECONDS UP. END OF RUN
                                                                                                                                                                                            A20(1)=A5S(AUC(1)+1000.)
                                                                                                                                                                                                                                                                                                                   COMPLETE RMS CALCULATIONS
A20(1)=A85(ADC(1)*1060*)
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          101(1)=A68(A50(3)*10*)
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                                                               SUBROUTINE CHIMSG(IBUF+NB)
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APPENDIX D
PILOT EXPERIENCE AND TESTING SCHEDULE

<u>Pilot</u>	Aircraft	Hours Flown
DS	T-38' F-16	1400 350
МK	T-33 C-47,B-25	800 1000
MM	C-141	2200
RL	F-111	1800
SF	F-4	500

Pilot Te	st Start #,	Sum of S	ines	Test Start	#/Step	Function
DS	4/2	Aug		1/9	Aug	
MK	7/3	Aug		10/12	Aug	
ММ	10/10	Aug		1/9	Aug	
RL	1/16	Aug		4/10	Aug	
SF	1/29	Aug		7/5	Aug	

APPENDIX E

PILOT COMMENT DATA

This appendix contains all the pilot comments and ratings given during the test runs. Most of the comments are one-word descriptions, and each thought is separated by a comma. All τ 's refer to τ_R .

Sum of Sine Waves

Pilot: DS Date: 2 Aug

Test 1 τ = .45 K = 49.38 PR 4 too sluggish, I can keep up with the command signal, but the stick is too sluggish

Test 2 $\tau = .45$ K = 123.42 PR 3 better, less sluggish, some lead required

Test 3 τ = .45 K = 133.33 PR 2.5 fast response, felt like I have weights on the wings, slight PIO, overshot

Test 4 τ = .25 K = 400 PR 2 pretty good, responded the right amount for stick movement, responded quickly

Test 5 τ = .25 K = 160 PR 2.5 not a whole lot of difference, not as responsive to stick inputs

Test 6 $\tau = .25$ K = 320 PR 2 felt like Test 4, no difference, just fine

Test 7 $\tau = .8$ K = 15.63 PR 7.5 sluggish stick, couldn't keep up with command signal

Test 8 τ = .8 K = 39.1 PR 7 some improvement, roll would keep up with command, some PIO (overshoot)

Test 9 $\tau = .8$ K = 225 PR 4

fairly quick response, I didn't like it, small stick input made large change in W

Test 10 $\tau = .15$ K = 1111.1 PR 4 required a lot of effort not to overcontrol, fast response

Test 11 $\tau = .15$ K = 444.44 PR 3 this is better, not as much effort (required to control), fast response

Test 12 $\tau = .15$ K = 833.33 ' PR 2 fast response, no problem with control

Test 13 $\tau = .1$ K = 1000 PR 1.5 liked it, fast response, no PIO (overshoot)

No Test 14, after several runs, DS could not improve on Test 13.

Pilot: MK Date: 3 Aug

Test 1 $\tau = .45$ K = 49.38 PR 6 response too sluggish, no overshoot

Test 2 τ = .45 K = 123.42 PR 4.5 much better, response to stick is still sluggish

Test 3 $\tau = .45$ K = 388.88 PR 5 response still sluggish, overshoots

Test 4 $\tau = .25$ K = 400 PR 3.5 better, responds quicker and small overshoot

Test 5 $\tau = .25$ K = 160 PR 4.5 too sluggish, overshoot okay, very slow

Test 6 $\tau = .25$ K = 800 PR 3 sluggish, slight overshoot, not enough damping

Test 7 τ = .8 K = 15.63 PR 7.5 not responsive, doesn't respond quick enough, overshoots, plant is no good

Test 8 τ = .8 K = 39.1 PR 6.5 not quite so bad, responds too slowly, still overshoots

Test 9 τ = .8 K = 225 much better adequate response, still too much inertia and overshoot

Test 10 τ = .15 K = 1111.1 PR 3.5 easier to track, too much inertia and slight overshoot

Test 11 $\tau = .15$ K = 444.44 PR 3 best one yet, responded quick, less overshoot

Test 12 $\tau = .15$ K = 900 PR 2 very responsive, no overshoots, no complaints, easy to fly

Test 13 $\tau = .1$ K = 1000 PR 2.5 not responsive, damping okay, no overshoot

Test 14 τ = .1 K = 2000 * PR 2.5 I like this, pretty responsive, little overshoot, good damping

Pilot: MM Date: 10 Aug

Test 1 $\tau = .45$ K = 49.38 PR 6 terrible, sluggish, stick seemed almost dead, it was slow when I wanted to move in a different direction, no good

Test 2 τ = .45 K = 49.38 PR 4 better, faster reaction to stick input, smoother not as sluggish as before, stick more sensitive, stick more proportional (further I move the stick--faster the response)

Test 3 $\tau = .45$ K = 277.77 PR 2 better, went right where I wanted it to go, just about right

Test 4 $\tau = .25$ K = 400 PR 4 a little slow, otherwise pretty good

Test 5 τ = .25 K = 160 PR 5.5 seemed even more slow, less sensitive, (I was) always behind what I wanted to do

Test 6 τ = .25 K = 600 PR 1.5 sensitivity good, reaction time on stick response good, proportional stick, overall pretty good, (I) liked it

Test 7 $\tau = .8$ K = 15.63 PR 8 terrible, slow, very sluggish, bad overall

Test 8 $\tau = .8$ K = 39.1 PR 5.5 little better, not as sluggish, too much inertia, overshoot

Test 9 τ = .8 K = 143.75 PR 3 sensitivity good, less inertia, fast reaction time, therefore had to compensate for overshoot, overall not bad-fairly good

Test 10 τ = .15 K = 1111.1 PR 4 good and smooth, a little fast at times, not bad overall,

needed more control (since it) wasn't sensitive enough

Test 11 τ = .15 K = 444.44 PR 2.5 better overall, sensitivity better, good and smooth, easier flying task

Test 12 τ = .15 K = 833.33 PR 2 better, improved sensitivity, everything else is the same, it reacts better

Test 13 τ = .1 K = 1000 'PR 4 fair, smooth, sensitivity (reaction of stick) was stair stepped, no extra momentum, W stopped when stick movement stopped

Test 14 τ = .1 K = 1250 PR 1 pretty good, smooth, sensitivity easy to control, just about right proportional movement of stick, no lag time, response was instantaneous

Pilot: RL Date: 16 Aug

Test l τ = .45 K = 49.38 PR 6 not very good, initial response slow, roll rate slow, overshoot, used maximum stick deflection to arrest roll rate

Test 2 τ = .45 K = 123.42 PR 5 better, primarily response is more predictable in arresting roll rate, initial response about the same

Test 3 τ = .45 K = 277.77 PR 4 seemed roll rate was non-linear before, this was more predictable, roll in and roll out no change, command got away from me before but I had better response with this run, warrants improvement

Test 4 τ = .25 K = 400 PR 4 didn't seem very predictable, roll in response didn't have a good feel, needed compensation

Test 5 τ = .25 K = 160 PR 4 slower, more predictable, easier to control, actually better in accomplishing task

Test 6 τ = .25 K = 600 PR 3 mildly unpleasant deficiencies, occasional small PIO (overshoot) very minor though, minimum desired performance better

Test 7 τ = .8 K = 15.63 PR 7 not very good, bang-bang system, definitely requires improvement, can't perform task, slow system, need max

deflection, control no problem

Test 8 τ = .8 K = 39.1 PR 7 better but not by much, quicker, roll out still needs lead time, task still difficult

Test 9 τ = .8 K = 156.25 PR 6 very objectionable, extensive compensation, must anticipate an input that can't be anticipated, tendency to overshoot

Test 10 τ = .15 K = 1111.1 , PR 5 needs improvement, still need pilot compensation, real high gain, less overall error but when there is an error (I) miss it by a lot

Test ll τ = .15 K = 444.44 PR 6 need something in between, poor initial response--all gone, there's more overshoot

Test 12 τ = .15 K = 833.33 PR 3 best overall, good response for large amplitude corrections

Test 13 τ = .1 K = 1000 PR 4 not all that bad, roll out response not predictable--a little too quick, for large correction some overshoot

Test 14 τ = .1 K = 1500 PR 2 negative deficiencies, predictability in roll out response, roll rate control very good, pretty good, very small corrections difficult to make, overall very good

Pilot: SF Date: 29 July

Test l τ = .45 K = 49.38 PR 5 very sluggish, as I approach target--can't feel where l should line up with target, smooth but excessive time delay

Test 2 τ = .45 K = 123.42 PR 3 nice reacting system, tended to overshoot but didn't task me, don't know how system reacts to my input, better than before, good feedback or stick motion, comfortable

Test 3 τ = .45 K = 166.66 PR 2 good system, easy to control, good feedback, good rate and position, slight overshoot, (I have to) anticipate targets

Test 4 τ = .25 K = 400 PR 1.5 really sharp, used very discrete inputs--almost digital, stopped W whenever I wanted to

Test 5 τ = .25 K = 160 PR 7 slow in responding, couldn't get it where I wanted, by the

time I got there target moved, need lots of compensation, good on small error not large

Test 6 τ = .25 K = 320 PR 2 I like it, able to precisely stop motion, bank rate is better on roll in

Test 7 τ = .8 K = 15.63 \pm R 8 time delay too large, no roll rate, no roll out, have to lead system, target is faster than me, command signal was contolling me

Test 8 τ = .8 K = 39.1 PR 7 rate slope not linear, couldn't judge input, very sluggish, overshot, good for catching up but not for stopping

Test 9 τ = .8 K = 237.5 PR 4 responsive but abrupt, mushy handling, good course correction but no fine correction, time delay acceptable, felt more comfortable to make little inputs

Test $10 \tau = .15 K = 1111.1 PR 1$ best one so far, easy to line up very responsive, very easy to control, no time delay, a little abrupt, easy to predict stick movement to correct error

Test 11 $\tau = .15$ K = 444.44 PR 4 higher time delay needed to lead the command signal, crisp in eliminating input, slow in getting input in, behind the power curve but didn't have to chase target, not as good as Test 10, for larger errors this system would be very deficient

Test 12 τ = .15 K = 666.66 PR 1 large errors show a slight objectionable time delay in input, crisp tracking good, didn't need to lead

Test 13 τ = .1 K = 1000 PR 3 slow moving target, I couldn't follow it, needed discrete inputs (steps), not objectionable for large errors

Test 14 τ = .1 K = 750 PR 3 slight tendency to overshoot not quite as crisp, good tracking, inputs smooth and reasonable, didn't need to move the stick very much

Random Step

Pilot: DS Date: 9 Aug

Test 1 $\tau = .45$ K = 49.38 PR 7

real slow, required full stick deflection

Test 2 $\tau = .45$ K = 123.42 PR 3 much faster response, slight tendency to overshoot

No Test 3, could not improve stick response compared to Test 2.

Test 4 $\tau = .25$ K = 400 PR 2 much faster, less tendency to overshoot, liked it

Test 5 $\tau = .25$ K = 160 PR 3 little too slow, less tendency to overshoot

Test 6 $\tau = .25$ K = 360 PR 2 real good, easier to control straight and level

Test 7 τ = .8 K = 15.63 PR 7.5 too slow, needed to use full stick deflection, too stable to oscillate

Test 8 τ = .8 K = 39.1 PR 7 slightly better, still required full stick deflection, large tendency to overshoot, used full stick to start and full stick to stop

Test 9 τ = .8 K = 125 PR 5.5 has big overshoot problem, responded fairly quickly, need a lot of compensation to control overshoot

Test 10 τ = .15 K = 1111.1 PR 5.5 great tendency to overcontrol, had to compensate, very quick response, just too sensitive, no appreciable overshoot

Test 11 τ = .15 K = 444.44 PR 2 better, more easily controlled, no appreciable overshoot

Test 12 τ = .15 K = 533.33 PR 1 very nice, no overshoot, quick response, good tradeoff between response and stability

Test 13 $\tau = .1$ K = 1000 PR 2 good, no overshoot, quick response

Test 14 τ = .1 K = 600 PR 1.5 good, no tendency to overshoot, quick response but controllable

Pilot: MK Date: 12 Aug

Test 1 $\tau = .45$ K = 49.38 PR 4 easy to fly, doesn't matter what I do W will eventually get

there

Test 2 $\tau = .45$ K = 123.42 PR 4.5 kind of sluggish, tended to overshoot, I did not like this

Test 3 τ = .45 K = 44.44 PR 4 easier to fly, better because the W responded more quickly, good damping, not too much overshoot

Test 4 τ = .25 K = 400 PR 3 like that better, good damping, not much overshoot, quick response

Test 5 $\tau = .25$ K = 160 PR 3.5 just as easy as before, I don't like the way it feels

Test 6 τ = .25 K = 500 PR 3.5 this is as good as I can do it, if it responds quickly, I like it, if it overshoots much I don't like it

Test 7 τ = .8 K = 15.63 PR 4 too much inertia, response is too slow, overshoots, uselessly atypical--never bang an airplane against stops except in acrobatics, easy to maintain task

Test 8 $\tau = .8$ K = 39.1 PR 5 too much inertia, response is quicker but harder to fly

No Test 9, could not improve on Test 7.

Test 10 τ = .15 K = 1111.1 PR 3 nice airplane, very responsive, quick no inertia, as soon as I move stick airplane moves

Test 11 $\tau = .15$ K = 444.44 PR 3 different but flies nice, response is slow, no overshoot

Test 12 $\tau = .15$ K = 1333.33 PR 3 I like this the best, quick response

Test 13 $\tau = .1$ K = 1000 PR 3 like this better, response is quicker, less overshoot

Test 14 τ = .1 K = 750 PR 2.5 responds real quick and stops, absolutely no overshoot, this is the best one

Pilot: MM Date: 9 Aug

Test 1 τ = .45 K = 49.38 PR σ too dull, stick not sensitive enough, had to overcompensate

Test 2 τ = .45 K = 123.42 PR 6 sensitivity has not changed, definite improvement in stick response, quicker, not bad overall--fair

Test 3 τ = .45 K = 155.55 PR 2.5 better than Test 2, didn't like sensitivity (not enough), speed compensated, easy to control, pretty good overall

Test 4 τ = .25 K = 400 PR 4 good, moderate speed, could be more sensitive

Test 5 τ = .25 K = 160 PR 2 better than Test 4, not as sensitive--almost like being sluggish, I liked it

Test 6 $\tau = .25$ K = 240 PR 1.5 sensitivity real good, nice and smooth movement

Test 7 τ = .8 K = 15.63 PR 5.5 too slow, W had some momentum, dull reacting, had to really push the stick

Test 8 τ = .8 K = 39.1 PR 5 sensitivity better, kind of dull, not much inertia--about the same as before, slightly better than Test 7

Test 9 τ = .8 K = 100 PR 4 sensitivity real good, liked the way it moved, sensitivity helped--compensated for the momentum

Test 10 τ = .15 K = 1111.1 PR 7 moved fast, didn't like it, sensitivity was good (didn't have to move the stick as far)

Test 11 τ = .15 K = 444.44 PR 2.5 much better sensitivity, just right, good response

Test 12 τ = .15 K = 533.33 PR 1 handled real well, good speed in response, sensitivity is good, moved when I wanted it to, felt real smooth, even flow, good overall

Test 13 τ = .1 K = 1000 PR 5 overall pretty fair, sensitivity okay, slightly unstable, felt like it was moving on its own, good speed for correction

Test 14 $\tau = .1$ K = 850 PR 1 good, nothing wrong, smooth, felt good

Pilot: RL Date: 10 Aug

- Test l τ = .45 K = 49.38 PR 3 slow roll, initial okay, overshot slightly but easy to overcome, used full stick deflection
- Test 2 τ = .45 K = 123.42 PR 2 roll rate faster, initial response good, overall predictable, liked it better, less stick deflection, less overshoot
- Test 3 τ = .45 K = 444.44 PR 2 nothing unpleasant, roll in good, roll out rate not the same, very predictable, slight overshoot but not PIO
- Test 4 τ = .25 K = 400 PR 3 slower system, less responsive, predictable, large correction gave slight overshoot but no PIO
- Test 5 τ = .25 K = 160 PR 2 better, more predictable especially in rolling out, more solid, roll rate good, most predictable
- Test 6 τ = .25 K = 208 PR 2 good and predictable, easiest task to accomplish so far
- Test 7 τ = .8 K = 15.63 PR 4 didn't like it, very sluggish, long roll in, small corrections hard to make, large corrections are easier, no PIO
- Test 8 τ = .8 K = 39.1 PR 4 improved response, small corrections easier, tend to overshoot on large corrections, still sluggish, no PIO
- Test 9 $\tau = .8$ K = 100 PR 4 sluggish, have to force overshoot, heavy workload
- Test 10 τ = .15 K = 1111.1 PR 3 good response, tendency to overshoot but less than before, very sensitive--not what you want for ILS final, otherwise good
- Test 11 τ = .15 K = 444.44 PR 3 better than before, less sensitive especially for small corrections, goo as far as roll out
- Test 12 $\tau = .15$ K = 500 PR 3 minimal pilot compensation
- Test 13 τ = .1 K = 1000 PR 3 good, better than the last test (Test 12), roll out response predictable, less tendency to overshoot
- Test 14 $\tau = .1$ K = 750 PR 2

roll out predictable, no pilot workload

Pilot: SF Date: 5 Aug

Test 1 τ = .45 K = 49.38 PR 6 very slow responding, needed considerable lead, not precise--couldn't tell where I would end up, had to put lead in, time delay okay

Test 2 $\tau = .45$ K = 123.42 PR 8 roll PIO problem, didn't know when to take rate out, difficult to control, too much compensation needed

Test 3 τ = .45 K = 88.88 PR 4 best one, (had to) kill motion with opposite input--pilot lead, hard to predict, rate acceptable, no real PIO

Test 4 τ = .25 K = 400 PR 7 PIO (pilot induced oscillation), too abrupt, rate seemed high

Test 5 τ = .25 K = 160 PR 2.5 very predictable, a little sluggish, good system, very tolerable

Test 6 τ = .25 K = 140 PR 2 good system, frequency a little low, could be more responsive, very tolerable, like it

Test 7 τ = .8 K = 15.63 PR 7 very sluggish, terrible system, had to wait on response, had to predict when to take out input

Test 8 τ = .8 K = 39.1 PR 8.5 sluggish, PIO prone, time delay hard to manage, verging on uncontrollability at times, not precise, rate too slow, not crisp

Test 9 τ = .8 K = 62.5 PR 5 sluggish, pilot lead required, little PIO, no problem with control, compensation required, phase lad noticeable but not objectionable

Test 10 τ = .15 K = 1111.1 PR 2.5 pretty precise, (I) wanted to let the stick drift into the target, good system

Test 11 τ = .15 K = 444.44 PR 5 breakout force very high, very sluggish, had to wait for the W to move, precise and smooth

Test 12 $\tau = .15$ K = 833.33 PR 2

 $\ensuremath{\text{good}}$ system, a little on the abrupt side, had to compensate for the high rate

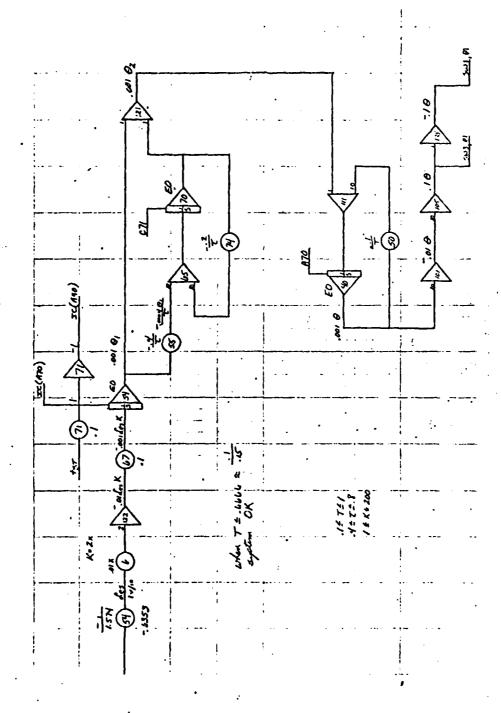
Test 13 τ = .1 K = 1000 PR 2 can't tell much of a difference (from Test 12), the gain is less, seems to be good, (the task is) not exercising me

Test 14 τ = .1 K = 750 PR 3 slight tendency to bobble, (I) can judge the stick however

APPENDIX F

SCHEMATIC FOR EQUATION 5

Figure F-1 is the schematic for Eq (5), the only pitch equation which had no stability problems.



APPENDIX G

SAMPLE STRIP CHART RECORDINGS

The following are sample strip chart recordings. Figures G-1 through G-3 show the Test 1 for MM. Figures G-4 through G-6 show Test 13 for MK. The voltage values in all of the figures are the following:

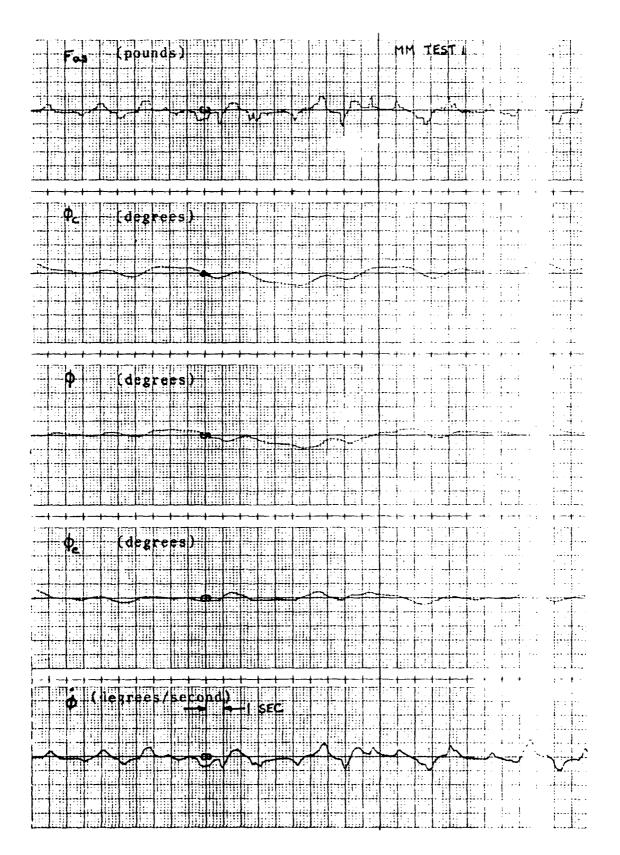
 $F_{AS} = .05 \text{ v/div}$

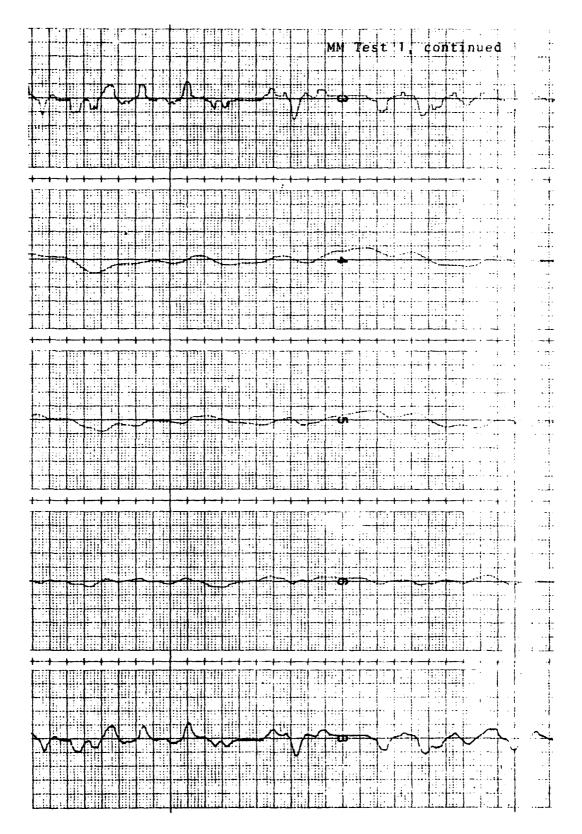
 $\phi_c = .5 \text{ v/div}$

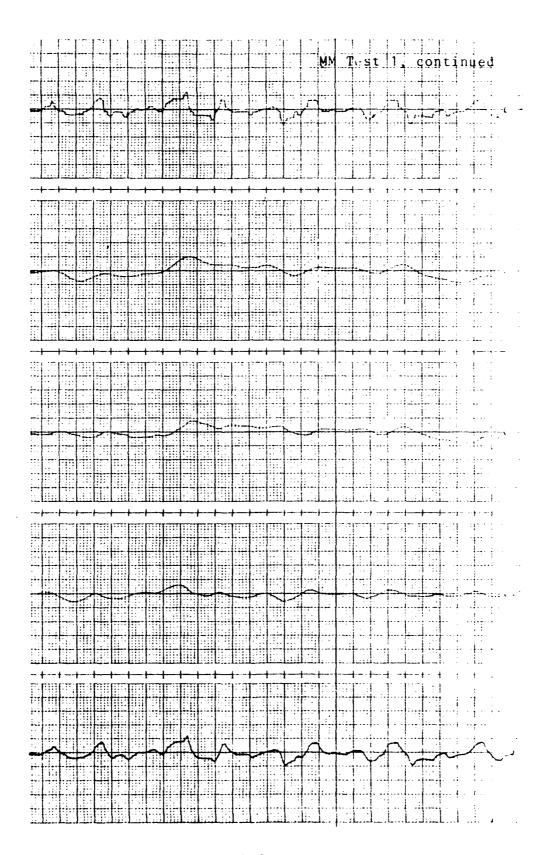
 $\Phi = .5 \text{ v/div}$

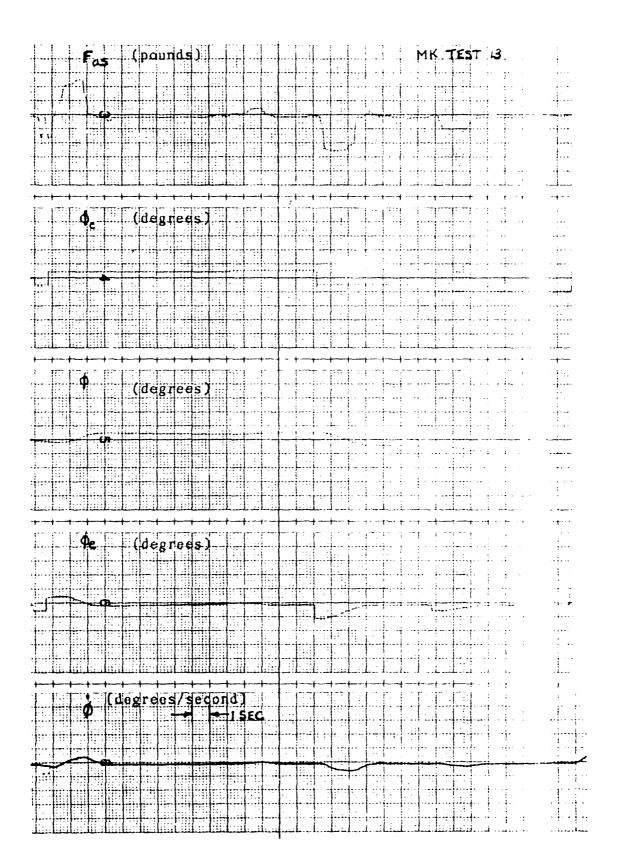
 $\Phi_e = .5 \text{ v/div}$

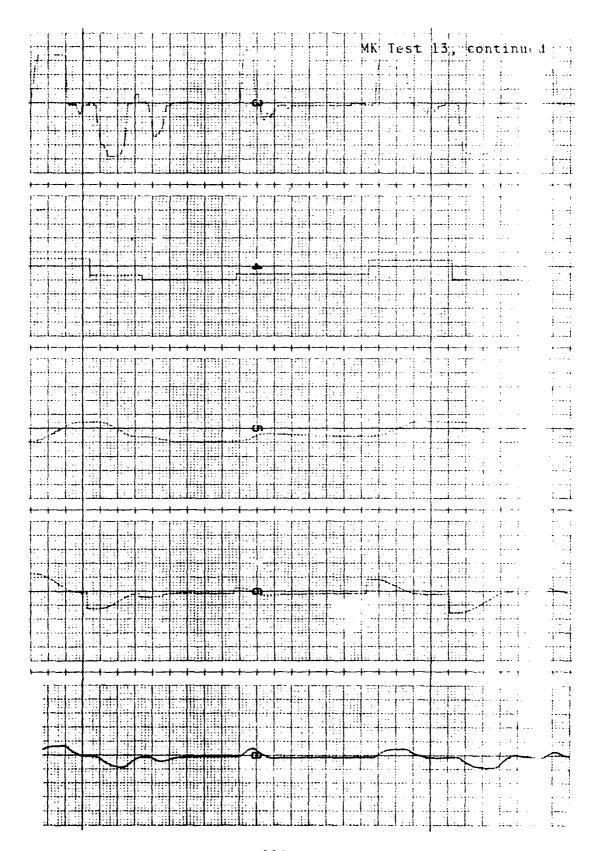
 $\dot{\phi} = .05 \text{ v/div}$

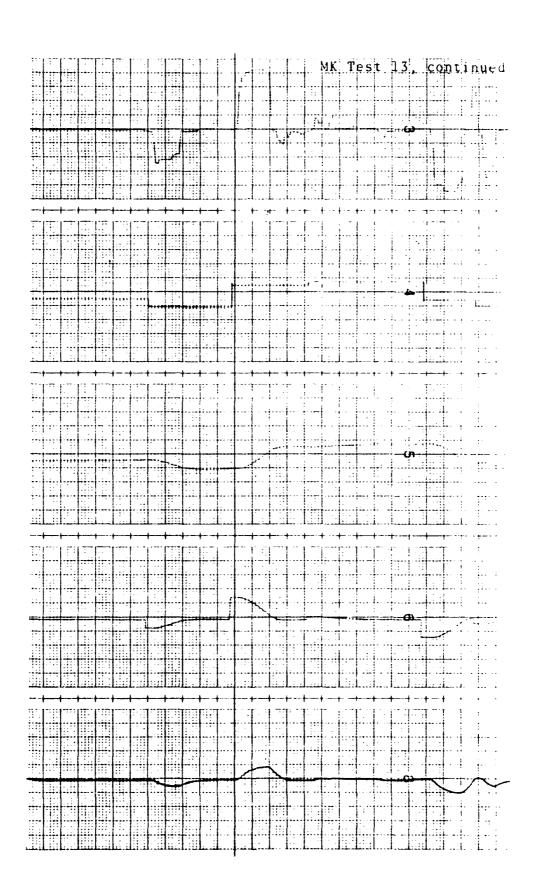












100 1000 1000 100

APPENDIX H

TABULATED DATA FOR RMS ERROR AND

TIME ON TARGET

The data in this appendix are read from left to right. The first value is located in the top left and last value in the bottom right. The data were printed for every second during a 90-second period. The first 10 values of RMS error were not used because of the physical limitation on the multipliers used (5 millivolts/10 volts). The first 10 values of error were on the order of 0.01V or less, giving an error of 50% or more. The RMS error value was calculated by the formula below.

RMS error = $\frac{1}{t} \int_{0}^{t} (error)^{2} dt$ Note: t is the time at any one point.

The mean of RMS is the average of the last 80 values for RMS error.

The list below are those tests where the subject could not improve stick action when the stick gain was changed. Therefore, there were no runs for the following tests:

Test 9 step function MK

Test 3 sum of sine waves DS

Test 14 sum of sine waves DS

DS test 1

RULL STEP FUNCTION

	R	MS VALUE I	t LKK is		
0.00	1.57	1.70	1.//	↓ • O →	1 .
1.3)	1.36	1.2),	$1 \rightarrow 1$	1.21	
1.14	1.53	1.57	1.74	1.53	4. 1
1.42	1.45	1.57	1.54	1.35	1. 3
1.55	1.29	1.25	1.23	1.24	1. 7
1.20	1.27	1.27		1.26	/
1.25	1.24	1.22	1.75	4.19	.
1.17	1.23	1.22	$1 \cdot 21$	1.23	1.
1.21	1.21	1.21	1.22	1.13	1. 7
1.59	1 • 58	1.54	1 • 50	1.30	1. 1
1.35	1.35	1 • 3 =	1 . 50	1.33	$1 \cdot \cdot 1$
1.38	1.39	1.550	1 • ⇒7	1.57	1.
1.42	1.41	1.5,	1.44	1.45	ī.,
1.44	1 - 44	1.45	1 • +2	1.44	1
1 - 4 4	1.45	1.42	1.42	1.4.	1.

164N OF MMS= 1.34

TIME ON TARVET (SECS)						
0.20	1.20	1.48	2.24	>•25	• •	
5.29	6 • 53	7.31	8 • 55	6 • 3 to	1	
11.36	11.45	12.28	13.2b	14.53	1	
10.51	17.38	18.36	19.59	20.40	41.	
22.03	22.85	23.90	24 . 70	21000	200	
27.93	28.05	2∄•4₺	30 • JA	51.0c	581.	
33.14	34.14	50.14	35 • L2	37.20	· · · · · · · · ·	
3 ± • 3 2	39.32	40.53	40.50	41.02	** **	
43.66	44.68	45.72	40.09	41.74	71.	
48.31	49.31	20.52	51.35	52.34	P. C	
54.57	54.55	20.21	ວຍ • ⊃ 7	57.03	.7.	
ລ່ຢ • 4 ຯ	29.46	υÜ•51	61.54	52.47	40	
63.42	5¢ • 4c	on•45	စည်း မေပါ	១៦.3ថ		
68.35	59.35	70.3€	71.30	71.70	; ; ·	
13.51	74.60	7 2 • 5 7	15.7	17.52	7	

DS test 2

RULL STEP FUNCTION

		KMS VALUE O	F EKROK		
0.00	1.11	U .64	0.79	نا ♦ کا ف	4
1.11	0.36	1.55	1 • ¬7	1.01	1 3
1.69	1.75	1.65	1.7	1.52	. >
1.51	1.49	1.45	1.52	1.50	4 . 1
1.51 .	1.64	1 • 6 0	1.78	1.55	1 /
1.56	1.50	1.51	1.46	1.50	i •
1.45	1.48	1.42	1.45	1 • 4 1	1 + 5
1.45	1.42	1.51	1 • 55	1.51	$1 \cdot \cdot j$
1.45	1.48	1.45	1.47	1.55	1 5
1.50	1.49	1.50	1 • 48	1.50	1
1.50	1.49	1.47	1.45	1.4.	£ - + 5
1.46	1 • 4 4	1.45	1.43	1.41	1 +2
1.40	1 - 44	1.42	1.44	1.45	1 -5
1.47	1 - 44	1.40	1.45	1.40	, i ,
1.46	1.46	1.46	1.45	1.45	1

1EAN OF RMS= 1.49

TIME ON TARGET (SECS)						
0.53	1.56	2.56	3.03	4.65	1	
6.61	7.61	1.79	8 • 25	4.23	J	
10.34	11.35	12.38	13.33	14.30	$1 \cdot \cdot \cdot 5$	
10.46	17.41	16.45	10.07	15.60	31 3	
21.29	21.70	22 .7 0	25.75	24.74	- 1.15	
26.09	27.13	217	29.10	30.15	51 .4	
32.17	33.25	34.22	33 • 29	36.00		
57.48	38.50	30.05	57.49	46.50	41. 1	
42.52	43.53	44.54	43.01	43.56	4 . 7	
47.68	40.67	43.73	50.12	51.32	- I -	
52.96	53.95	54.43	55.99	57.04	5 . 3	
5y.06	60.06	61.09	c2•10	53.11		
65.13	ou • 27	66.32	61.26	5 h • 3 b		
69 . 52	70.48	71.55	72 • 52	16.096	75. 6	
74.66	75.71	76.65	77.70	75.63	10.00	

DS test 4

HOLL STEP FUNCTION

	R	MS VALUE O	F とれないな		
1.56	2.09	1.58	1.47	1 • 4 3	1.
1.20	1.24	1.25 :	1 • 45	1.74	ì.
1.71	1.71	1.52	1 = 64	1.52	i .
1.53	i • 45	1.45	1.45	1.27	1
1.41	1.52	1.51	0 د م 1	1.57	1 •
1.52	1.00	1.57	1.00	1.54	1.
1.47	1.50	1.48	1.45	1.47	1.
1.44	1.44	1.41	1.42	1.38	4 •
1.37	1.57	1 7	1.43	1.46	1.
1.43	1.43	1.45	1.44	1 • 4 1	i • •
1.52	1.04	1.52	1.55	1.51	1.
1.53	1.58	1.57	1.00	1.05	i •
1.54	1.53	1.52	1.54	1.53	1 •
1.53	1.51	1.51	1.001	1.49	1 •
1.48	1.47	1.48	1.47	1.40	1

MEAN OF RMS= 1.50

TIME ON TAMOFF (SECS)						
1.00	1.51	1.00	2•ಇರ	·•95	** • `	
2.25	6.51	7.30	8.15	3.24	• •	
10.30	11.29	12.54	13.35	1 4 ⋅ 3 ti	1	
10.51	17.59	13.35	17.44	23.45	21.	
22.52	22.19	23.74	24.75	30.58	200	
20.93	27.75	28.93	29.98	30.9°	31. /	
33.04	34.01	35.03	36.12	37.00	٠٠.	
39.12	40.13	41.14	42.16	45.18	44.	
45.21	40.21	47.22	47 • 54	40.25	4	
v0.3d	21.34	52.37	53.37	74.57	o • .	
22.83	96.31	57.58	ა ნ • პნ	55 .5 €	2.5	
. 0 •58	1.39	52.61	53.63	೨୩• ៦೮	to •	
06.60	67.70	00.71	69.10	59.97	71.	
72.00	73.03	74.10	75.05	76.05	77.	
72.03	19.07	80.12	81.15	82.16	33. ·	

ns test 5

12	OLL			
	7.10	E 112	· • •	1.1.

	ľ,	45 VALUE O	F ERRIR		
1.91	18	u •91	1.55	J.8-	1.1
1.11	0.03	1.50)	1.30	1.42	1 • 50
-	1 • . 6	1.25	1.55	1.23	1.1?
1.34	1.51	1.01	1.73	1.00	1 • 100
1.22	=	1.59	1 • 1,0	1.503	1.00
1.61 .	1.54	1.62	1 • 21	1.45	1 • • /
$I \bullet D \bar{\phi}$	1.12	1.54	1.02	1.51	1. 1
1 • 4 7	1.04		1.40	1.45	1.45
1.50	1.40	1 • 4 4	1.47	1.47	1.47
1.51	1 • 4 8	1.45	_	1.58	1
1.45	1 • 24	1.05	$1 \cdot \circ 1$	1.55	1.1
1.56	1.05	1.55	1.75		1.74
1.5.	1.51	1 • ∷ ∂	1 • >4	1.54	=
1.52	1.00	1.691	1.00	1.5.	1 •
1.51	1.02	1.01	$1 \cdot 1$	1.49	1 • •
1.4.	1.48	1.47	1.46	1.50	1.51

10AN OF 115= 1.44

TIME ON TAKOIT (330)						
0.13	0 • (9	1.91	2.11	5 • ± 5	5 • 5 ñ	
5 • 6 €	J. 99	7.55	8.15		$1 \circ 1$	
11.21	11.00	12.70	13.71	14.73	40.16	
15.73	17.20	17.73	A	1 " • 3 1	20.00	
20.92	21.97	22.97	د . ه د د	23.31	24 . 10	
20.00	20.49	24.60	21000	37.00	51.07	
32.07	32 • 45	J ± •04	54 • 35	31 • Ú n	36.007	
	30.15	3:14	40.17	41.13	41. 1	
37.12	40.01	44.55	4 ن و ر 4	生みまりだ	40.00	
42.54	43.52	4 B • 511	49.00) (. • □ 4	31.09	
47.65	. 35 • 25 . 35 • 25	74.07	55 . 57	5t .71	51.75	
o2•6 ⁴	59 . 76	60.74	ಲ ∂ • ಿರ	21.9c	55.01	
13 • 7 3		66.61	€7.00	61.77	20000	
ح 10 • 4 د	50 a ∪ U	71.25	12.27	15.20	7-1-00	
29•23 75.233	70 • ≥d 76 • ≥3	11.00	10.20	1 1 2 1	74.	

DS test 6

KULL	
STEP	FUNCITON

	14	MS VALUE U	F ERHJA		
1.12	1.77	1.29	1.25	1.41	1.39
1.19	1 • 0 •	1 • 1 1,	0.35	1.46	1 • 4 7
1.54	1.43	1.47	1 • 39	1.32	1.5
1.55	1.59	1.52	1.01	1.54	1.54
1.54	1.51	1.51	1.45	1.53	1 - 4 5
1.45	1.46	1.42	1 • 40	1.57	1.37
1.30	1.34	1.30	1.51	1.51	1.32
1.56	1.51	1.20	12 13	1.28	1.20
1.20	1.52	1.34	3 - 3 - 3	1.50	1.32
1.30	1.29	1.20	1.29	1.20	1.26
1.76	1.53	1.30	1 • 40	1.30	1.28
1.23	1.28	1.52	1 - 34	1.33	1.55
1.35	1.52	1.52	1 - 31	1.33	1.30
1.32	1.30	1.31	1.52	1.30	1.31
1.23	1.51	1 - 1 -	1.09	1.23	1.50

4+ AN OF MMS= 1.35

TIME ON TARGET (SECS)						
U-16	1.10	≥•15	3.23	4.23	しゅんど	
ti∙≥ti	7.29	8.29	9.55	9.65	10.45	
11.41	11.08	12.68	15.95	14.93	15.14	
15.49	16.51	17.40	17.76	15.79	19.13	
20.87	21.00	22.89	23.90	24.65	25.13	
20.90	27.94	24.91	50 · JO	50.91	32 • 02	
33.03	34.63	35.07	36.65	37.10	30.12	
39.12	40.12	41.10	±2.16	43.18	44.71	
49.22	45.52	46.32	47.32	4 8 • 3 5	49.04	
50.32	01.34	o 2 ⋅ 02	52 • 38	53.87	54.1	
ე ს •მნ	56.12	5/.17	58 • 19	50.17	60.13	
61.19	62.22	b∠⊛ha	65.32	54.37	30.02	
65.71	bb • 73	67.7b	t 3 • 7 o	05•18	70.03	
71.82	72.67	15.13	74 • 17	75.16	76.13	
77.1b	10.25	11005	o0 • ≥ 1	31.25	62.23	

DS test 7

50.99

55.06

39.30

62.75

52.07

35.02

00.41

03.26

₹ULL					
TEP FUNCTIO) fu				
	N	AS VALUE OF	FLRADR		
2.77	2.22	1.91	1.75	1.72	1 • 45 0
1.62	1.56	1.58	1.43	1.10	1.24
1.87	2.20	2.15	2.11	2.07	2.36
2.71	2.76	2.09	2 • 01	2.58	2.54
5.60	2.63	2.50	2.52	2.44	2.46
2.44	2.41	2.36	2.53	2.30	∠ • 🖫 😘
2.35	2.33	2.32	2.30	2.27	2 €1 €
2.25	2.20	2.25	2.22	2.20	? • ≟ 4
2.38	2.39	2.38	2.40	2.38	2.47
2.34	2.32	2.29	2.20	>•35	2.52
2.33	2.30	2.28	2.20	2.2€	. 24
2.22	2.21	2.28	2 • 29	5.5%	2 • 47
2.26	2.27	2.29	2.30	5 • 5 F	2.26
2.25	2.24	2.26	2.24	2.20	6.62
2.28	2.27	2.26	3.25	z •24	2.00
HLAN OF RMS	≈ ?• 2 9				
		TIME ON TAR	(GET (SECS)	•	
0 01	บั•38	1.36	2.30	3.41	4.45
9.01	6 • 45	7.40	8 • 45	9.53	10.06
5.41	10.75	11.15	12.18	1:.19	13.54
10.78	13.69	14.00	15.09	10.74	17.74
13.60	18.49	19.04	20.10	21.07	22.14
1 8 • 0 5	24.08	25.14	26.14	27.19	27.30
25.0c	28.47	29.47	30 • 30	51.50	32.54
27.9:	34.55	34 · £3	35.15	36.13	56.35
55.54	36.43	37.07	37.00	4 ﴿ وَ وَ وَ وَ	უ ყ. 55
50•84 16 €0	41.59	42.62	43.62	43.70	43,42
40.52	45.9K	46.49	47.97	4 0.01	50.03
44.92	400,0	, 5 •		. 2 0.7	5- L No

33.07

57.53

52.05

56.20

52.27

36 • عرا

01.04

55 · 27

54.0% 53.51 52.75

96 • c)

52.24

55.64

50.85

54.25

ROLL STEP FUNCTION

•

	ĸ	MS VALUE O	F LRRUK		
2.74	2.16	1.44	1.70	?•3ઇ	2.72
- -	2.36	2.51	2.10	2.14	2 • ⊌5
2 • 55	_	· ·	1.36	0.10	3 • 8 5
1.99	1.40	1.70			
2.00	2.00	1.07	1.37	1.45	1 • "
- -	1.82	1.72	1.55	1.51	1.77
1.5	- ·	1.75	1.77	1.75	1.74
1.70	1.74	-	=	2.73	1.76
1.73	1.77	1.76	1.73	=	-
1.72	1.71	1.75	1.13	1.71	1.00
_	1.70	1.09	1.06	1.65	1.54
1.70			1.62	1.51	1.51
1.63	1.62	1 atij		1.52	1.01
1.61	1.58	1.62	1.65		_
1.59	1.59	1.57	5 ف • 1	1.56	1.05
		1.00	1.56	1.56	1.014
1.08	1.47		="	1.61	1.61
1.63	1.65	l • pl	1.62		1.49
1.60	1.59	1.62	1 • .1	1.55	1.443
1 4 0 0					

1EAN OF RYS= 1.73

	{	THE OR TAR	ROLT (SEUS)		5.06
0.04	1.04	≥ • ù 3	5.05	5.50	
4.71	5.66	6.70	7.76	.5 • 71	9.75
	11.76	12.81	13.41	15.01	14-17
10.76	16.50	17.60	18.45	19.54	19.00
15.60		22.68	22.97	23.98	24.30
20.94	21.93	20.02	23.27	> 3 . 0 4	30.02
25.93	26.99		32 • 38	34.00	34.00
31.07	31.09	51.90	=	57.03	40.03
35.02	37.10	31.38	33.04	-	45.14
41.10	42.14	43.13	44.12	45.12	
47.18	48.22	49.00	49 - 35	50.27	51.31
52.32	23.30	53.66	54.65	55.22	25.0
57.24	28.24	59.51	60 • 52	51.33	51./1
	63.00	64.03	65.02	១៦.0១	67.05
02.01		64.81	70 - 37	71.40	73.15
5 B • U 5	09.07 74.55	74.45	75.41	76.43	77.43

DS test 9

RULL STEP FUNCTION

	н	MS VALUE J	F ERROR		
2.52	1.76	1.57	9 . 40	e • 38	2.15
2.14	1.32	$1 \bullet j \varphi$	1.72	2.09	2.00
1.95	1.87	1.63	1.19	1.76	1.4.9
1.63	1 • 56	1.07	1 •0	1.53	1 • -5
1.65	1.55	1.01	1.55	1.57	1 4
1.53	1.50	1.45	1.48	1.47	1.49
1.45	1.45	1.42	1.51	1.51	1.52
1.48	1.47	1 • • •	1 • 46	1.45	1.42
1.45	1.42	1 • 4 1	1.41	1.40	1.45
1.52	1.51	. • • • 3	1.45	1.49	1.48
1.47	1.45	1.45	1.45	1.44	1.45
1.41	1.42	1 • • 1	1.40	1.40	1.40
1.44	1.49	1.45	1 . 47	1.45	1.44
1.57	1.56	1.55	1.54	1.50	1.00
1.53	1.52	1 • 52	1.51	1.55	1 • 5 5

16AN OF RMS= 1.54

		TIME ON TAR	RUECH COECH)	
0.15	0.74	1.78	2 • ∟8	្តខារ	3.53
4.78	5.80	ნ•85	7 • 8 6	7.90	5.5
9.71	10.73	11.71	12.74	13.74	14.79
19.78	10.01	17.00€	13.79	17.45	20.74
50.44	21.09	ಜಿಜ⊕ರ್*	13 - 73	34.73	3000
26.73	27.75	20.75	20.79	30•62	31.5
52.84	33.37	54 • 6 B	პა∙ ∂ნ	50.91	40.00
51.95	53.47	40.02	41.50	41.99	45.42
44.01	45.07	40.05	47.jb	40.12	40.40
4 → • 0 ರ	ou.07	51.09	52.39	53.09	54 • 05
55.11	50.12	37.15	56 • 19	59.21	oU•a1
61.22	02.23	53.25	64 • 25	55.27	nn•∈d
66.71	57.11	50 · 60	69.11	70.17	71.10
71.17	72.0b	73.08	74 - 11	75.10	70.15
77.12	73.12	74.16	a0.€00	30.00	n1.15

DS test 10

HOLL STEP FUNCTION

3111	1 040 113	•				
			KMS VALUE 0	F ERROR		
	5.24	5.14	4.26	3.57	5.44	3.11
	2.96	2.43	2.70,	3 . 3	6.48	2 • • 0
	2.44	2.35	2.27	. 13	2.19	2.11
	2.05	2.01	1.06	1.00	1.35	1 • 6
	1.35	•0	1.85	1.03	1.82	1 • ♂ 0
	1.82	1.02	1.40	1.77	1.82	1 - 7 +
	1.80	1.75	1.70	1.75	1.76	1 • 73
	1.71	1.72	1.75	1.03	1.69	1.00
	1.66	1.64	1.03	1.65	1.75	1 • 79
	1.30	1.77	1.75	1.74	1.72	1.73
	1.70	1.70	1.71	1.50	1.57	1.00
	1.70	1.00	1.70	1.00	1.65	1 (
	1.64	1.56	1.65	1.54	1.61	1.55
	1.65	1.04	1.60	1.04	1.04	1.05
	1.63	1.65	1.02	1 • ÷ 0	1.61	1 • 3
1EAN	uF R⊿S=	1.80				
			TIME ON TAR	tour CECS)	
	0.00	13.0	0.54	1.00	2 • 1 1	11 • ذ
	4.14	4.08	5.7∂	71	7.33	• i
	1.03	10.08	11.Co	12.63	15.14	14.15
	15.15	10.19	17.10	18.20	19.23	20.1
	21.23	21.27	22 ∙ 25	23.23	24.25	25.00
	25.00	26.48	21.49	28.48	20.78	23.54
	30.83	51.54	32.89	33.96	54.25	3% • 3
	36.23	30 • 58	51.55	38 . 25	39.62	4 J 🗸 , 0
	41.63	42.01	45.64	44.04	4 5 • Ü ·	47.11
	46.25	47.23	40.27	45.77	49.91	.0.7
	51.01	52.79	53.22	54. 23	55•24	កឥ∙ខ្គ
	56.63	57.55	58.68	59 • ≥p	8 4 • 1 د	51.73
	o2.63	ဗာဒ 📆 🔾 ဒီ	64.Un	b3•Vb	66.0b	97.00
	58 • 16	50.55	67.30	70 • 38	71.42	72.43
	• • • •		77 3	78 1	76.93	77.00

73.06

75.05

76.93

NS test 11

ĸ	ÜL	L	
S	ΤĒ	ρ	FUNCTION

\$ 2 G		MS VALUM O		1 57	1 4. 4
3.20	0.79	2.03	1.55	1.57	1.43
1.33	2.15	1.77	1 • 55	1.83	1 • / 1
1.71	1.35	1.75	1.75	1.74	1.03
1.65	1.59	1.57	1 • • •	1.51	1 • 3 5
1.50	1.45	1.45	1.45	1.45	1.45
1.42	1.45	1.45	1.57	1.59	1.37
1.38	1.37	1.35	1.53	1.34	1.37
1.34	1.55	1.54	1.36	1.55	1 + 51
1.31	1.27	1.51	1.29	1.2ខ	1 - 50
1.20	1.27	1.37	1.35	1.57	1.55
1.35	1.56	1.55	1 • 4	1.33	1.34
1.33	1.54	1.32	1.31	1.35	1.31
1.32	1.59	1.50	1.29	1.20	1 - 2 =
1.24	1.28	1.21	1.27	1.20	1.25
1.25	1.05	1.25	1.28	1.2 "	1.27

A CAN

TIME ON TARGET (SEES)						
0.13	1.13	2.11	3.18	4.25	3.13	
u.16	6.43	7.36	3.35	4.30	10.41	
11.38	11.54	12.61	13.55	14.68	15.71	
16.05	17.01	13.05	15.70	19.59	30.00	
21.52	22.62	63.64	24.39	25.22	2000	
20.92	27.39	29.00	30.02	51.04	30.00	
33.00	34.05	35.66	35.69	37.10	30.13	
39.14	39.50	40.48	41 • 73	42.52	43.52	
44.53	45.59	40.05	45 · 82	47.91	4×.51	
49.93	50.70	೨೩.∀೯	51.84	52.34	53.35	
54.92	55.88	56.96	57.95	5 · • • • 7	5, 2 , 54	
20.27	61.56	52.52	65.33	4 • 37	55 • c5	
55.57	57.40	68.41	54.42	70.45	11.41	
72.50	73.55	74.58	75 . 50	76.55	17.06	
78.50	79.60	où•⊎5	ಕ0 • 80	81.80	82.76	

DS test 12

ROLL STEP FUNCTION

	t	RMS VALUE U	F ERROR		
2.72	1 • 7 b	1.57	1 • +7	1.57	1.20
1.1	1.24	1.57	1.36	1.40	1.55
1.41	1.29	1.54	1.41	1.58	1.00
1.50	1.51	1.51	1 + + 1	1.44	1 • • 7
1.40	1.36	1.38	1.37	1.57	1.55
1.34	1.55	1.38	1.57	1.3 ♂	1.33
1.45	1.45	1 • 4 1	1.42	1.45	1.46
1.43	1.45	1.44	1 • 4 4	1.41	1 • 4 4
1 - 41	1.53	1.46	1 • +6	1.45	1 - 44
1.49	1.50	1.58	1.48	1.45	1 • 4 7
1.47	1 • 4 7	1.4.	1 • 44	1.45	1 • 4 3
1.46	1 • 47	1.47	1 • 4 4	1.45	1 . +4
1.43	1.47	1 - 4 4	1.45	1.46	1 • • •
1.44	1.43	1.45	1.42	1 • 4 1	1.40
1.41	1.39	1.40	1.39	1.38	1.57

MEAN OF HMS= 1.43

TIME ON TARGET (SECS)						
0.20	1.20	2.23	3 • 25	4.26	A . 380	
S • 25	7.03	7 • 0 Ü	8 • ⊃€	14 o to 16	10.00	
11.10	12.09	13.04	14.04	14.50	1 . 51	
16.33	17.38	18.40	19.35	20.43	21.40	
22.43	23.44	24.43	85.00	20.45	-1.0	
28.52	29.43	20.75	30 • 33	51.79	326+3	
33.03	ડ ડ•⇒5	34.70	33.12	30.20	57. 2	
3 4.18	39.22	40.30	41.29	42.2€	43.23	
44.35	45.51	45.61	7د • 45	41.59	4 2 4 2 4	
49.33	49.74	50.81	51 • 55	52.52	500 🕶 🖖	
38.FC	55.88	30.91	57.52	50.91	11.00	
⊳∂. 35		62.17	63 • 32	54.23	55.24	
66.28	05.78	67.57	58 € 58	67.50	70.00	
11.66	72.6 7	75.60	74 • 75	74.75	7 • 77	
77.77	7 - 77	7,.75	×0 • 31	52.55	~2•11	

ns test 13

ROLL			
STEP	FUNC	ī	10%

	ĸ	MS VALUE U	と かいとなって		_
1.92	3 • 0 ·	2.04	5.54	1.92	1 • " 7
1.70	1.04	1.65	1.53	1.56	1.7
1.79	1.50	1.74	1.73	1.56	1 • 5
1.65	1.57	1.62	1.55	1.53	€ ، ا
1.55	1.01	1.58	1.07	1.57	1.0
1.50	1.50	1.43	1.46	1.44	1.47
1.45	1.46	1.44	1.42	1.42	1.43
1.48	1.41	1.59	1.55	1.40	1.34
1.46	1.41	1.40	1.57	1.40	1.4
- ·	1.46	1.45	1.45	1.40	1.45
1 - 4 9	1.45	1.46	1.45	1.45	1.42
1 • 4 4	1.42	1.42	1.40	1.41	1.54
1.46	·	1.44	1 • 4 4	1.45	1.42
1.58	1.45	1.01	1 • >0	1.50	1.46
1.4.	1.52	1.47	1.47	1.47	1.47
1.4	1 • 4 ti	1.47	1 - 7 /	. • · ·	~ •

1_AV JF KMS= 1.44

TIME OF TANGET (SECS)							
5.19	0.48	1.41	3 J	3.41	4.03		
5.55	5.54	7.51	2 • 20	9.50	10.06		
11.01	11.48	12.51	13.55	14.56	15.55		
10.60	17.58	18.51	18.79	19.88	2000		
21.23	22.17	23.22	24.15	25.23	20.20		
21.27	28.24	29.24	30 - 24	31.53	31.70		
32.70	33.73	34.77	35.74	36.60	31.77		
	37.42	47.54	41.95	44.027	45.21		
58.80	43.46	40.27	47.26	40.21	44.47		
44.22	50.48	51.14	52.12	53.15	54.19		
4 1.46		25.57	57. 17	J ⁽¹ • 5 b	99.64		
55.23	20.21	35.07 3.007	55.11	54.65	55.71		
60.62	5 1.06		65.17	21.37	70.00		
30.77	67.02	97•91	74.11	7: 13	75.15		
72.02	72.11	73.00		51.25	, 2		
77.17	78.18	19.20	40 - 32	31020	./. •		

DS test 14

⋅₹	ソレレ	
S	TEP	FUNCTION

		KMS VALUE D	IF ERKUR		
1.94	1.77	1.76	1.00	1.57	1.70
1.73	1.52	1.45	1 • 36	1.42	1 • 4 0
1.51	1.15	1.51	1.27	1.29	1.50
1.30	1.36	1.55	1.25	1.51	1.26
1.27	1.21	1.19	1.13	1.20	1.23
1.29	1.29	1.20	$1 \cdot 29$	1.27	1.29
1.26	1.31	1.42	1 • 4 3	1.41	1 • 5 ₺
1.57	1.38	1.57	1 • 4 0	1.34	1.45
1.34	1.55	1.55	1.30	1.32	1.50
1.33	1.33	1.52	1.29	1.31	1.3
1.27	1.29	1.27	1.28	1.29	1.00
1.26	1.25	1.27	1.36	1.34	1.35
1.37	1.35	1.35	1 • 55	1.34	1 • 5 •
1.33	1.33	1.58	1 • 36	1.37	1.55
1.50	1.35	1.54	1 • 54	1.59	1.58
4EAN OF KMS=					
		TIME UN TAR			
0.25	1.28	2.30	2.51	5.31	4 • 56
5.36	5 • 41	7 • 4 û	3.11	フ・4 6	10.46
11.46	12.46	13.05	14.04	1:.54	1
16.89	17.91	10.00	13.71	20.90	31.53
22.97	23.98	20.03	20.03	27.05	. 3 • 0 €
25.37	27.34	30.38	30.70	31.75	32.73
3 3.7 3	34 • 68	54 •88	35.92	36.93	01.51
১৪•∄৪	39 • 98	40.99	41.99	43.02	44.03
45.07	40.07	47.07	48.12	47.15	36.12
5û•71	51.49	52.47	53.52	54.52	J7 • 17
95 • 55	57.5H	58.55	59.61	50.67	01.rb
62.63	23.70	64.50	04 • 30	55.88 71.0	56.71
7 0 € ت	50.06	69.11	70.10	71.05	72.15
15.17	74.10	74.43	15.40	70.4t	77.47
7n.50	79.52	80.55	81 - 35	81.83	ತΩಿ∗ಗ≎

Al test 1

ROLL		
STEP	FUNCT	10.4

	h	MS VALUE 0	r		
2.24	1.95	1.12	1.25	1.22	1.21
	1.11	1 •,11	1.17	1.30	1.53
1-33		1.32	1.18	1.1b	1 - 25
1.35	1-11	1.31	1.50	1.33	1.32
1.42	1.41	-	1.50	1.20	1.27
1.35	1.29	1.54		1.34	1.55
1.50	1.23	1.54	1.34		1.50
1.33	1.31	1.32	1.29	1.30	-
1.28	1.28	1.26	1.25	1.25	1.23
1.25	1.24	1.24	1.22	1.23	1.21
1.23	1.18	1.20	1.19	1.20	1.24
1.19	1.19	1.19	1.17	1.18	1.10
	1.16	1.21	1.22	1.20	1.22
1.17	_	1.26	1.19	1.24	1.25
1.19	1.18		1.25	1.25	1.39
1.24	1.26	1.24		1.22	1.01
1.25	1.22	1.23	1.22	7.0 - 5	

4EAN OF RMS= 1.25

		TIME ON TAR	GET (SECS)		
0.03	0.88	1.80	2.50	3.33	4 • 7 4
5.91	6.96	7.94	8.40	8.69	9.71
	11.74	12.73	13.7=	14.75	10.68
10.74	16.49	17.53	18.50	14.54	20.55
10.66		23.57	24.62	20.59	26.650
21.53	22.59		29 • 23	36.32	51.76
27.60	28.64	25.74	35.32	36.32	37.32
32.34	33.32	34.33	-	42.37	43.48
38 .3 8	59.54	40.37	41.39	43.41	47.37
44.43	45.43	45.44	47.47		25.51
50.47	51.49	52.49	53.48	54.53	
20.45	57.51	50 • 5b	აშ∙ ა7	50 . 57	51.54
62.61	63.50	53.45	64 - 55	65.32	bé∙ခံ
67.33	68.33	69.40	70.40	7 U • 3 6	/1.00
72.02	73.05	74.05	75.03	7600	77 . Ju
78.08	79.08	80.12	81.15	52.15	83.14

;; test 2

	OLL	
š	TEP	FUNCTION

		ara arta da O	F ERHJK		
			1.07	1.65	1.70
2.52	1.58	1.83		1.25	1.24
1.40	1.30	1.29	1.27	1.57	1.45
1.23	1.23	1.11	1.52		1.01
1.51	1.47	1.46	1.44	1.47	
1.54	1.56	1.51	1.54	1.40	$1 \cdot 0 1$
	1.44	1.44	1.41	1.43	1.+0
1.47	1.53	1.54	1.55	1.54	1.65
1.40		1.49	1.49	1.45	1.45
1.53	1.52		1.46	1.45	1.45
1.46	1.45	1.46	1.47	1.43	1.45
1.46	1.45	1.44		1.42	1.41
1.47	1.45	1.41	1.42	1.41	1.40
1.41	1.41	1.40	1.40		1.57
1.39	1.58	1.38	1 - 59	1.38	
	1.36	1.35	1.56	1.54	1.55
1.50	1.34	1.34	1.51	1.32	1 • 54
1.33	1004	•••			
TEAN OF RMS=	1.43				

		TIME ON TAR	GET (SECS)		
	0 (3	0.71	1.58	2.75	3.73
0.06	0.39	6.76	7.81	3.31	~ 5.1
4.73	5.74			15.30	13.49
10.81	11.85	12.81	12.91	15.50	13.75
14.53	15.53	16.54	17.54		29.97
19.43	20.46	21.44	22 • +7	23.50	
25.52	26.52	27.55	28.50	24.57	50.53
- ·	31.75	32.22	33.23	34.24	35.22
31.54		38.27	39.27	40.20	41.31
36.30	57.27	44.51	44.72	44.96	45.0°°
42.52	43.51	•	50.04	51.03	51.11
40.96	47.97	48.96	-	56.11	57.11
52.03	53.U8	54.09	55.07	62.18	55.17
58.12	54.12	60.17	61.18		65.18
64.20	65.11	á5.17	66.21	67.22	
- · ·	70.22	71.22	12.23	73.28	74.27
69.21	76.28	77.31	78.50	79.31	79.50

test 3 MK

4 JLL		
STEP	FUNCT	LON

			RMS VALUE OF	ERROR		
	2.24	1.37	1.71	1.57	1.22	$1 \cdot 20$
	1.57	1.67	1,66	1.53	1.54	1.54
	1.40	1.46	1.50	1 • 33	1.29	1.34
	1.55	1.54	1.23	1.52	1.27	1.34
	1.51	1.54	1.45	1.49	1.45	1.43
	1.57	1.68	1.67	1.65	1.02	1.54
	1.63	1.60	1.59	1.57	1.55	1.54
	1.54	1.55	1.62	1.64	1.59	1.51
	1.58	1.57	1.53	1.55	$1 \bullet imes \epsilon$	1.53
	1.55	1.54	1.52	1 • 50	1.50	1.43
	1.49	1.49	1.48	1.40	1.47	1.40
	1.40	1.49	1.48	1.46	1.46	1.45
	1.46	1.44	1.44	1.44	1.42	1.44
	1.43	1.46	1.46	1.45	1.45	1.45
	1.45	1.44	1.42	1.44	1.40	1.40
1EAN	OF RMS=	1.47				

		TIME ON TAI	RGET (SECS))	
0.05	0.71	1.00	2.71	3.70	4.71
5.73	5.69	0.16	7.19	0•1É	9.001
10.18	11.19	12.19	13.21	14.21	15.20
16.26	17.21	18.26	19.23	20.20	31.00
21.02	21.73	22.78	23.75	24.77	25.42
25.63	25.88	26.83	27.10	23.89	20.92
3u•92	31.94	32.97	55.94	34.95	ა ნ•98
30.98	57.74	37.78	38 • 53	39∙58	40.40
41.58	42.58	43.62	44.653	45.2%	45.37
46.86	47.91	43•3€	47.57	50.91	51.92
52.49	32.68	53.91	54 - 37	ob.93	50.12
56.92	57.84	50 · 87	ລ9•ດ7	50.93	51.57
62.95	63.90	64.95	65.92	56.91	57.92
63.96	69.37	69.70	70.72	71.71	72.71
73.75	74.73	75.70	75.72	77.7c	18.77

MK test 4

ROLL STEP FUNCTION

		RMS VALUE O	F ERROR		
2.77	1.30	1.45	1.25	1.22	1.29
1.12	1.25	1 - 05	1.12	1.1€	1.02
0.98	0.94	0.45	1 • 04	1 • 0 4	1.08
0.99	1.03	1.09	1.41	1.04	1.07
1.07	1.05	1.05	1.35	0.97	1.07
1.17	1.15	1.15	1.21	1.23	1 - 4
1.21	1.26	1.22	1.21	1.20	1 • 1 6
1.10	1.17	1.18	1.15	1.20	1.19
1.20	1.17	1.18	1.18	1.10	1.10
1.14	1.15	1.17	1 • 23	1.20	1.25
1.27	1.25	1.25	1.25	1.23	1.24
1.23	1.24	1.28	1.29	1.20	1.27
1.28	1.27	1.20	1.20	1.27	1.27
1.24	1.26	1.25	1.26	1.36	1.30
1.34	1.35	1.54	1.33	1 • 4 0	1.40
1EAN OF RMS=	1.19				
		TIME JN TAR	GET (SECS)	•	
0.01	0.70	1.75	2.71	5.73	4.70
5•76	6.83	7.79	- • 19	9.73	10.7 -
11.81	12.81	13.84	14.61	15.35	15.35
17.86					
	18.58	19.91	20.35	21.∃2	22.00
23.94	18•68 24•94	19.91 25.94	20 • 35 26 • 97	21.32 27.30	
23•94 25•98	-				22.00
	24.94	25.94	26.97	27.90	22•10 23•58
28.98	24.94 29.94	25.94 30.95	26.97 31.45	27.90 31.77	22.10 23.58 32.78
25•98 55•79 59•85 44•97	24.94 29.94 54.74	25.94 30.95 35.79	26.97 51.45 56.78	27.90 31.77 37.54	22.40 23.58 32.78 55.79
25•98 55•79 59•85	24.94 29.94 54.74 40.87	25.94 30.95 35.79 41.83	26.97 51.48 36.78 42.57	27.90 31.77 37.84 43.12	22.40 28.58 32.78 55.79 45.97
25•98 55•79 59•85 44•97	24.94 29.94 54.74 40.87 46.01	25.94 30.95 35.79 41.83 47.61	26.97 31.45 36.78 42.57 48.01 53.39 59.12	27.90 31.77 37.84 43.12 48.98	20.90 28.58 32.78 35.79 45.97 20.04
25.98 33.79 39.88 44.97 51.02 56.06 62.11	24.94 29.94 54.74 40.87 46.01 52.08 57.11 62.98	25.94 30.95 35.79 41.83 47.61 55.06	26.97 51.45 56.78 42.57 48.01 53.39	27.96 31.77 37.84 43.12 48.98 54.02	22.70 23.58 32.78 35.79 43.97 30.04 55.03 51.12
25.98 33.79 39.88 44.97 51.02 56.06	24.94 29.94 54.74 40.87 46.01 52.08 57.11	25.94 30.95 35.79 41.83 47.61 53.06 58.13	26.97 31.45 36.78 42.57 48.01 53.39 59.12	27.96 31.77 37.84 43.12 48.98 54.02 50.11	22.70 23.58 32.78 55.79 45.97 50.04 55.03
25.98 33.79 39.88 44.97 51.02 56.06 62.11	24.94 29.94 54.74 40.87 46.01 52.08 57.11 62.98	25.94 30.95 35.79 41.83 47.61 53.06 58.13 53.07	26.97 31.45 36.78 42.37 48.01 53.39 59.12 64.36	27.96 31.77 37.84 43.12 48.98 54.02 50.11 65.05	22.70 23.58 32.78 35.79 43.97 30.04 55.03 51.12

MK test 5

ROLL	
STEP	FUNCTION

	R	MS VALUE O	F ERRIK		
0.00	1.37	1.57	1 • 25	1.37	1.11
1.05	1.11	0.91	1.17	U • 9 5	0 - ೮೬
1.11	1.03	36.0	ۇز • ن	1.01	1.02
	1.14	1.24	1.23	1.15	1.20
1.05	1.27	1.28	1 • 24	1.27	1.27
1.24		1.22	1.22	1.22	1.15
1.25	1.23	1.19	1.18	1.20	1.25
1.19	1.17		1.10	1.23	1.30
1.25	1.24	1.25		1.27	1.26
1.27	1.29	1.27	1 • 25		1.25
1.25	1.25	1.23	1 • 25	1.25	
1.22	1.23	1.25	1.24	1.24	1.04
1.24	1.25	1.26	1.27	1.24	1.25
1.26	1.25	1.25	1.24	1 • 2 4	1.23
1.23	1.23	1.23	1:4	1.23	1.23
1.22	1.22	1.23	1.23	1.21	1 • 21

		TIME ON TAR	GET (SECC)		
0.29	1.34	2.34	3.33	4.54	3・59
6.34	7.41	8 - 35	9.41	10.41	11.44
	13.46	14.41	15.48	16.45	17.40
12.41		19.48	20 • 40	21.52	22.55
18.49	19.04	24.49	23.40	26.47	27.45
23.28	23.45	-	31 • 52	32.55	33.53
28.53	29.53	30.48		33.32	33.73
54.54	35.60	36.53	37.54	43.74	43.17
39.65	40.09	41.75	42.73		49.23
44.22	45.26	46.26	47 • 27	48.51	
50.31	51.29	52.33	5 3 • 32	54.54	55.54
56.37	57.36	58.34	၁8 🔸 မ 🚶	50.59	60.04
51.49	61.58	b2.57	25.21	54.01	55.00
66.62	67.65	ob •63	5c • vc	70.70	71.57
12.70	72.72	73.07	14 - 50	75.66	75.11
77.68	78.71	79.68	80.76	81.72	32.17

Mr. test 6

4 OLL		
STEP	FUNCT	ION

1.96 1.53 1.20 1.11 1.12 1.07 1.21 1.17 1.20 1.19 1.16 1.19 1.16 1.19 1.16	2.10 1.36 1.15 1.19 1.13 1.11 1.18 1.17 1.20 1.17 1.16 1.20 1.19 1.18	RMS VALUE OF 1.70 1.29 1.07 1.16 1.15 1.15 1.21 1.15 1.20 1.20 1.20 1.16 1.19 1.20 1.15 1.20	F ERKOR 1.07 1.27 1.08 1.14 1.11 1.00 1.21 1.17 1.19 1.16 1.14 1.17 1.20 1.18 1.22	1.11 1.26 1.10 1.15 1.15 1.20 1.21 1.21 1.17 1.21 1.17	1.26 1.25 1.25 1.16 1.20 1.20 1.27 1.20 1.18 1.14 1.22 1.20 1.13
AN UF RMS=	1.18	TIME UN TA	RULT (SECS)	1. 3 fs

4 L A

MK test 7

ROLL STEP FUNCTION

		RMS VALUE	OF ERRUR		
2.98	2.48	1.82	1.95	1.05	1.00
1.68	1.42	1.38	0.93	1.84	1.98
1.92	2.02	2/13	2.06	2.00	2.03
1.97	1.91	1.8E	1.36	1.81	1.03
1.77	1.74	1.70	1.71	1.04	1.63
1.62.	1.61	1.56	1.57	1.56	1.55
1.65	1.68	1.69	1.56	1.64	1.65
1.62	1.59	1.59	1.00	1.70	1.00
1.79	1.79	1.77	1.76	1.73	1.74
1.71	1.72	1.71	1.71	1.63	1.68
1.65	1.60	1.75	1.77	1.76	1.75
1.77	1.75	1.75	1.74	1.73	1.71
1.75	1.78	1.77	1.77	1.76	1.74
1.75	1.75	1.74	1.75	1.73	1.74
1.74	1.73	1.72	1.71	1.70	1.69

		TIME ON TA	RGET (SECS)	
0.01	0.03	0.76	1.31	2.01	3.31
4.60	5.80	6.85	7.53	7.81	7.01
8 • 74	9.28	9.24	9.71	10.73	11.78
12.78	13.78	14.78	15.81	10.79	17.50
18.80	19.84	20.85	21.57	22.83	23.37
24.90	25.88	26.93	27.92	29.89	29.90
30.14	30.12	30.95	31.53	32.52	33.52
34.50	35.53	36.54	37.43	37.47	37.44
38.08	39.08	40.10	41.12	42.14	43.19
44.12	45.12	40.12	47.10	43.10	40.21
50.17	50.97	50.98	51.36	52.34	· -
53.33	53.98	55 • Qa	56.08	57.07	o3 • 32
58.58	58.59	59.38	60 • 38	51.37	១៩៩០។
62.37	63.35	64.40	f [+ 41	=	J2+37
67.10	68.12	69.11	73.68	55.87 71.13	56.00 70.15

MK test 8

くりにに	
STEP	FUNCTION

	•	MS VALUE O	F ERRUR		
3.10	2.09	1.02	1.57	2.45	2.05
2.49	2.29	2.31	2.25	2.15	2.10
2.06	1.97	2.05	2 • 46	2.00	1.94
	1.36	1.05	1.80	1.90	1.36
1.92	1.85	1.79	1.77	1.71	1.73
1.85	1.05	1.06	1.65	1.66	1.50
1.72	_	1.74	1.75	1.71	1.87
1.79	1.76	1.81	1.31	1.77	1.17
1.82	1.85	1.76	1.70	1.72	1.71
1.79	1.75	1.80	1.81	1.79	1.79
1.09	1.65		-	1.92	1.33
1.76	1.76	1.98	1.98		1.32
1.87	1.8ó	1.05	1.83	1.82	
1.81	1.50	1.79	1.70	1.80	1.32
	1.80	1.81	1.79	1.79	1.77
1.81		1.75	1.75	1.74	1.75
1.77	1.76	7.01.7	****	• • •	

		TIME ON TAR	IGET (SECS)	l .	
0.04	0.45	1.33	2 • 38	2.61	2.39
3.49	4.23	4.28	4.40	tı • Û Û	J • 4 1
7.98	9.01	3.45	1.70	10.75	11.75
12.75	13.80	14.77	15.81	15.84	15.06
17.70	18.70	14.71	20.53	21.69	12.72
25.77	24.74	25.18	25.70	27.77	23.72
28.78	29.12	29.03	30.37	31.32	31.5
32.53	33.53	34.54	30.59	36.09	30.007
37.84	38.88	39.92	43.82	41.52	42.493
43.92	44.93	45.04	40.34	45.34	47.37
40.37	49.38	47.42	49.00	50.57	51.72
52.72	53.72	54.76	55 • 7 <i>3</i>	20.76	57.17
58.78	59.76	UJ.77	51. 32	52.23	62.27
55.30	64.30	05.30	υ δ • 33	57.25	50 • 5 5
69.32	70.36	71.58	72.57	75.40	74.41

MK test 10

ROLL	
SIEP	FUNCTION

	R	MS VALUE O	F ERROR		
2.77	2.49	2.14	1.75	1.57	$1 \cdot 50$
1.63	1.24	1.39	1.45	1.30	1-24
1.63	1.68	1.52	1.62	1.75	1 • 7 >
1.77	1.65	1.68	1.76	1.62	1.50
1.56	1.52	1.50	1.43	1.47	1.43
1.48	1.43	1.48	1.51	1.47	1 • 4 7
1.47	1.47	1.44	1.43	1.42	1.41
1.58	1.40	1.38	1.40	1.33	1.34
1.36	1.45	1.47	1.45	1.45	1.43
1.41	1.45	1.40	1.59	1.41	1.5%
1.38	1.57	1.32	1.50	1.36	1 - 41
1.40	1.39	1.40	1.39	1.50	1.49
1.48	1-47	1.47	1 • 40	1.45	1.46
1.44	1.44	1.43	1.44	1.45	1.42
1.41	1.42	1.46	1.45	1.44	1.43

TIME ON TARGET (SECS)						
0.14	0.39	1.40	2.43	3.13	4.13	
5.13	6.21	7.20	5 • 1 9	J.16	10.25	
10.61	11.40	12.40	13.33	13.51	14.01	
15.51	16.54	17.54	18.09	19.55	20.55	
21.60	22.00	25.02	24 • 50	25.63	20.06 4	
27.62	28.65	28.39	24 - 93	27.67	30.00	
31.90	32.88	33.72	34.53	35.92	うちゅいき	
37.92	38•92	39.95	40.93	41.59	42.48	
44.01	44.29	44.76	40.77	46.79	47.73	
48.78	47.82	50.84	5 1 • 38	58.8c	J3.84	
54.82	55 • 88	56.34	o7 • 8∃	58.50	53.63	
59.31	60.33	61.32	€2.35	52.40	to 2 . 46	
64.40	65.43	66.47	67.43	o3.42	39.45	
70.48	71.27	71.77	12 • 7 b	73.81	74.77	
75.81	76.70	77.01	78.01	75.38	د لا • لا ۍ	

1.1K test 11 R JLL STEP FUNCTION RMS VALUE OF ERADY 0.00 3.74 1.37 1.11 1.11 1.11 0.94 0.96 1.54 1.40 1.27 1.24 1.27 1.26 1.22 1 • Ú iš 1.59 1.59 1.47 1.51 1.43 1.55 1.47 1.44 1.43 1.40 1.45 1.57 1.43 1.47 1.45 1.51 1.47 1.43 1.42 1.40 1.40 1.38 1.35 1.57 1.58 1.33 1.34 1.33 1.35 1.33 1.23 1.30 1.39 1.57 1.55 1.39 1.40 1.38 1.38 1.36 1.30 1.35 1.35 1.33 1.34 1.54 1.50 1.31 1.31 1.32 1.51 1.55 1.57 1.38 1.34 1.42 1.45 1.41 1.41 1.40 1.59 1.41 1.38 1.57 1.30 1.57 1.37 1.37 1.35 1.54 1.33 1.54 1.5 MEAN OF RMS= 1.58 TIME ON TARGET (SECS) 2.99 0.98 1.98 3.93 5.01 6.04 7.04 8.06 9.11 9.34 1.95 10.25 12.99 11.93 14.01 15.05 15.05 15.53 16.54 17.60 18.64 19.63 20.62 21.60 22.65 23.69 24.64 27.30 25 . 57 20.65 30.55 31.37 27.85 28.80 29.88 32.37 33.90 54.94 35.93 36.92 37.94 30.74

41.99

47.05

52.22

57.77

63.57

67.92

74.01

30.05

42.77

43.07

53.24

50.77

63.82

68.32

74.75

81.03

45.02

43.54

54.27

59.77

64.82

59.93

75.90

82.0L

44.01

49.19

50.77

64.000

70.17

77.00

43.02

40.02

45.02

50.21

55.71

61.76

65.93

72.00

78.08

40.97

46.05

51.22

56.72

62.77

66.90

12.98

79.03

MF. test 12

4 OLL	
STEP	FUNCTION

	r	KMS VALUE O	F EKROK -		
1.92	2.25	1.25	0.70	1.32	1 • .41
1.26	1.25	1,11	1.17	1.25	1.07
1.54	1.57	1.52	1.47	1.43	1.49
1.40	1.39	1.42	1.32	1.50	1.01
1.46	1.48	1-48	1.50	1.42	1.44
1.31	1.40	1.49	1.05	1.54	1.52
1.50	1-48	1.45	1.46	1.40	1.47
1.43	1.41	1.43	1.41	1.40	1.43
1.53	1.50	1.48	1 • 50	1.49	1.43
1.46	1.46	1.46	1.47	1.46	1.44
1.44	1.47	1.48	1.47	1.48	1.45
1.48	1.49	1.48	1.44	1.47	1.47
1.47	1.45	1.43	1.41	1.47	1.45
1.44	1.44	1-45	1.45	1.42	1.42
1.40	1.59	1.40	1.38	1.54	1.40

TIME ON TARGET (SECS)						
0.20	1.26	2.28	3 • 25	4.25	5.29	
5•2¢	7.29	8 • 26	9.31	10.31	11.31	
11.40	11.70	12.70	13.73	14.13	15.70	
16.70	17.74	13.80	.>.75	20.75	20.80	
21.32	22.35	23.28	24 - 30	25.33	25.34	
27.52	28.40	28 • 68	2ರ•೧୭	29.73	30.74	
51.74	52.75	33.75	34 • 77	35.77	32.79	
37.78	38.78	3 9•82	40.00	41.83	42.43	
42.81	43.81	44.01	45.02	40.79	47.84	
48.82	49.82	50•84	51 • 87	52.88	53.89	
54.89	55.43	50.42	56 • 43	57.42	57.68	
58.52	59.49	60.46	51.54	62.55	53.55	
64.53	65 . 58	66.57	u1•5V	57.65	65.53	
69.57	70.66	71.65	72 • 63	13.66	74.65	
75.67	76.68	77.70	78 • 58	79.76	34.72	

区 test 13

ĸ	JL	L			
3	7:	Ρ	FUNC	Į	ION

	સ	MS VALUE 0	F ERROR		
0 • 0 0	1.58	0.91	1.57	1.52	1.32
0.34	1.04	0.91	1.11	1.07	1.62
	1.07	ぴ・サコ	1 • 04	1.10	1.20
18.0	=	1.21	1.23	1.20	1.16
1-17	1.17	1.17	1.19	1.19	1.15
1.22	1.21	1.13	1.15	1.14	1.15
1.17	1.20	1.17	1.15	1.14	1.15
1.10	1.16		1.14	1.1:	1.14
1.10	1.15	1.18	_	1.1	1.1.
1.12	1.13	1.19	1.13		1.22
1.15	1.18	1.24	1.24	1.25	
1.22	1.19	1.21	1.26	1.22	1.19
1.20	1.20	1.19	1.17	1.20	1.19
1.21	1.21	1.20	1.20	1.10	$1 \cdot 1 \circ$
1.17	1.17	1.17	1.17	1.17	1.10
_	1.19	1.15	1.17	1.20	1.20
1.18	1.1	1010	-		

4EAN OF KMS= 1-17

		TIME ON TAR	GET (SECS))	
0.36	1.36	2.39	3 - 40	4 • 4 4	5.49
6 • 4 ⊃	7.43	8.48	9.00	13.46	11.44
12.46	13.53	14.44	15.54	15.55	15.50
17.5d	18.58	18.63	19.51	29.51	21.440
22.33	23.37	24.35	25 • 38	26.35	27.52
	29.59	30.40	31.42	52.30	55.45
23.42	34.70	35.77	36.73	37.74	20.74
33.72	40.77	41.82	42.77	43.33	44.52
39.74		47.88	48.30	48.30	4 3 a 13°.
45.80	46.82	52.01	23 • 62	54.03	55.87
50.87	51.88	5±•01	59.11	56.11	£1.11
56.06	57.06	64.15	65.13	50.17	.7.01
62.12	63.10	69.07	70.00	71.11	72.37
67.03	68 • 06	75.08	75 • 17	77.17	73.11
13.12	74.08	81.16	81.00	s2.13	53.25
77.10	80.17	O T + T P	01.00	324.0	

FK test 14

ROLL STEP FUNCTION

1.54	1.78	0.91	1 = 2 =	1.45	1.2
1.53	1.57	1.44	35	1.35	1.3
1.23	1.26	1.22	1 • 21	1.21	1.3
1.20	1.14	1.14	1.19	1.16	1.1
1.15	1.15	1.09	1.15	1.11	1 • 1
1.09	1.11	1.15	1.15	1.10	1.0
1.07	1.05	1.07	1.16	1.07	1.1
1.07	1.16	1.20	1.15	1.16	1.1
1.18	1.16	1.17	1.16	1.15	1.1
1.15	1.13	1.14	1.15	1.12	1.1
1.17	1.18	1.17	1.20	1.22	1.3
1.20	1.20	1.21	1.19	1.19	1.1
1.13	1.16	1.10	1.18	1.16	1.1
1.17	1.19	1.22	1.21	1.21	
1.19	1.19	1.18	1.19	1.15	i • 1

4 5

TIME ON TARGET (SECS)							
û•20	1.25	2.19	3.25	4.20	5.25		
6.08	6.58	7.56	8.43	9.43	10.43		
11.45	12.43	13.46	14.45	15.46	16.43		
17.49	18.48	19.54	20.53	21.50	22.54		
23.53	24.57	25.55	26.53	27.50	23.29		
24.55	30.50	31.59	32 • u3	53.62	34.60		
35.62	36.62	57.50	33 . p7	57.59	40.55		
41.50	42.12	42.66	45 • 65	44.64	45.72		
46.71	47.69	48.71	49.73	5U•74	31./4		
52.81	53.79	54.79	55 • 79	ან• 7 9	J7.43		
ემ • 0 3	59.03	50.04	60.33	60.82	1.35		
62.03	53.86	64.43	บวิจาร	56 .9 0	5 7. → Ū		
68.91	69.91	70.95	71.95	12.97	75.92		
74.97	75•58	76.25	77 • 25	18.23	10.21		
80.26	31.25	42.26	კ პ∙∠6	34.27	35.31		

MR test 1

ROLL STEP FUNCTION

	RMS	VALUE 0	· 1. 118		
1.94	1. 13	1.70	1 • 47	1.31	1.28
1.19	1 + 1 1	1.20	1.11	1.16	i • ii o
1.15	1.63	1.07	1.17	1.14	1.17
1.25	1.26	1.19	1 • - 1	1.23	1.15
1.19	1.41	1.13	1.15	1.15	1.13
1.18	1.31	1.57	1 • 40	1.52	1.44
1.45	1.45	1.41	1.41	1.57	1.59
1.39	1.57	1.33	1.50	1.34	1.45
1.34	1.55	1.50	1 • 38	1.38	1.56
1.35	1.42	1.40	1 • 46	1.47	1.45
1.45	1.44	1.40	1.45	1.42	1.43
1.53	1.40	1.31	1.40	1.50	1.39
1.37	1.39	1.45	1 • 47	1.40	1.46
1.45	1-46	1.45	1.40	1.42	1.43
1.43	1.48	1.48	1.40	1.46	1.45

464% OF KMS= 1.34

TIAL ON TARBLE (SECS)						
0.71	0.74	1.39	2.53	5.40	4 • 4 0	
v.45	6.48	7.40	B • 4명	0.51	10.00	
11.54	12.54	13.59	14 • 60	14.71	14.74	
10.56	16.71	17.69	13.73	19.75	29.78	
21.75	22.50	23.70	242	25.62	14.€00	
27.63	27.63	27.00	28 • ≈ 7	29.03	2 +• ⊍ 0	
29.73	50.75	31.70	32 • BB	35.71	5-78	
53.32	36.52	57.82	38 . 83	37.90	4 U . 10	
41.89	42.69	40.27	43.28	44.13	45.16	
46.17	46.37	45.50	40 • 42	47.98	48.43	
43.97	50.99	ა 1. 98	53.62	54.01	್ರಿ-ಚಿಡ	
ns • 04	57.07	53.04	58.03	5 d • 93	34.42	
60.92	61.08	61.75	61 • 8 b	62.90	55.10	
24.90	55.93	55.95	57.93	5 s • 9 7	4,3643	
70.70	70.72	74.53	71.37	72.95	7:.45	

MM test 2

ROLL STEP FUNCTION

	ix	MS VALUE O	IF TRROR		
2.47	1.94	1.44	1 . 47	1.51	1.43
1.33	1.36	1 -17	1 • 27	1.20	1 • 1.0
1.54	1.48	1.4)	1.42	1.57	1.50
1.39	1.49	1.47	1•48	1.44	1.41
1.39.	1.38	1.38	1.36	1.5%	1. 15
1.30	1.30	1.48	1.01	1.51	1+8
1.45	1.46	1.55	1.55	1.51	1 - 7.5
1.53	1.51	1.52	1.50	1.50	1.41
1.49	1.45	1.45	1.45	1.42	1.75
1.44	1.41	1.46	1 • • 0	1.48	1.59
1.38	1.57	1.38	1.44	1.44	1 • • •
1.45	1.42	1.41	1 • 44	1.52	1.49
1.49	1.50	1.40	1.40	1.47	1.46
1.44	1.44	1.45	1.45	1 • 4 4	1.44
1.44	1.42	1.41	4.41	1.42	1.41

		TIBE ON TAK	TARSEF (SECS)			
0.06	0.70	1.51	2 • 1 स	3.21	→ ₹ 5	
0.21	0.26	7.28	3 • 28	7.31	フェッと	
10.01	11.03	12.05	13.05	14.07	15.05	
10.09	10.08	15.75	17.50	12.50	12.74	
20.82	21.64	22.40	23.05	24.67	ن 🕶 🕁 😘	
25.92	27.92	23.63	23.43	29.42	30.42	
31.40	32.48	32.08	31 • UB	54.07	35.12	
30.13	57.14	50.10	59.15	40.17	41.1	
42.10	43.22	44.25	45.27	46.27	47.27	
48.31	49.29	50.53	51.33	58.36	55.52	
54.38	55.41	56.39	96 • 39	57.01	50.05	
29.08	03.08	51.08	51.72	51.72	5.3.57	
63.50	64.61	60.50	55 • 62	57.53	50.65	
54.71	70.71	71.70	72.70	15.75	74.75	
75.77	76.78	77.01	78 • 80	73.85	- J•05	

NM test 3

ROLL STEP FUNCTION

	*	MS VALUE O	F ERKUR		
1.53	1.77	1.29	1.24	3.86	1.31
1.05	0.88	اع دار. (ا	0.49	1.00	1.11
1.63	1.54	1.67	1.57	1.52	1.53
2.00	1.97	1.92	1000	1.85	1 3
1.80.	1.77	1.17	1.72	1.71	1.74
1.67	1.65	1.63	1.00	1.01	1 • • 0
1.57	1.05	1.58	1.5	1.52	1.53
1.51	1.51	1.55	1.55	1.53	1 • 32
1.04	1.67	1.66	1.65	1.63	1.54
1.60	1.62	1.65	1.77	1.81	1 • : 1
1.00	1.80	1.77	1.77	1.77	1.74
1.74	1.01	1.84	1.04	1.83	I • 02
1・7ッ	1.00	1.70	1.73	1.77	1.75
1.7+	1.74	1.74	1.74	1.73	1 • / 1
1.71	1.71	1.72	1.73	1.75	1.72

TIME ON TARGUL (SEOS)						
U • 47	1.56	2.54	3.25	4.54	5.01	
6.63	7.63	8.63	9.56	13.60	11.55	
11.61	12.18	13.21	14.23	15.25	10.61	
16.01	16.56	17.56	18.96	19.00	30. 9	
21.62	22.63	23.62	24.65	2 1.67	20.00	
27.65	28.73	29 .7 5	30.72	31.78	32.16	
53.77	34.00	35.80	36 • 02	37.32	30.03	
59.88	40.45	40.62	41.52	42.63	45.4	
43.54	43.59	44.5B	40.01	46.62	41.00	
40.61	49.68	50.31	50.34	50.2%	ગઇ. ೬૩	
51.52	52.54	30.5B	54.o2	55.50	50 - 50 €	
57.62	57.79	57.97	ნგ . ქ7	59.95	51.63	
52.03	63.02	54.08	55·11	áe•12	3/.10	
68.13	69.13	70.16	71.17	72.17	73.21	
74.21	75.22	75.37	75.62	76.65	77 • e 4	

HM test 4

ROLL STEP FUNCTION

	'n	MS VALUE O	IF EKRGR		
2.53	1.57	1.02	1.47	1.73	2 • 4 2
1.03	1.34	1 مرة 1	1.66	1.60	1.663
1.65	1.51	1.49	1.33	1.40	1.43
1.55	1.58	1.57	1.42	1.65	1.55
1.57.	1.61	1.58	1.53	1.55	1.554
1.50	1.49	1.66	1.7)	1.70	1.73
1.78	1.77	1.75	1.75	1.73	1.74
1.74	1.73	1.72	1.71	1.73	1 • 0 8
1.67	1.67	1.65	1 • 65	1.7+	1.75
1.72	1.69	1.71	1 • 70	1.69	1 • 117
1.66	1.56	1.69	1.54	1.57	1 • • • •
1.72	1.75	1.74	1.73	1.73	1 • 70
1.76	1.76	1.75	1.75	1.74	1.72
1.71	1./1	1.63	1.70	1.03	1.69
1.70	1 • 69	1.69	1.69	1.67	1.67

		TIME ON TAI	ROET (SECS)	
0.21	0.96	1.90	2.39	5.61	5.00
4.94	5.49	6.95	7.10	5.30	10.03
10.75	12.03	13.09	14.05	15.08	1: • 68
17.10	18.14	19.15	17.54	19.56	25.38
21.42	22.49	23.40	24 - 43	25.56	20.002
27.54	28.54	28.97	28 • 54	29.37	2000
30.42	31.44	32.47	33 . 4 1	44.03	34.43
55.45	30.40	37.45	38 • 47	59.49	40047
41.52	42.54	43.36	44.39	44.37	44.55
45.27	46.28	47.32	40 - 52	49.54	30.42
51.38	52.41	52.4H	52 • 78	53.84	54.41
54.45	54.44	54.96	55 • ±9	57.01	10000
58.01	Jh.46	59.48	50 - 21	51.54	53.13
63.53	64.58	50 • 58	65 • 52	ഉ7∙ഉ≧	ဗ်င⊙ာ…
69.06	64.55	70.56	71.56	1:.5	75.41

MM test 5

ROLL STEP FUNCTION

			RMS VALUE OF	EHRUR		
	2.48	2.63	ટ • તે છે	2.09	1.77	1.73
	1.65	1.05	2 • 1 0	1. 16	1.9)	1.,-
	1.97	2.52	2.29	2.25	2.19	1.14
	2.11	2.08	2.16	2.05	1.90	1 3
	1.91	1.92	1.99	1.96	1.91	1 • # 8
	1.59	1.85	1.62	1.09	1.74	1. +1
	1.89	1.85	1.86	1.82	1.62	1.73
	1.81	1.70	1.77	1.73		1.72
	1.73	1.77	1.77	1.77	1.74	1.75
	1.73	1.71	1.71	1.70	1.50	1.55
	1.67	1.64	1.64	1.63	1.71	1.75
	1.74	1.73	1.72	1.71	1.71	1.09
	1.71	1.80	1.62	1.56	1.36	1.79
	1.70	1.77	=	1.70	1.75	1.72
	1.81	1.57		1.06	1.64	1.35
IJAN	OF RMS= 1	L•54				
			TIME ON TARG	ET (SECS)	
	ŭ.03	0.05	0.78	1.76	2.81	5.641
	4.75	5.21	5.23	5 • 46	· • 3 · 9	7.41

		TIME ON TA	KSET (SECS)	
ù•03	0.05	U.76	1.76	2.81	₹•61
4.75	5.21	5.23	5 • 46	· • 3 · •	7.91
8.71	8 • 65	8.01	9.58	10.55	11.01
12.10	13.16	14.18	15.20	10.13	17.23
18.23	18.99	18.99	13.35	20.94	21.96
22.98	25.79	24.99	25.43	20.42	25.53
27.40	26-44	23.40	30.42	31.40	12.47
33.49	34.52	35.54	35.00	37.52	54.1.7
39.39	39.38	39.83	40 • 05	41.07	42.0
45.71	44.92	45.92	46.96	47.99	4 2 4 4 5
49.98	51.01	52.12	53.04	53.33	54.36
54.31	ob • 54	56.31	57.46	58.34	54.37
60.22	50.19	00.41	51 · 39	52.43	7 3 . → û
54.42	55.48	56.48	57.47	56.51	1.4.55
69.85	63.83	70.57	11.38	72.36	73.42

MM test 6

みししし			
STEP	FUNC	T	ION

	ĸ	HS VALUE O	F LAH JH		
	2.17	0.91	1.45	1.27	1.44
1.13		1 4 1 1	1.17	1.11	1.00
1.11	1.11	=	1.41	1.40	1.55
1.07	1.03	1.31		1.22	1.28
1.35	1.36	1.23	1.29		
1.22	1.23	1.21	1.17	1.32	1.53
	1.51	1.30	1.30	1.35	1 - 34
1.35			1.50	1.3%	1.92
1.54	1.31	1.34		1.34	1.59
1.43	1 • 40	1.55	1.40		1.55
1.43	1.52	1.51	1.47	1.41	
	1.64	1.62	$1 \bullet 61$	1.59	1.55
1.62		1.55	1 - 34	1.62	1.07
1.58	1.56		1.54	1.54	1.63
1.68	1.65	1.65		1.7;	1.70
1.70	1.74	1.75	1.72		
1.70	1.70	1.07	1.01	1.67	1.55
		1.60	1.64	1.64	1.52
1.50	1.65		= ' '		

	1	TIME ON TAR	3c1 (5885)		
0.30	1.36	2.33	3 • 39	4 • 5 6	46 کو د
-	6.74	1.75	3 • 54	4.15	10.11
5.75		12.68	12.74	13.70	10079
11.11	12.11		18.60	19.85	20.02
15.84	16.00	17.83		25,50	73
21.89	22.55	23.94	24.54	29.45	30.45
26.72	27.75	28.79	29.40		50 • 43 50 • 47
31.44	32.47	33.49	34 · 50	55.07	
55.8¢	37.10	58.09	59 • ∪7	40.12	47.41
	41.14	42.12	45.15	44.19	44.42
40.94		45.74	46 • 33	47.86	4 5 - 21 4
44.42	44.78	51.93	52.31	53.09	55.03
44.86	50.86		55.42	5 b • 5 °	37.42
53.18	54.21	54.57		50.73	11.13
57.68	57.67	58 • 6≄	59.73		67.15
62.75	63.77	54.80	65.52	50.03	
63.86	69.50	10.88	71 • 38	72.95	15.495

MM test 7

ROLL STEP FUNCTION

	K	MS VALUE U	. k < 0R		
1.57	1.57	1.67	1.24	1.22	1.70
1.76	1.37	1 477	1 • 76	1.60	1.78
1.57	1.48	1.52	1 • 52	1.50	1.46
1.42	1.40	1.49	1 • 50	1.60	1.55
1.00.	1.60	1.48	1.55	1.51	1.50
1.48	1.47	1.66	1.17	1.50	1.73
1.78	1.74	1.13	1.73	1.73	1.65
1.72	1.76	1.74	1.72	1.71	1.72
1.70	1.68	1.67	1.67	4.65	1.55
1.63	1.63	1.60	1.15	1.78	1.77
1.74	1.75	1.73	1.73	1.73	1.72
1.71	1.70	1.60	1 • 67	1.56	1.71
1.76	1.76	1.77	1.77	1.75	1.75
1.80	1.86	1.86	1.•36	1.03	1.04
1.83	1.83	1.81	1.00	1.79	1.79

		TIME ON TAI	RUCT (SECS)	
0.06	0.25	1.20	2.33	3.31	3.00
5.53	3 • 96	4.96	5.99	7.03	5.01
9.03	10.03	11.09	12.09	13.06	14.07
15.11	16.18	16.68	15 • 55	16.74	17.25
17.98	18. ₹8	19.98	21.32	22.03	23.05
24.07	25.10	25.17	25.13	25.23	25.24
27.25	28.23	29.29	30 • 30	51. 25	47.24
32.17	32.22	35.13	34.14	35.15	35.14
57.17	38.19	39.22	40 - 27	41.12	41.14
41.91	42.72	43.58	43.54	43.54	44.17
45.21	46.22	47.19	48.01	40.19	44.19
50.24	51.27	52.27	53 • 28	54.31	. 4.38
54.37	54.56	55.31	55 • 28	5:4.63	53.72°
56.99	57.04	57.01	58 • 66	59.0a	- C - 9 H
61-07	62.08	63-11	64 - 12	55.13	55.15

MM test 8

ROLL STEP FUNCTION

		RMS	AYFAF	70	ERROR		
2.96	5.02		2.41		2.15	1.92	2.36
2.62	2 • 66		2.51		2 • 30	2.19	.10
2.04	2.05		1.95		2.18	2.23	2.28
2.19	2.19		2:18	•	2.50	3.32	2.24
2.25	2.21		2.18		2 • 1 4	2.1:	2.24
2.23	2.21		2.10		2.26	2.33	(· · 51
2.29	2.26		2.24		2 • 21	2•2u	1.15
2.14	2.15		2.12		2 • 11	3.15	. • 10
2.15	2 • 14		2.12		2 • 11	2.17	2.24
2.23	2.22		2.21		2 • 1 b	2.17	7.15
3.14	2.15		2.16		2.16	2.14	1.15
2.16	2.14		2.14		2.12		13
5•09	2.07		2.09		2.12	2.10	2.10
2.08	2.07		2.06		2.07	2.07	7.11
2.13	2.12		2.10		2.10	2.10	2.03

MEAN OF KMS= 2.16

TIME ON TARGET (SECS)							
0.04	0.00	1.09	2•05	3.11	5 • 4 1		
5.3H	3.90	4.89	5 • 41	し •94	7.95		
ช.9ห	9.95	10.98	11.11	11.0	11.40		
12.39	15.41	14.23	14.26	14.25	15.21		
16.24	17.25	18.20	19.51	17.51	1 7 . +0		
20.10	21.10	22.14	22.45	22.42	12.02		
23.67	24.67	25.87	25 • 09	27.95	25.40		
29.92	30.95	31.95	32 ⋅ 37	32.50	53.12		
34.07	34.03	34.68	35 - 72	35.49	50.08		
56.14	57.17	38.19	39 • 22	40.23	41.00		
42.16	42.53	42.52	45.24	44.21	44.14		
44.51	45.52	45.53	47.54	48.48	44.75		
50.5d	51.01	51.87	51 • 39	52.2£	54.26		
54.28	55.28	ou•27	o7 • €9	53.0s	50.63		
38.04	58.94	ラリ・ ラd	ь1.05	52.01	50.00		

MM test 9

ROLL STEP FUNCTION

		þ-	KMS VELUE (OF LRKOK		
	1.57	1.54	1.12	1.37	1.41	1.02
	1.11	0.96	1 -47	1.11	1.10	1.01
	1.00	1.11	1.11	1.13	1.25	1 • 36
	1.27	1.19	1.23	1 • 58	1.35	1.50
	1.35.	1.54	1.45	1.54	1.40	1.49
	1.43	1.40	1.53	1.58	1.57	1.55
	1.57	1.54	1.52	1.52	1.50	1.00
	1-47	1.45	1-47	1.45	1.53	1.93
	1.52	1.51	1.55	1.49	1.40	1.49
	1.58	1.56	1.55	1.55	1.56	1.05
	1.52	1.54	1.52	1.53	1.51	1.:0
	1.50	1.49	1.47	1 • >0	1.49	1.43
	1.49	1.47	1.46	1.47	1.46	1 4
	1.45	1.43	1.44	1.42	1.45	1.77
	1.57	1.58	1.59	1.55	1.55	1.55
EAN	OF RMS=	1.45				
		r	IME ON TAR	GET (3209)		
	U.98	1.98	3.03	4.04	· · · · · · · · · · · · · · · · · · ·	(, o J.4
	7 7.	· · · · · · · · · · · · · · · · · · ·				• • •

		TIME ON THE	RGET (SECS)	
U•98	1.98	3.03	4.54	9.0.	ار و را به
7.05	ರ 🛮 🛈 ಚ	9.11	3.56	9.99	13.13
12.04	13.06	14.05	15.09	16.09	10.36
16.61	17.63	18.10	18.29	1 1.2 t	20.30
21.33	22.37	22.72	22.72	23.64	24.04
8a•c5	26.68	27.18	27.19	2 3 • 3 0	: 1.08
30.12	31.07	32.12	35.10	54.17	3,.15
36.14	57.22	38.20	53.19	34.28	3 4 3 2
40.55	41.56	42.63	43 • 59	44.62	40.42
45.38	46.07	47.07	45 • 08	4 4 • 0 9	20.54
51.14	31.19	52.U8	53.07	54•0₹	95.37
ნი•მკ	57.09	56.12	50.29	5 n • 1 1	5 4 4
00.93	01.15	62.95	63.97	á+•95	50.75
51.02	58.02	69.06	70.02	. 71.16	71
71 1	10.10	3000	10102	. / 1 • 1 0	1 4 4

13.76

74.98

10.17

12.90

12.15

11.55

MM test 10

ROLL STEP FUNCTION

	RAS	VALUE	OF ERROR		
1.57	1.37	1.29	1.56	1.32	1 • .2 0
1.10	1.04	1:23	1 • 26	1.38	1.24
1.13	1.22	1.21	1 • 18	1 • 1 4	1.25
1.22	1.29	1.39	1.52	1.23	1.50
1.6Q	1.57	1.55	1 • 5 5	1.55	1.0
1.50	1.43	1.46	1 • 44	1.41	1.42
1.41	1.5d	1.44	1 • 44	1.43	1.43
1.41	1-44	1.43	1.45	1.41	1.55
1.40	1 • 59	1.55	1 • 39	1 - 34	1.57
1.35	1.31	1.57	1 • 54	4 • 5 >	1.54
1.32	1.52	1 • 3 હ	1.45	1.42	1 - 4 1
1.41	1.40	1.41	1.51	1.59	1.43
1.57	1.39	1 • 4 1	1.41	1.42	1 • 4 1
1-4G	1.40	1.39	1.44	1.46	1.45
1.44	1.48	1.49	1.49	1.49	1.48

TIME ON TARGET (SECS)							
0.41	0.70	1.71	2.74	5 • 7 b	4 1)		
5.75	6.01	5.98	7.24	3.23	** • ** **		
10.50	11.26	12.30	15•28	13.55	14.41		
15.36	15.64	16.05	17.39	1 4.13	1-25		
10.00	19.89	20.92	21.73	22.97	. 3 . +3		
24.97	25.98	26.96	21.39	2 / . 0 0	30 . 00		
31.00	32.03	32.53	32 - 10	35.70	34.034		
39.94	30.39	37.12	34 • 14	34.14	40.12		
41.13	42.19	43.17	44.15	45.21	75.1.		
47.20	48.23	47.25	5 3 • 8 5	51.32	30.01		
53.52	34 · 33	34.37	54.52	34•5 4	15.43		
ერ•87	57.88	ちゅうよ	シブ・3ブ	50.91	11 · 35		
62.32	63.62	b3•b1	64.43	90.49	+6.02		
6/.52	0 c • 8 c	J∀•55	10.00	70.62	/1.08		
72.58	12.57	7 5 . 35	14.43	7 1.43	7 4 .		

MM test 11

ROLL			
STEP	FUNC	Ţ	101

	** ?	45 VALUE U	F ERRUR		
		1.12	1.57	1.52	1.44
1.94	1.76	1 488	1.92	1.85	1.31
1.63	1.96		1.52	1.64	1.77
1.77	1.63	1.67		1.65	$1 \bullet \circ 2$
1.78	1.72	1.68	1 • 64		1.58
	1.58	1.57	1.00	1.85	
1.58.		1.85	1.00	1.36	1.75
1.68	1.65	1.73	1.71	1.70	1 • 1 +
1.77	1.75	_		1.05	1 . 19
1.66	1.06	1.64	1.00	1.50	1.00
1.61	1.59	1.58	1.57		1.52
	1.60	1.65	1.5	1.65	-
1.54		1.70	1.74	1.74	1.75
1.72	1.76	-	1.76	1.75	1.74
1.74	1.78	1.77		1.69	1.1.8
1.75	1.72	1.70	1.70	l a o u	1.71
1.73	1.50	1.61	1 •		1.1.
	1.19	1.79	1.19	1.7%	1 • 1
1.80	4017	• *			

41.43 OF R 45= 1.71

	1	TIME ON TAR	GET (SECS)		
0.41	1.41	2 • 4 b b • b 5	3 • 4 5 1 • 0 5	4.31 6.75	7.65
მ•86 მ•66	5•89 9•68	10.69	11.71	12.74	1•38 1.•58
13.31	14.34 20.40	15.30 21.45	16.56 22.42	22.52	27.58
25.37	24.38 29.40	24.53 30.48	25.37 31.44	25.34 32.40	25.40
20.43	35.52	ან•52 42•63	57.52 43.61	58.0° 44.6≩	41.00
48.55 46.65	41.01 47.08	47.07	47.55 50.35	43.52 51.33	4 : • 0 ↑ シ / • 7 ሪ
49.73 53.44	49.77 55.58	49.93 54.54	ນ ລ ຸເ3	50.65 52.7c	57.67 57.75
ა8•63 ი4•43	59.68 64.42	60 • 68 54 • 42	61 • 65 25 • 11	58.10	50.10 70.18
6672	67.77	à8 • 75	2 73	<u>6</u> 9.55	, 00 , .

MM test 12

ROLL STEP FUNCTION

(KAS VALUE O	F Lkwok		
	1.33	1.77	1.57	1. 0
	1 445	1 . 20	1.75	1.01
-	2.01	1 . 18	1.92	1 - 74
		1.72	1 • 7 ७	1.15
_		1.75	1.75	1 . 7 %
=	=	1.71	1.00	1.17
_	- .	1.71	1.70	1.7
	=	1.51	1.66	i • 00 U
		1.654	1.63	1 • 2
-		1.59	1.57	1.0
- '			1.5.	2.651
-		1.50	1.50	1
-	•	1.57	1.5	1.30
-	=	1.05	1.55	1 3
1.09	1.66	1 • 00	1.79	1 - 53
	2.57 1.42 2.10 1.82 1.65 1.66 1.75 1.68 1.67 1.60 1.56	2.57	2.57	2.57

		TIME ON TAR	(GET (SECS)	ı	
6.00	0.76	1.94	2.59	4.03	• 3 3
v • 0 ť	7.04	is - 0 3	ყ•∪ნ	8.43	1.45
9.91	10.21	11.20	12 • 24	13.25	14 • .4
15.30	16.29	17.30	13.35	19.34	23.35
21.56	22.33	23.43	≥3•∶3	25.94	2 4 . 25
23.97	26.78	27.98	20.57	25.57	1.54
30.30	31.38	32.42	33 • 42	34.42	37.42
30.45	37.49	38.48	39 • 30	40.52	41.5°
41.48	42.34	43.38	44 - 30	45-41	44.
47.44	43.42	49.42	50 • 45	51.43	97.35
23.47	54.52	ນຽ∙ສຄ	36.22	5 6. 21	2002
36.78	37.46	50.46	59.47	56.47	51.52
62.52	63.57	64.56	မသ 🗸 ပင်	စ်စ်စဉ်ပ	ပ္သမ္းရီ
60.00 60.00	67.57	68.57	હ∌ • દેઇ	70.56€	71.11
72.63	13.50	74.00	75.65	70•28	77.71

MM test 13

RULL STEP FUNCTION

		RMS VALUE D	FERROR		
1.03	1.57	1.12	1.29	1.5	,
1.73	1.01	1.67	1.45	1.43	
1.41	1.59	1.54	1.44		1.45
1.65	1.59	1.51	1 •	1.50	i • 1
1.52	1.00	1.63	1.55	1.654 1.6	و* و • ⊥
1.55	1.39	1.53	1 • 4.0	1.55 1.58	4 - 3 4
1.57	1.57	1.55	1 () 5		1.50
1.63	1.00	1.61	1.00	1.54	1.5
1.56	1.54	1.55	1.55	1.50	1.00
1.58	1.58	1.06	1.55	1.51	1 • * *
1.52	1.01	1.01	1.05	1.53	1.
1.59	1.59	1.57	1.55	1 • É J	1.19
1.53	1.54	1.51	1.04	1.55	4
1.55	1.60	1.62	1.00	1.05	1.5
1.59	1.59	1.58		1.05	10
		4 ● U.S.	1.7	1 • 100	1 - 6

		TIME ON TA	Maci (udos)	•
J•23	0 - 10	1 - 31	ن با	· • • • •	• • •
4 • 63	5.00	0.94	7.90	う・ラン	
10.94	11.96	12.38	13.31	1:081	1
15.46	16.48	17.13	17.54	10.30	
20.38	20.51	20.58	1.13	22.75	1 4 . 5 .
25.05	24.53	25.59	لان • 26	27.60	1 - 3
28.74	29.76	30.75	31.04	32.62	
54.04	34.49	35.4.	56 • 50	37.54	1000
59.10	40.13	41.16	42 • 17	43.17	3 ₍ • ' 3
43.59	44.62	4-64	45 • u.d	47.63	43.52
49.68	30.17	⊃ 0 • 0 a	21.0h	52.11	** * • • •
54.09	55.12	56.12	57.13	58.17	- 11
60.14	61.13	85.40	62.23	50.16 50.36	د 1 • ۱ ۰۰
64.65	54.70	65.10	55 • E3		v ' • 65
61.20	70.16	71.17	72.20	57.05 73.1c	74.13

MM test 14

۲	ソレレ			
S	TEP	FUNC	Ţ	IU.V

	1 21	45 VALUE 0	F ERROR		
3.14	2.09	1.70	1・27	1.41	1.70
	1 • 36	1 -34	1 • 36	1.42	1.52
1.63	=	1.31	1.55	1.20	1.25
1.51	1.26			1.33	1 • 115
1.22	1.38	1.37	1 • 34		= "
1.51.	1.27	1.25	1 • 23	1.36	22
	1.24	1.27	1.25	1.34	1.40
1.24	- · -		1.47	1.42	1 - 44
1.47	1.47	1.47			1.02
1.42	1-44	1.40	1.41	1.3/	
1.40	1.39	1.50	1.34	1.50	1.56
	1.51	1.52	1.49	1.49	1 • 4 >
1.50		1.44	1.45	1.4:	1.45
1.47	1.45	-	= -	1.46	1.43
1.43	1.42	1.43	1 • 41		-
1.39	1.41	1.38	1.59	1.40	1 • 4 3
_	1.41	1.41	1.42	1.43	1.⊸0
1.45	= -		1.55	1.46	1.4/
1.41	1.40	1.55	¥ U U	• • • •	-

		TIME ON TAR	GET (SECS)	1	
0.06	1.01	2.60%	3.00	4.33	4.45
5.51	6.48	7.55	7.06	5.653	n = 0, 1
10.65	11.46	12.08	15.71	1 4 • 7 1	11.75
16.74	16.78	17.73	13.74	19.75	10.75
21.75	22.79	23•88	24 • 04	2 2 • 5 5	• 3 ×
21.78	27.79	20.72	23.72	327	\$9.55
51.58	32.35	33.38	34 - 43	30.42	રેળ•ધાટે
37.47	36.47	37.47	40 • 40	41.51	72.10
42.67	43.63	44.54	44.7	45.3%	47.40
47.12	47.43	48.41	49 • 45	5 U • 4 E	51.44
52.48	53.40	54.50	5 % DZ	26.54	57.00
5d•58	29.59	a 6 • 6 3	(1.52	5.1.67	, D • U B
a4.68	00.66	56.60	57 . 72	27.57	· · · · · · · · · · · · · · · · · · ·
58.88	69.92	70.92	71.55	72.05	7: • • 3
74.96	75.98	77.01	73 • Co	78.12	18.50

RL test 1

rt	JL L		
S	TEP	FUNC	TION

		.,,,	F इवरणस्	1 0 /	2.4
1.58	1.93	3.73	5.42	3.26	
2.84	3.11	2.71	2.75	2.70	200
2.43	2.42	2.34	2 • 28	2 • 1 ò	2.2
2.14	2.19	2.15	2.10	2.09	2.1
	2.00	1.99	2.06	2.13	7.1
2.01	2.05	1.99	2.00	2.06	2.0
2.09		1.97	1.96	1.9=	1.0
2.02	2.00		1.35	1.04	1.
1.39	1.90	1.88			1.1
1.81	1.61	1.79	1.70	1.74	
1.73	1.72	1.71	1.70	1.77	1.
1.75	1.78	1.77	1 - 33	1・パラ	1 .
1.87	1.35	1.84	1.35	1.82	1 • 1
1.80	1.50	1.79	1.74	1.75	1 . 7
-		1.70	1.75	1.70	1 • 1
1.79	1.73		1.76	1.75	1.
1.75	1.77	1.77	1.10	101	

		TIME ON TAR	RGET (SECS)	1	
0.00	0.41	0.43	0.55	₩•3 5	$1 \cdot 1$
2.45	2.40	3.11	4.19	2.13	5.20
7.20	8.23	9.21	10.25	11.24	17.51
15.18	13.16	13.7U	14.71	13.71	10.18
	18.25	19.20	19.03	19.85	207
17.25	22.67	23.38	24.34	25.37	25.614
21.89		20.09	29.65	30.67	31.70
25.58	27.62	_	38 • 59	36.74	31.13
52.70	53.72	34.73	41 • 34	42.86	43.04
38.74	39.80	40.78	47.32	44.25	40.43
44.92	43.73	40.41		52.14	52.13
49.46	20.47	51.52	52.15		٠١٠)
54.01	55.06	26.0 €	57.04	ນຄ•0≀ຄໍ	
60.13	51.17	£2.13	· 1 · 13	54.18	57.15
60.23	56.05	51.07	(5.05	59.11	70.12
71.07	71.58	71.72	72.11	73.5⊲	74.51

RL test 2

ROLL STEP FUNCTION

		5.45 VALUE O	IF ERRIN		
1.15	1.76	o.91	1 • 24	1.11	1.10
1.19	1.24	يا ⊷ يَال	0.13	1.10	1 - 1 1
0.97	1.11	ပ •ပိုင်း	0 • n8	ប្.১១	S 7
1.05	1.38	1.37	1 • 58	1.10	1.32
1.61	1.61	1.02	1 • 35	1.50	1.09
1.57	1.55	1.53	1.50	1.51	1.45
1.44	1.46	1.52	1.53	1.61	ج، ٠٠
1.61	1.09	1.57	1.57	1.50	1.55
1.57	1.55	1.55	1.53	1.54	1.00
1.52	1.52	1.50	1.52	1.45	1.+9
1.47	1.45	1.45	1.46	1.45	1.43
1.42	1.41	1.42	1.41	1.40	1 - + 3
1.41	1.38	1.35	1.57	1.42	1 - 40
1.45	1.44	1.4.7	1.42	1 • 4 1	1 + 44
1.44	1.48	1.47	1.4/	1.45	1.95

		TIME ON TAI	RGET (SECS)	
0.03	1.14	2.16	3.19	4.15	5.71
0.20	7.26	8.25	9.29	10.50	11.23
12.50	13.34	14.50	15 • วัย	15.41	17.45
10.28	18.35	10.95	1∌.76	20.75	21 • 12
21.85	22.10	22.40	25 • 45	24.47	. 3.18
25-63	20.72	27.77	63.79	23.7v	30.71
51.80	32•8 3	33.20	35.73	54.72	50.72
30.72	37.75	34.71	34.53	39.79	40.13
41.82	42.85	43.58	44.54	45.88	11 6 6 5 d
46.97	43.01	49.03	50.13	51.06	50.3
53.12	34.12	33.12	50.13	5/•21	55.14
59.15	5U • 17	61.24	62 • 22	53.27	54 4 3 3
65.31	u6.51	67.51	bs • 56	ნა• ಟ 2	క గంపువ
70.55	71.35	72.57	73.41	74.43	70.05
75.51	700.32	77-59	73 - 13	7 1 . 5	0.43

RL test 3

ત	UL	L	•			
ذ	TE	P	- 0	NC	1 1	ON.

1.94 1.30 1.29	1.9=	1.15	1.54	1 • 54
196/	1.46	1.57	1.57	i • /
1.51	1.41	1.77	1.44	1.00
	1.01	1 • 55	1.57	1.5%
=	1.01	1.50	1.51	1.+
	1.44	1.42	1.41	1.40
	1.41	1.41	1.41	1 • 55
	1.40	1.57	1.39	1 • 50
		1.37	1.41	1.34
	1.42	1.45	1.42	1.41
	1.39	1.40	1.59	1.5
		1.59	1.35	1 - 5
		1.40	1.35	1 - 58
1.35	1.56	1.39	1.37	1 - 48
	1 • 47 1 • 54 1 • 45 1 • 41 1 • 41 1 • 40 1 • 44 1 • 42 1 • 41 1 • 57	1.47	1.47	1.47

		TIME ON THE	KGET (SECS)	•	
0.99	1.40	2.26	3. 23	4.30	9.25
6.31	7.55	8.39	9.38	10.06	10 • ∞
11.61	12.28	13.33	13.74	14.71	15.73
16.80	17.28	19.24	19.23	20.28	20.63
21.67	22.64	23.53	23.70	24.04	20.03
26.08	27.10	28.12	29.14	3 U • 1 7	31.13
32.19	33.18	34.22	35.20	36.25	4 (• 1 ئ
30.22	39.29	33.68	40 - 55	41.71	40.72
42.99	43.66	44.63	45.71	45.71	47.12
43.76	49.09	30.Ul	50 · 97	52.06	55.92
54.03	54.19	55.22	55 • 24	57.20	\$ 5 4 2 2
58.83	59.83	60.05	61.90	62.30	n 5 • 13
64.46	ε5•25	66.27	67 • 26	68.2€	1 د ۱۰۰۰
	71.31	71.75	72.10	75.72	74.70
70.21 75.76	10.77	17.77	19.25	79.0s	80.12

RL test 4

ĸ	ULL		
S	(EP	FUNCT	LON

•						
			KMS VALUE OF	<u> </u>	,	
	5.76	3.19	3.26	2.69	اد 5 و ہے	2.44
	2.22	2.11	2.03	2.02	1.90	1.39
	1.92	1.83	1.79	1 • 84	1.84	1.65
	1.90	1.57	0 د و	1.60	1.73	1.12
	1.70	1.68	1.72	1.70	1.66	1.02
	1.63	1.59	1.59	1.59	1.50	1.57
	80.1	1.60	1.60	1.60	1.59	1.55
	1.50	1.59	1.53	1.52	1.50	1.01
	1.50	1.48	1.46	1.47	1.53	1.52
	1.51	1.50	1.53	1.56	1.57	1.5
	1.54	1.54	1.54	1.52	1.50	1.12
	1.50	1.52	1.49	1.49	1.4€	1.47
	1.51	1.50	1.53	1.50	1.50	1.56
	1.55	1.54	1.54	1.54	1.53	1.53
	1.55	1.54	1.53	1.58	1.57	1.558
M E A .I	OF RMS=	1•61				
			TIME ON TARG	SET (SECS)		
	0.09	0.05	0.90	1.53	0 • 1 0 • 1	4.02

	1	IME ON THE	RGET (SECS))	
0.09	0.05	0 . 9 ه	1 • 53	3.01	4 . 0 ≟
5.01	6.03	7 • 0 b	7.83	s.35	1.41
10.45	11.41	12.38	12.58	13.00	14.63
14.50	15.33	16.34	17.45	18.55	19.40
20.38	20.73	21.74	22.70	23.73	24.75
25.80	26.83	27.82	28 • 25	27.32	50.30
31.15	31.24	32.07	33.10	34.10	36.12
30.12	31.15	38.17	39 . 22	40.23	91.28
42.26	43.26	44.23	45 • 24	45.47	45.47
47.48	48.49	43.22	49.42	50.33	51.55
52.37	53.59	54.38	55.42	50.45	57.47
28.46	58.81	54.82	a6 . 84	51.3n	J: . 70
52.40	65.88 .	04.70	25.71	56.35	-7.17
67.81	ud. 71	61.77	70 • ≎3	71.77	12.56
72.95	73.98	74.96	75.33	75.31	10007

RL test 5

RULL STEP FUNCTION

		RMS VALUE O	F ERROR		
3 -3 8	4.26	5 • 7 ն	3.24	2.90	: •7L
2.41	2.42	2.19	2.19	2 • 1 2	2 - 9 8
2.13	2.08	1 • 98	2.04	1.98	1.67
1.82	$1 \cdot ci 1$	1.79	1.79	1.71	i . U
1 • 8 0	1.75	1.75	1.72	1.6€	1.79
1.63	1.06	1.65	1 • 56	1.70	1 9
1.54	1.64	1.65	1.71	1.70	1.4
1.67	1.62	1.64	1 • 0 0	1.54	1.73
1.66	1.67	1.66	1.65	1.65	1.55
1.62	1.62	1.60	1.59	1.57	1 • ±7
1.57	1.77	1.79	1.31	1.42	1.43
1.82	1.80	1.80	1.74	1.77	1.70
1.77	1.78	1.78	1.75	1.70	1.75
1.74	1.75	1.75	1.75	1.73	1.74
1.75	1.78	1.78	1.70	1 • 7 ს	1.76

		IAT NO BELT	RGET (SECS))	
0.00	0.01	0 • 3 7	1.41	2.46	3.44
4.46	b•53	6.0 6	5.75	7.98	e 🐞 🕽 🕂
9.04	9.90	11.00	12.01	13.00U	14.35
15.09	16.08	17.11	13.45	15.56	10.38
20.01	20.74	21.93	22 · > 3	23.94	الإنجاب والان
25.14	26.14	27.22	∠3 • U4	2 3 • 3 9	21.00
30.40	31.37	32.44	32 · 75	33.50	34. 2
35.53	36.57	57.60	33 • 52	37.50	4.00
40.64	41.64	42.63	43 · 68	44.67	45.12
46.72	47.07	48.11	43.10	20.11	51.11
52.14	52.41	32•68	u3•89	54.37	f 3
55.88 55.88	56.07	57.91	54. 12	5 1. 3a	, j • ⁴ •
61.62	52.13	63.10		55.25	50.21
67.18	58.25	59.22	(५•೮ರ	70.35	/1.41
72.50	12.45	73.45	74 • 47	75.47	16.43

RL test 6

ROLL		
STEP	FUNC	TION

		AS VALUE O		. 7)	
3 - 55	4 • 24	ناە∙د	3.04	≥•77	₫••/
2.37	2.25	2 , 28	2 • 3 €	1.85	1 • **
1.99	2.03	1.54	1 • 36	1 • ⇔ π	1 - 3
1.73	1.72	1 • 71	1.74	1.72	1 • 4
1.64	1.71	1.67	1 - 56	1.600	Ì.
1.59	1.57	1.60	1.51	1.53	i • =
1.56	1.61	1.06	1 5	1.61	1.00
1.60	1.59	1.57	1.06	1.54	1.5
1.55	1.54	1.54	1. 10	1 - 12	1.0
1.53	1.50	1.50	1.50	1.55	1.5
1.53	1.53	1.52	1.51	1.51	1 • 4
1.48	1.43	1.47	1.46	1 • 4 %	1 • 4
1.44	1.49	1.50	1.43	1.49	1.5
1.49	1.48	1.45	1	1.47	1 • 4
1.45	1.45	1.44	1.43	1.43	1 • 4

TIME UN TARGET (SECS)							
0.05	0.06	0.94	1. 75	2.93	4.31		
4.90	5•ე5	6 • 5 8	7.09	± 60	4.59		
10.00	10.75	11.76	12.51	15.70	143		
15.79	16.79	17.89	18.85	19.13	20.15		
21.17	21.94	22.42	23 • 44	24.45	25.45		
20.52	27.50	27.98	28 • 62	29.62	50.70		
31.69	32.49	32.89	33 • ≈U	34.7 /	31 • 33		
35.88	57.45	38.45	39 . 52	40.40	41.45		
42.52	43.52	44.24	44.73	45.74	40.02		
47.81	48.97	49.87	50 • 33	51.13	ગઢ•ઇઠ		
53.07	54·12	55.11	56.13	57.13	53 + 16		
59.21	60.18	61.23	62.73	63.22	54.23		
65.28	55.87	66.33	67.40	ခ်မှ ခဲ့သို့	J 1 • J 5		
70.37	71.42	72.38	73.46	74.47	79.47		
76.48	17.50	18.55	79 • 53	ಟ≎•೨೦	.1.07		

RL test 7

ROLL STEP FUNCTION

	K	MS VALUE O	F ERRUR		
2.01	1.11	2.03	1.57	1 • •	≥ • 93
2.01	2.01	1 • 99	1.76	1.30	1.4
2.04	1.97	1 🕹 b 0	1.0	1.84	1.79
1.94	2.00	1.92	1.08	1.85	1 • 5 U
1.30	1.78	1.77	1.75	1.71	1.71
1.73	1.82	1.84	1.54	1.02	1.3
1.92	1.91	1.90	1 • 58	1.8:	1.56
1.64	1.88	1.86	1.55	1.85	1.5
1.86	1.87	1.86	1.54	1.55	12
1.81	1.33	1.83	1.73	1.82	1 • 5 0
1.73	1.79	1.77	1.75	1.75	1.79
1.79	1.78	1.77	1.75	1.77	1.75
1.74	1.73	1.77	1.79	1.73	1.75
1.75	1.74	1.75	1.75	1.73	1.73
1.71	1.70	1.65	1.72	1.79	1.19

		TIME ON TAR	KGET (SECs))	
0.04	0.06	1.10	2.11	2.41	2.45
3. 50	4.50	4	5 • 30	0.20	7.03
7.03	7.75	5.75	9.23	10.51	11. 1
11.91	12.16	15.10	19.19	1: •23	118
17.21	18.28	19.23	20.29	21.24	ಪಚ∗ಾಡಿ
23.24	23.18	23.50	24 • 25	25.25	• . 7
20.35	26€,57	27.58	28 • 59	23.62	03.45
31.64	31.68	52.23	53.27	34.25	1. 1. 1. 1. 1. 1.
3 5•59	35.69	56.74	57.75	აც.75	50.17
40.82	40.39	41.20	42 - 26	43.28	4× • 18
45.33	46.53	47.56	45 - 30	49.42	41.57
49.81	où•78	51.82	ა2 • 82	53.82	", t . " G
55.66	56.71	>0 • 54	57.13	30.14	5.24.17
60.27	61.22	62.26	63 • ₹8	54.23	i5 € 50
60.32	67.30	6n • 51	64 - 33	55.9€	m + • 25

RL test 8

ROLL STEP FUNCTION

1.61 1.92 1.82 1.65 1.65 1.57	1.11 1.64 1.73 1.59 1.64 1.58	RMS VALUE 0 0.51 1.77 1.77 1.53 1.63	F ERROR 2 • 15 1 • 03 1 • 71 1 • 57 1 • 60 1 • 65	2 • 1 1 1 • 7 0 1 • 7 0 1 • 7 0 1 • 5 6	2.05 1.00 1.55 1.56 1.76
1.61 1.67	1.59 1.65	1.59 1.53	1.56 1.51	1.67	1.57
1.59 1.73	1.58	1.58	1 • 45	1.59 1.54	1.58 1.54
1.72	1.77	1 • 74 1 • 71	1.74 1.72	1.74 1.74	1.74
1.72	1.76 1.74	1.75 1.75	1 • 75 1 • 74	1.73 1.72	1.77
1 • 70 1 • 71	1.72 1.71	1 • 74 1 • 71	1.74 1.70	1.72	1.72

		TIME ON TA	KGET (SECS)	
0.34	1.46	2.30	2.76	د با و د	
5.1 8	5.60	0.003	1.00	5.40	9 • 1 ÷
9.45	14.43	11.50	12.46	11.40	୍ଟ 🗝 🕀 ଅ
15.56	16.54	17.50	13.20		14.49
20.39	21.40	22.40	23.42	1 3 • 3 6	12.54
26.45	26.63	27.39	28 • 45	27.43	23.97
30.18	31.14	32.22		29.19	ن ،
54.19	35.22	36 • 12	აპ•22 2₹ ১০	55.20	35.78
41.17	41.18		57.12	30.15	01.13
45.22	45.71	42.19	43.18	44.24	45.24
49.75	- -	46.71	47 • 71	45.53	41.5
	50.74	51.52	51.52	54.52	us.s6
53.21	34.27	55 • 29	56.13	5ื่ธ•1ืฮ	5/.14
30.16	59.22	60.19	61.19	62.26	65.2b
64.23	54.90	55•10	ω ύ • 10	€7.07	5 • 0 3
69.17	70.17	71 • 17	72 • 18	73.26	74.32

RL test 9

RULL STEP FUNCTION

			RMS VALUE OF	ERROR		
	1.90	2.09	1.29	1 • 47	1.31	1 • i 1
	1.05	1.24	1.23	1.51	1 • 0 0	1.14
	1.19	1.68	1.65	1.77	1.57	1.52
	1.48	1.51	1.71	1.67	1.64	1.62
	1.62	1.58	1.57	1.55	1.54	1.0
	1.49	1.54	1.53	1.50	1.51	1 • 1.3
	1.48	1 • 4 7	1.46	1.45	1.45	1.45
	1.49	1.47	1 • 46	1 - 53	1.53	1 • 1
	1.00	1.50	1.53	1.52	1.52	1.0
	1.50	1.50	1.50	1.43	1.46	1.46
	1.47	1.40	1.45	1.46	1.45	1.45
	1.47	1 • 47	1.40	1.45	1.49	12
	1.57	1.57	1.55	1 • ∞6	1.07	1.00
	1.55	1.54	1.54	1.74	1.52	1.65
	1.51	1.50	1.50	1.59	1.56	1.51
4 FA IV	OF RMS=	1.50				
			TIME ON TARO	et (ŞECS)		

TIME ON TARGET (SECS)							
0.01	0 • 36	1.59	2.41	5.41	+ + + 1		
5.41	6 • 48	しゃのソ	7.71	21 . 7 1	1.71		
10.74	10.79	11.13	11.09	13.00	19.31		
15.06	16.03	16.01	17.05	13.00	11.00		
20.06	21.08	22.12	22.34	23.52	. · • : 5		
25.33	25.77	26.82	27.30	25.37	21.33		
50•87	31.92	32.94	33 • 59	34.77	ل يا د :		
პი∙05	57.07	38 • U3	33.14	3 3.60 €	40.00		
41.05	42.07	42.47	43.12	44.13	99.73		
4 1 • 46	40.48	47.49	48.47	44.49	4 . 14		
50.84	51.29	52.92	53. <i>3</i> 3	54.61	15.662		
56.02	o6∙97	50.01	59.03	60.02	11. 194		
6U.87	51.90	62.45	63.12	64.12	- 7.13		
ou•18	31.17	58.21	59.27	70.23	71 . 7		
12.20	73.30	74.28	75.52	76.33	7/.39		

RL test 10

RULL	
STEP	FUNCTION

STEP	FUNCTION					
			RMS VALUE O	DE ERRUR	•	
	1.91	5.45	2.87	2.67	2.23	2.07
	2.06	1.80	1.73	1.75	1.664	1 5
	1.57	1.57	1.52	1.49	1.59	4.46
	1.57	1.55	1.51	1 • 48	1.55	1 - 41
	1.44	1.41	1.35	1.50	1.35	1.56
	1.39	1.36	1.51	1.40	1.5>	1.40
	1.38	1.40	1.41	1 • 59	1.53	1 • * 1
	1.39	1.56	1.33	1 • 34	1.56	1.33
	1.33	1.30	1.31	1.19	1.31	1.43
	1.41	1.41	1.39	1.55	1.47	1.46
	1.46	1.44	1.45	1.45	1.45	1.48
	1.49	1.46	1.47	1.45	1.45	1.47
	1.46	1.46	1.45	1.45	1.43	1.45
	1.44	1.45	1.45	1 • 40	1.43	1.44
	1.44	1.45	1.42	1.45	1.49	1.47
4LAN	UF RMS= .	1.43				
			TIME ON TAR	RSET (SECS)	•	
	0.05	J.48	1.10	2 • 11	3.13	1 .
	D.1d	6.18	7.24	8.24	9.21	10.00
	11.28	12.53	15.31	14.35	15.03	15.51
	16.08	17.05	18.03	19.09	20.11	21.14
	22.12	23.12	24.19	25.13	25.19	4 د. • ۱
	27.04	23.67	23.69	27.40	30.74	2 1.00
	32.90	33.52	34.53	30.53	క్ష∙చ్చ	51.04
	38 ∙ 55	39.59	40.63	41 • £7	42.50	41.00
	44.69	45.72	40.76	47 • 76	40.71	'• • I
	49 . 87	50.92	51.74	52.47	23.31	5 4 · 4
	55•2s	56.28	57.33	უ გ • 34	5 4 • 5 c	5 • /
	60.72	51.72	62.78	63.72	54.75	· / • • • ·
	ps • 12	57.20	58.22	49-18	70.21	71.01
	12.26	73.27	73.53	74 • 50	75.55	7 20 25
	77.20	78.20	19.22	ದ0 • ೭೩	90.45	,1.52

RL test 11

RULL STEP FUNCTION

ĸ	MS VALUE O	F EKROK		
2.64	3.51	2.33	2.65	7.40
2.15	1.92	1. 19	1.669	1 ?
1.97	1.90	1.96	1.36	ڭ، يا
1.75	1.69	1.72	1.70	2 (10)
1.66	1.63	1 • 0 0	1.66	1.53
1.56	1.54	1.52	1.50	1.45
1.55	1.54	1.54	1.53	1.7
1.51	1 • 50	1.47	1.47	1.49
1.54	1.51	1.53	1.51	1. 0
1.49	1.49	1.45	1.47	1.4
1.48	1.47	1 • 46	1.44	1 - 4 4
1 • 44	1.45	1.42	1.41	1.41
1.41	1.40	1.39	1.59	1.75
1.37	1.57	1.00	1.35	1 . 5
1.57	1.37	¥ • 36	1.57	1.45
	2.64 2.15 1.97 1.75 1.66 1.56 1.55 1.51 1.54 1.49 1.48 1.44 1.41	2.64 3.31 2.15 1.92 1.97 1.96 1.75 1.69 1.66 1.63 1.56 1.54 1.55 1.54 1.51 1.50 1.61 1.50 1.49 1.49 1.49 1.49 1.48 1.47 1.44 1.45 1.41 1.40 1.57	2.64 3.31 2.39 2.15 1.92 1.99 1.97 1.96 1.96 1.75 1.69 1.72 1.66 1.63 1.60 1.56 1.54 1.52 1.55 1.54 1.54 1.51 1.50 1.47 1.54 1.51 1.53 1.49 1.49 1.45 1.48 1.47 1.46 1.48 1.47 1.46 1.41 1.40 1.39 1.37 1.37 1.55	2.64 3.31 2.33 2.68 2.15 1.92 1.79 1.89 1.97 1.96 1.96 1.86 1.75 1.69 1.72 1.70 1.66 1.63 1.60 1.60 1.56 1.54 1.52 1.50 1.55 1.54 1.52 1.50 1.55 1.54 1.67 1.67 1.69 1.47 1.47 1.64 1.51 1.63 1.61 1.49 1.49 1.45 1.47 1.48 1.47 1.46 1.44 1.44 1.45 1.42 1.41 1.44 1.45 1.42 1.41 1.44 1.45 1.59 1.39 1.37 1.37 1.56 1.36

TIAL ON TARGET (SECS)							
0.20	1.21	1.46	2.43	د ۹ و د	* • > 5		
5.56	o • 58	7.55	8.53	5.61	$1 \circ \bullet \cdot 1$		
11.01	11.78	12.76	13.74	14.61	1 15		
16.18	17.23	18.20	19.28	20•26	20.0		
21.50	22.65	23.69	24.45	27.61			
27.54	23.24	21.20	30.27	31.25	1.2.2.9		
33.29	33.63	34.650	30.15	57.65	37.00		
3 მ•7∠	39.68	40.57	41.75	42.70	4 7 .		
43.93	44.96	46.01	47.02	47.99	4 - 401		
50.04	51.07	52.66	უ პ • პნ	54.12	ځ د نه ۱۹۰۹		
55.41	56.44	57.45	೨3 • 48	54.44	.5.52		
61.51	32.55	⊍3•5 5	64• 15	50.5 <i>1</i>	401.07		
ú7.58	ამ• ხ1	59.65	70 • ພ€	71.70	72.00		
73.73	74.72	75.75	13.15	77.50	701		
78.97	80.00	81.06	a2.07	ម ១.ប ស	8.5.32		

RL test 12

ROLL STEP FUNCTION

rt	45 VALUE U	कि इ.स.स. १४		
1.76	1.70	$1 \cdot 5I$	1.57	$1 \bullet \oplus 1$
1.24	1.25	1.30	1 • 3 u	1.4
1.32	وو. ن	4 . 27	1.14	1.11
1.14	1.10	1.11	1.11	i + 1 1
1.51	1.30	1.31	1.27	1.00
1.29	1.27	1.22	4 • 3 J	1.41
1.28	1.20	1.20	1.27	1 • 7
1.32	1.39	1.43	1.53	1.00
1.39	1.31	1.34	1.5%	1.53
1.50	1.51	1 . 29	1.51	1.54
1.54	1.32	1.51	1.32	4 + 54
1.56	1.51	1.55	1.55	1.
1.53	1.51	1.50	1.50	1.50
1.30	1.23	1 • 41	1.31	1.00
1.32	1.51	1.50	1.39	1 • 1 3
	1.76 1.24 1.22 1.14 1.31 1.29 1.28 1.32 1.32 1.34 1.35 1.35	1.76	1.76	1.76

1.44 OF RM = 1.28

		TIME ON TAI	KOIT CECS)	
0.01	U • 45	1.55	2 . 55	*•53	19 4
5.54	o◆りサ	7.60	ن ≟ و د	1.54	19 • * b
11.63	12.61	13.50	14.75	15.69	71
17.74	13.70	19.70	∠0 • 7 ਤ	21.57	11.78
23.23	23.66	24.54	25.95	2,.97	21.
28.9 7	30.00	31.03	51 . 97	32.31	3.5
34.40	35.39	36.44	57.43	50.43	21.56
40.45	41-24	91.61	42.62	45.54	14.65
45.63	46.71	47 · L. 3	48.72	43.75	J. J. 1 11
51.77	52 . 77	13.60	54.41	55.34	
57.07	53.09	50.05	₽1.Ua	51.12	1 .
05.13	54.10	64.85	65.53	ნნ•აპ	7.
იმ • 5 7	39.57	70.63	/1 · oz	7.3.53	1 3
74.47	75.50	70.47	75.05	77.87	7. • ° 0
79.23	30.21	v1.22	62.25	30.22	31.50

RL test 13

ROLL	
STEP	FUNCTION

1.00 1.05 1.07 1.17 1.55 1.57 1.54 1.54 1.56 1.56 1.56 1.56	1.94 1.04 1.05 1.55 1.57 1.52 1.41 1.39 1.37 1.51 1.51 1.52	1.20 0.90 0.90 1.41 1.30 1.34 1.46 1.36 1.35 1.35 1.35 1.32 1.32	F	1.00 1.00 1.00 1.57 1.40 1.50 1.50 1.57 1.50 1.54 1.54 1.56 1.51	1.01 1.04 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.05
1.31	1.30	1.34	1 • 54	1.32	1.10

46AN OF AMS = 1.31

	Ţ	THE U. TAK	GET (DECS)		
	1.50	2.20	5.29	4.34	3
0.26	_	8.30	9.39	10.40	11.45
U • 34	1.40	14.43	15.41	11.090	
12.46	13.45	17.30	20.00	22.01	21 🗸 🤫
13.28	10.30		20 • nV	2: .34	7.15
22.58	23.95	24.90	51.19	32.1	: .17
23.12	23.12	30.14	36.37	37.37	
34.20	55.27	35 • 38		4 3 • 4 %	99.0
39.43	40.42	41.44	42 - 48	46.07	1 -1
40.51	43.71	46.91	47.41		1
5 4 - 54	51.76	ეპ.•0∠	54.01	nt•01	. 1. 10
07.05	56 . 63	5 ৮ • მ ა	59 . 36	5 C • 5 S	
62.36	03.53	64.42	JD•4J	52.4%	``• ·• :
	00.00	76.45	70 - 30	11.00	12
50.45	74.51	1:0.55	70.00	77.57	7.
73.55 70.67	73.70	00.67	61 • 6 8	52.71	15.14

RL test 14

RIEL STEP FUNCTION

	H	MS VALUE 3	- J.e		
1.60	1.57	1.11	1.27	1.11	1. · C
1.19	1.04	1 • U >	1.45	1.5"	1.00
1.54	1.50	1 • ' <u>ن</u> 1	1.30	1.47	1.53
1.42	1.43	1.57	1.50	1.43	i . + 1
1.55	1.38	1.33	1.53	1.55	1.51
1.29	1.53	1.52	1.85	1.27	1 • :7
1.26	1.25	1.25	1.20	1.27	1.50
1.13	1.21	1	1 • 3 >	1.30	1.67
1.29	1.28	1.27	1.28	$1 \bullet \hat{c} \leftarrow$	1 • ′ G
1.29	1.29	1.27	1 - 25	1.27	1.27
1.29	1 • 27	1.26	1 • 7 5	1.24	1.4
1.20	1.25	1.21	1 • 15	1.616	1. 7
1.30	1.29	1.000	1 . 43	1.4	4
1.53	1.52	1.32	1.51	1.30	i • * 0
1.34	1.54	1.36	1.54	1.54	·

4. AN OF KMS= 1.31

		TIME UN TAN	R OT (SECS)	
0.45	1.43	2.45	3 • 4 S	0.65 €	. 53
6.51	7.53	8 • 4 9	9.14	**• .3 c	10.00
11.89	12.95	15.93	14.55	150.45	123
17.29	16.26	19.31	20.33	20.5€	_1 · · ·
22.65	23.64	24 + 64	. 5 • 7.1	2 → • 7 .	1.
28.70	29.15	36.75	31.75	33.77	55.17
34.80	35.82	೨६⊛೮೪	57 • 3°s	3	
40.00	41.84	42.72	42 . 99	47.55	19.632
45.32	40.25	47.35	48 • 33	4 31	9 1.17
ou . 59	01.74	52.71	55.74	54.75	.73
55. 7 9	57.01	50.73	37.84	50. 37	34.7
62.17	63.22	64.17	υ5 • 17	56.2J	1.15
ь7•31	ამ∙ 55	59.53	70.00	71.65	11.00
73.05	73.96	74.98	75.5s	75.95	1 1.3
75.01	79.52	υ 0•3 ο	ئان ، 1	32.35	\$

SF test 1

H	٦L	L				
5	IE	Р	FUNC	Ţ	10	Ŋ

			RMS VALUE OF	FERRUR		
	2.55	1.36	1.11	1 • 55	1.5.	1.41
	1.11	1.71	1.57	1.72	1.01	1.54
	1.57	1.49	1.47	1 • 47	1.55	1 • 54
	1.33	1.29	1.35	1.69	2 • 0 w	2.37
	2.11	2.16	2.16	2.13	2.10	2 - 56
	2.06	1.97	1.99	1.76	1.93	1.3
	1.90	1.88	1.65	1.46	1.91	1.1
	1.90	1.91	1.95	1.74	1.91	1.71
	1.87	1.38	1.86	1.84	1.82	1.5
	1.80	1.19	1.78	1.79	1.82	1.58
	1.86	1.85	1.63	1.90	1.92	1 • • 0
	1.88	1.38	1.57	1 • 86	1.85	1 - 4
	1.84	1.82	1.82	1.01	1.80	1.19
	1.84	1.32	1.94	1.93	1.92	1.3
	2.00	2.02	2.01	1. 99	1.99	1. '8
MEAN	JF KMS=	1.85				
			TIME ON TARG	SET (SECO)		

		TIME ON TAR	GET (SECS))	
0.03	1.03	2.05	3-10	4.11	5.44
6.11	€ • 34	r. •84	7.16	ರ•14	1.17
10.21	11.19	12.23	13.19	14.30	10.00
16.31	17.31	10.29	18.35	10.30	1 4 - 51
10.20	19.33	20.08	21.10	22.10	11.14
24.14	25.19	24.17	27.23	28.19	25.02
30.22	31.25	32.25	53.17	33.13	45.11
34.80	35.04	35.33	36.37	57.38	5: • 57
39.40	40.42	41.44	42 . 44	43.44	44.45
45.49	46.53	47.52	48.53	48.81	45.75
49.81	ວ 0 • 8 3	51.87	51.71	52.14	na • 13
54.12	55.14	55.47	56 • 43	57.52	5 • 4 o
59 .5 3	oú•08	6 € • H3	61.51	52.80	25.53
54.11	54.15	54.00	64.60	65.68	45.45
55.43	56.51	o 1 •48	88 ∙ >3	5 1.51	70.57

SF test 2

×	ULL		
š	TEP	FUNCT	10N

167	10401104					
			HMS VALUE OF	FERROR		
	2.74	2.10	1.53	2 • 58	2.44	. 55
	2.19	2.00	1.49	1.66	ر 3 و 2 ح	7.16
	1.95	1.90	1.61	1.02	1.96	$1 \cdot 5I$
		1.78	1.72	1.75	1.72	1.71
	1.82	1.66	1.63	1.77	1.54	$1 \cdot 1$
	1.68	-	1.75	1.72	1.59	1.17
	1.76	1.74	1.74	1.70	1.54	1.07
	1.77	1.75	1.65	1.02	1.00	1 - 74
	1.67	1.06	1.61	1.00	1.50	1.7
	1.62	1.62		1.57	1.57	1.06
	1.57	1.57	1.54	1.58	1.57	1.00
	1.60	1.60	1.57	1.09	1.53	1 7
	1.61	1.00	1.55		1.54	1.14
	1.56	1.03	1.06	1.5	1.61	1.00
	1.63	1.02	1 • 02	1.61		1.70
	1 ∙ 5 ธ	1.58	1.57	1.52	1.70	1.0
4 EAN	JF RMS=	1.68				
			TIME ON TAR	GET (SECS))	
	0.06	0.48	1.40	1 • 58	2.20	3.23
	4 • 30	5.29	6.36	7 - 54	7.55	15
	0.10	10.16		12.23	12.41	12.33

MEAN OF RMS=	1.65
--------------	------

		HAT NO SMIT	GET (SECS)	•	
0.00	0.48	1.40	1 • 58	2.20	3.23
4.30	5.29	6.35	7 - 54	7.55	15
9.14	10.16	11.18	12.23	12.41	10.00
14.05	15.03	16.01	17.08	18.00	13.08
20.06	20.98	22.12	22.42	22.64	25.34
24.87	25.88	26.87	27.38	20.95	25.43
30.03	31.02	32.07	33.39	34.07	. 12
36.12	37.10	51.17	59.13	59.35	40.01
41.20	42.33	43.34	44 . 58	45.41	નાહિકના ડે
-	48.42	49.32	43.35	50.32	51.34
47.43	52.37	53.30	54.37	55.42	34. J 1
51.62	57•54	58.54	57.45	59.82	56 • 38
56.51	62.28	62.47	63.18	54.00	51 • 1 c
61.95	07.15	52 · 17	69.13	70.20	71.10
56.15 72.18	73.23	74.25	74.78	75.13	75.31

SF test 3

ROLL STEP FUNCTION

	KMS VALUE	OF LRKIK		
1.94 1.	11 1.20	0.7+	0.06	1.1
1.19 1.	89 2.14	2.05	1.79	1.1
2.00 1.	91 1.82	1.02	1.91	1. 3
1.87 1.	96 2.10	2.31	1.99	1
1.94 2.	03 2.05	1.77	1.98	1
1.95 1.	31 1.97	1.17	1.94	1. 2
1.96 1.	93 1.94	1.93	1.89	1.05
1.93 1.	91 1.91	2.01	2.03	1.30
1.98 1.	96 1.96	1.94	1.92	د ي
2.08 2.	0b 2.05	2.04	2.03	2.62
2.02 2.	00 1.99	2 • UÜ	1.99	2.10
1.99 1.	97 1.95	1.95	1.92	1.1
1.91 1.	91 1.92	1.70	1.59	1. 7
1.80 1.	67 1.85	1.85	1.34	1 - 1
1.83	32 1.81	1. 10	1.80	1.77

		TIAL O'L TA	RGET (DEDS))	
ܕ28	1.29	2.31	3.34	4.34	5 • - 3
6.41	ú.85	7.08	8.09	9.06	• 1
j•83	10.35	11.56	12.91	13.26	1
14.84	15.54	15.58	15.45	17.45	1 " • • "
13.48	19.71	20.40	21.53	22.45	25.43
24.47	25.37	25.34	26 • 43	27.40	2-102
23.47	29.56	30.52	31.52	32.52	31.00
33.58	34.60	35.29	35.25	35.77	30.93
37.08	3 ა. 05	39.07	40.39	41.09	+1 • 7
41.88	42.91	43.62	44.55 .	45.53	45.
40.13	47.21	48.22	49.26	+9.96	20.0
01.33	52.34	o3.34	54.57	55.41	70.13
57.39	50.42	58.54	59.39	00.42	51.42
06.49	53.46	J4.48	€5 • 52	56.51	67.1
pd • 55	67.58	70.58	71 • 50	72.61	73.93

SF test 4

K GI	-L		
3.14	P	FUNC	LION

		RMS VALUE OF	FERROR		
2.79	1.76	1.70	1.47	1 ∙5்∂	1.47
1.11	1.76	2.03	1.33	2.01	↑ • • 1
1.95	1.75	2.69	2.10	∠ • 0 4	1 • 28
1.96	1.96	1.91	1.58	1.84	$1 \cdot 1$
1.89	1.81	1.80	1.80	1.79	1 • 75
1.75	1.73	1.71	1.68	1.65	1 • 44
1.60	1.63	1.61	1.4	1.62	1 • 1
1.00	1.52	1.57	1.56	1.55	1.55
1.52	1.51	1.51	1.49	1.55	1.08
1.62	1.61	1.67	1.00	1.63	1.64
1.62	1.52	1.62	1.51	1.50	1 . 50
1.58	1.58	1.56	1.56	1.50	1.50
1.58	1.50	1.57	1.57	1.55	1.53
1.58	1.56	1.57	1 , 10	1.55	1.54
1.50	1.54	1.54	12	1.52	1. 0

		TIME ON TAR	RGET (SEDS))	
0.15	0.06	1.00	2.01	3.00	4.04
5.05	5.70	n.95	5.65	5.5B	7 - 95
b.11	9.13	9.48	9 . 85	10.31	11.1
12.38	15.04	13.51	14.55	15.56	15.1
16.53	17.61	18.61	19.60	20.65	21.76
22.72	23.67	24.72	23.77	26.75	27.75
28.82	29.79	30.55	31.12	32.13	37.1.
34.15	35.18	3 t • 2 5	37.22	3%.23	51.1
46.27	41.32	42.29	43.33	43.93	44.2
45.27	46.27	46.49	47.23	43.23	4 1 . J.
50.27	51.31	52.31	53.33	4.34	44 موريا
56.56	57.19	58.13	53.73	37.2b	o **• **1
6U.K6	51.92	. 62.91	53. 15	គ្ន•0⊍	65.49
υ 5•20	67.25	68.30	69.17	70.32	71 • 11
72.53	73.33	74.37	75.37	70.41	77 • 4 3

SF test 5

ROLL STEP FUNCTION

		RMS VALJE O	គ ព្រះនាក់ -		
3.1 0	1.37	1.72	1.37	2.12	1.93
1.84	1.47	1.70	1.00	1.61	1.7.4
1.60	1.65	1.63	1.47	1.55	1.40
1.49	1.45	1.46	1.40	1.45	1.54
1.35	1.54	1.34	1.50	1.29	1.53
1.29	1.27	1.28	1.28	1.26	1.77
1.43	1.45	1.46	1.43	1.43	1.92
1.41	1.51	1.58	1.57	1.57	1.0
1.55	1.56	1.53	•	1.52	12
1.53	1.62	1.63	1.51	1.60	11
1.59	1.58	1.67	1.67	1.67	1.70
1.65	1.65	1.64	1.03	1.59	1.01
1.62	1.60	1.60	1.59	1.59	1.7
1.57	1.55	1.56	1.54	1.54	1.53
1.57	1.59	1.58	1.50	1.65 8	1.77
ACAN OF KMS=	1.52				
		TIME ON TAR	GET (SECS)	
0.06	1.06	2.08	3.10	5.06	4 0
5.04	b • 01	7.01	8.03	9.01	· • : 5
13.01	11.03	12.08	13.11	14.03	14.13
16.13	17.11	18.14	19.20	20.20	21.14
22.25	23.22	23.79	24.77	25•59	25-42
27.5s	28.57	29.63	, i . · . -	31.70	51.55
32.53	33.58	34.59	53.34	36.62	31.02
38.60	39.14	39.27	40.32	41.3.1	42.00
43.32	44.51	45.33	46.34	47.3E	4 4 ?
4 3.23	49.23	50.21	51 • 22	52.22	35.17
54.27	55.26	55 • 23	56 • už	ნი•96	50.401
50.99	60.03	61.08	62.11	63•1U	· 4, • ** ;•
65.13	66.13	67.17	စ်စီ • နှင့်	57.20	10.13
71.18	72.22	73.26	74 • 25	75.28	7 - • 23 7
76.72	77.12	78 • u7	78 • 00	72.12	وياداد

SF test 6

KOLL STEP FUNCTION

3 L. 1	1011011011					
			KMS VALUE OF			
	1.13	1.11	2.04	2.30	2.00	1.5
	1.73	1.67	1 • 6 \$	1.53	1.40	1 • • 6
	1.45	1.58	1.67	1.54	1.64	1 - 12
	1.47	1.55	1.57	1.74	1.37	1.,0
	1.75	1.76	1.75	1.72	1.70	4 • 16
	1.65	1.64	1.64	1.01	1.62	1.0
	1.61	1.63	1.57	1.56	1.50	1.02
	1.52	1.51	1.50	1 • 48	1.41	1.45
	1.46	1.45	1.45	1.46	1 • 4 4	1.41
	1.48	1.48	1.48	1 • +5	1.45	1.17
	1.55	1.55	1・5つ	1.55	1.52	1 4
	1.51	1.50	1.50	1.47	1.49	1.40
	1.51	1.53	1.53	1.54	1 • 6 0	1 • > 0
	1.60	1.59	1.62	よっつり こ	1.56	1 • 60
	1.57	1.56	1.55	1.05	1.00	1.04
1 : A	# OF RMS=	1.75				
			TIME ON TAR	SET CSECS)	
	J-21	1.25	1.94	2.18	% •2 6	1 . " 5
	5•2b	6.24	7.23	క• పక	9.51	10• ຮ
	11.33	11.04	12.13	15-16	1 7 • 1 0	14 • 54
	15.65	16.68	17.50	18.10	14.54	19-11
	20.13	21.14	22.10	60.53	23.88	. 4 2
	25.90	26.92	27.94	28 - 18	29.74	30.00
	31.00	31.99	55.05	34 · Jo	55.07	30.00
	3/.10	38.12	39.15	40.15	41.17	42.41
	43.23	44.22	45.22	45.22	47.20	40.4
	44.37	49.54	50.36	o1 • 46	52.41	52.41
	23.13	74.13	55.16	55 • 14	57.15	1: 1 o i o
	59.19	60.19	50.81	61 • 95	52•58	~ 5 • 1 7
	64.52	64.56	65.02	to • 60	oh•92	07.51
	58.33	69.37	70.40	71 • 58	72.37	75.41
	74.45	75.42	70.46	77 • 50	70.40	70.00

SF test 7

ROLL STEP FUNCTION

		KMS VALUE OF	ERRUR		
2.77	1.37	1.93	3 • 01	2.91	. 4
2 • 33	2.46	2.33	2.28	2.17	2.15
2.02	1.99	•		1.96	1.94
1.87	1.88	1.80	1.19	1.80	1.73
1.75	1.77	1.74		1.32	1.05
	1.85	1.04	1.94	2.01	2.00
1.99	1.77	2.00	1.53	1.32	1.40
1.87	1.87	1.85	1.04	1.33	1.
1.87	1.87	1.66	1 • 34	1.02	1.15
1.90	1.90	1.90	1 • 58	1.50	1
1.85	1.03	1.85	1.82	1.73	1.50
1.78	1.78	1.76	1.76	1.75	1.75
1.77	1.78	1.75	1.76	1.76	1.77
1.72	1.75	1.72	1.71	1.70	1.72
1.77	I • 75	1.74	1.75	1.72	1.72
OF RMS=	1.85				
		TIME ON TARG	SET (SECS)		
0.00	0.71	4.654			2.45
3.53	4.51			6.54	1.,4
	2.33 2.02 1.87 1.75 1.89 1.99 1.87 1.87 1.90 1.85 1.78 1.77 1.72 1.77	2.33 2.46 2.02 1.99 1.87 1.88 1.75 1.77 1.89 1.85 1.99 1.97 1.87 1.87 1.87 1.87 1.90 1.90 1.85 1.63 1.78 1.78 1.77 1.78 1.72 1.73 1.77 1.75 OF RMS= 1.85	2.77	2.33	2.77

		IAT NO DELT	ROET (SECS)	
0.00	0.71	1.654	1.08	1.55	2.45
3.53	4.51	5 . 4 1	6.53	b • 5 4	1.14
8.91	9.00	9.71	10.30	11.31	1.1.41
13.33	14.54	15.38	16.39	17.39	1 1 - 59
18.65	16.88	19.46	19 · d5	19.81	20004
21.20	22.25	23.14	23.78	23.27	23.00
24.73	25.69	င်ပ•စ်ဗ	27.74	2 ~ • 75	21.18
50.79	51.79	ತಿವ⊛ಚರ	33.37	34.69	30.12
35.05	35.60	50.70	37.72	35.72	31.00
39.60	37.77	4 • 79	41.79	43.66	45.86
44.85	45.32	46.89	47 . 55	46.12	49.11
50.97	51.99	52.97	53 • 98	54.97	:6.02
56.13	o6•42	57.54	58 • 36	59.42	ક∂ • મ 1
01.47	52.47	53.40	54 - 10	55 . 53	55. 17
56.03	5ۥ50	67.51	60 ∙ √5	5 7.50	70 - 16

SF test 8

4001	
STEP	FUNCTION

		KMS VALUE O	F ERROR		
1.94	1.91	2.82	3 • 25	3 . 0 4	2.3
2.63	2.46	2.34	2 • 23	2.59	2.1
2.49	2.45	2.42	2.35	2.27	2.71
2.18	2.14	2.09	2 • 34	2.01	2.61
2.01	2.02	1.97	1.96	1.9 ti	1 . 1.:
1.89	1.94	2.00	1.78	1.94	1.15
1.94	1.96	1.47	1.92	1.91	1.
1.86	1.89	1.65	1.65	1.03	1:
1.62	1.80	1.80	1.73	1.77	1.75
1.74	1.75	1.74	1 • 71	1.688	1.75
1.00	1.77	1.78	1 • 17	1.74	1.75
1.76	1.32	1.01	1.79	1.79	1.78
1.77	1.77	1.77	1.75	1.75	1.74
1.73	1.72	1.73	1 - 71	1.74	1.73
1.73	1.72	1.71	1.72	. 1.70	1.0

45AN OF KMS= 1.90

TIME	ON	TARGET	(SECS)
1 4 1 1		IMNULI	1.364.37

				•	
0.06	0.54	ម∞១០	0.56	1.15	2.11
ა 1 მ	4.20	5.16	6.21	6.26	12
5.91	7.18	8.19	9.20	10.23	11.0
12.23	13.28	14.26	15 · 28	16.35	17.14
17.19	18.03	19.01	. 3 5	21.05	22.10
23.10	23.54	23.55	24.12	24.07	, e
25.92	26.17	27.18	28.20	29.20	30.27
31.25	31.02	31.93	33 • 38	33.38	34
35.05	36.07	37.10	38.13	5/.12	40.13
40.99	41.49	42.51	43.47	44.48	45.09
45.11	46.13	46.96	43.62	40.01	50.05
50.77	50∙82	51.37	52.30	55.38	34.39
55.42	55.94	50.00	57 • 12	3d.72	5 1 . 74
60.76	61.79	52.78	63.75	63.76	64.13
65.42	00.46	57.40	63 - 50	63.48	73.00

SF test 9

ROLL STEP FUNCTION

**		RMS VALUE C	F ERRUK		
2.24	1.76	1 • ⊃ ಚ	1.40	1.41	1
1.46	1.47	1 • 1 <i>I</i> ,	1.56	1.30	1.52
1.20	1.22	1.25	1.33	1.35	1.003
1.61	1.55	1.52	1.54	1.52	1.71
1.78	1.76	1.75	1.71	1.73	1 - 77
1.76	1.79	1.76	1.76	1.73	1.70
1.70	1.66	1.66	1.56	1.64	1 • U
1.60	1.68	1.67	1.04	1.65	1.05
1.61	1.61	1.64	1.74	1.72	1.71
1.72	1.69	1.69	1.66	1.66	1
1.65	1.63	1.63	1.61	1.60	1 . 1
1.61	1.01	1.61	1.01	1.59	1 . 10
1.57	1.57	1.57	1.55	1.55	1.55
1.54	1.54	1.56	1.58	1.58	1 - 7
1.56	1.56	1.54	1.55	1.55	1.54
MEAN OF RMS=	1.60				
		TIME ON TAR			
0.11	1.14	1.59	2.33	3 • 3 5	4 • 55
4.33	5.31	6.31	7 ⋅ 38	8 • 3 6	7 •
10.56	11.26	11.38	12.34	13.45	15. 4
13.81	14.81	15.88	16 • 36	17.83	10.00
18.33	19.36	20.36	21 • 3)	22.42	35 • 13
22.99	23.97	25.00	25.05	27.05	25.07
29.04	30.12	31.12	32-13	33•10	34.14
35.14	35.13	35.56	th wile \$	37.97	रेड• ≠उ
40.02	41.03	41.73	41 • 72	42.43	43.47
44.51	45.47	46.52	47.59	4 € • 5 3	4
50.61	51.56	52.59	53 • 52	24.64	25 • ≈ 5
55.93	56.56	57.57	58 • 59	5y•66	65.5
61.66	02.63	53.6 /	54.73	á5•á8	56 • /s
67.70	68.77	69.22	69.53	70.58	710
72.58	73.62	74.61	75.61	76.72	75.72

SF test 10

RULL			
STEP	FUNC	ı	LUN

	ł	KMS VALUE O	FLAKUR		
1.12	1.11	1.11	1.30	1.11	5. 4
0.94	1-11	0.94	0.23	1.40	1.00
1.41	1.39	1.34	1 • 38	1.65	1.00
1.57	1.57	1.57	1.47	1.45	1
1.45	1.44	1.45	1.56	1.33	1.45
1.49	1.48	1.47	1.43	1.45	1.1
1.39	1.41	1.57	1.43	1.46	1.42
1.42	1.45	1.49	1.7	1.46	1-95
1.59	1.42	1.41	1 • 44	1.59	1.41
1.41	1.37	1.55	1.36	1.35	1.13
1.34	1.33	1.52	1.03	1.51	1. 19
1.31	1.35	1.55	1 - 34	1.54	1.54
1.35	1.53	1.32	1.51	1.39	4.45
1.44	1.42	1.46	1 - 41	1.41	1 U
1.40	1.41	1.45	1.45	1.44	1.15

		TIME ON TA	RGET (SECS.)	
0.28	1.01	2.00	5.34	4.03	5.11
6.05	7.10	6.13	3.66	9.45	10.00
11.29	12.31	13.31	14.25	14.26	1:.31
15.08	17.03	10.11	19.53	20.15	21.09
22.17	23.17	24.15	25.13	26.19	21.00
27.19	28.23	23.24	30.25	31.27	30.00
33.28	34.33	35.33	35.74	36.52	51.00
35.55	58.39	39.24	40.25	41.27	42.41
45.29	44.37	45.36	46 • 30	47.33	40.000
49.43	50.43	51.37	52.44	55.44	31.18
55.47	56.52	57.49	53.57	ე ∄•ეგ	60.54
61.59	62.00	52.31	0 د و 3 ه	54.52	55.43
66.32	67.42	60.38	69.41	69.50	07.1
70.93	71.97	72.98	73.93	75.01	74.02
77.07	77.57	77.56	78 - 22	19.22	50.00

SF test 11

RULL STEP FUNCTION

RMS VALUE	OF EKKUK		
11 1.57	1 • 11	1.22	1. 0
24 1.34	1 • 56	1.30	1. 4
26 1.01	1.30	1.14	1.11
16 1.11	1.13	1.11	1.41
36 1.31	1.31	1.52	1.51
44 1.43	1.43	1.40	1 - 1
36 1.40	1.58	1.54	1.4
59 1•39	1 • 33	1.35	1.27
53 1.33	1.50	1.32	1.0
27 1.25	1 • ਟਰ	1.26	1.13
51 1.32	1.29	1.30	1 • 1)
29 1.29	1.30	1.24	1 • •
29 1.24	1.25	1.26	1.7
30 1.31	1.29	1.20	1
27 1.27	1.50	i.51	1.50
	11 1.57 24 1.36 26 1.71 16 1.11 36 1.31 44 1.43 36 1.40 39 1.39 33 1.33 27 1.25 31 1.32 29 1.29 29 1.24 30 1.31	11 1.57 1.11 24 1.36 1.56 26 1.71 1.50 16 1.11 1.13 36 1.31 1.31 44 1.45 1.45 36 1.40 1.58 39 1.39 1.53 33 1.33 1.50 27 1.28 1.28 31 1.32 1.29 29 1.29 1.30 29 1.24 1.26 30 1.31 1.29	11 1.57 1.11 1.22 24 1.36 1.56 1.30 26 1.21 1.50 1.14 16 1.11 1.13 1.11 36 1.31 1.31 1.32 44 1.45 1.43 1.40 36 1.40 1.58 1.34 39 1.39 1.53 1.35 33 1.50 1.52 27 1.28 1.28 1.26 31 1.32 1.29 1.30 29 1.29 1.30 1.26 29 1.24 1.26 1.26 30 1.31 1.29 1.26

		TIME ON TAI	RGET (SECS)	
0.30	1.33	2.34	5 · (4	4 • 4 3	9.71
ა.48	6.50	7.51	მ • ამ	9.53	.16. 0
11.58	12.56	13.55	14 - 56	17.65	10.5
17.68	10.71	13.70	20 ∙ 63	21.63	21.05
22.60	23.57	24.59	25.02	20.54	410.7
28.45	20.72	29.77	30.70	31.75	32.77
33.82	34.00	35.32	36 • □ 3	37.83	5 . 10
39.64	39.95	40.93	41.35	42.99	4
45.03	45.38	41.02	40 • 67	49.04	13.60
71.06	52.11	53.13	54 • 12	55.14	11 - 1 C
56.39	57.58	53.4b	53.42	61.47	51.47
62.50	63.47	□4•17	54 • 75	50.70	60.15
01.77	ud•78	65.77	70 • 55	11.73	70. 2
75.52	13.77	74.61	75.78	76.d2	7/. 1
78.67	79.83	80.06	01-21	-1.50	es and

SF test 12

4 JLL				
STEP	FUNC	I	ı	ON

	t	RMS VALUE O	F ERRUK		
4.52	1.37	1.70	2 • 00	1.55	1 - 70
1.57	1-41	1.45	1.51	1.21	1.14
1.25	1-11	1.21	1.21	1.17	1.45
1.37	1.56	1.32	1.34	1.40	1 • • 7
1.33	1 • 4 1	1.36	1.36	1.55	1 - 54
1.32	1.50	1.51	1.26	1.25	
1.25	1.24	1.23	1.25	1.22	1 • :1
1.19	1.24	1.21	1 • 35	1.22	1. J
1.20	1.19	1 • 1 %	1.13	1.10	1. 1
1.24	1.24	1.24	1.25	i • 21	1.1
1.20	1.21	1.15	1.19	1.13	1 7
1.17	1.18	1.25	1 • 26	1.25	2 • ⁵ 4
1.24	1.25	1.26	1.26	1 • 2 5	1 + 700
1.25	1.24	1.24	1.22	1.23	1 • 10
1.22	1.23	1.22	1.22	1.50	1.7

		TIME ON THE	GET (SECS.)	
მ.0მ	1-08	1.71	2.33	3.34	• • • •
5.39	U + 41	7.30	4.45	9.46	200
11.48	12.51	13.48	14.54	10.50	1
16.60	17.68	10.67	13.08	14.67	11.
21.74	22.74	23.78	24 - 74	25.75	2
27.74	28.79	29.83	50 - 54	31.00	ં છે
33.94	34.07	35.94	36. 15	37.93	
40.00	40.58	41.45	42 - 43	73.4.	77.75
43.44	45.46	47.53	48 • 51	49.50	
50.73	51.52	52.57	ექ •ებ	54.57	· • 1
56.58	37.02	38.62	54.04	50.67	* 1 · · 1
62.63	03.72	63.67	44.50	át••⊃2	1 Sec. 4 19 3
67.56	68 - 25	4 8 6 8 3	69 • d1	70.00	11. 1
12.81	73.87	14.93	75 • 95	16.92	37.
73.93	79.98	01-01	b2.01	31.97	52 . S.

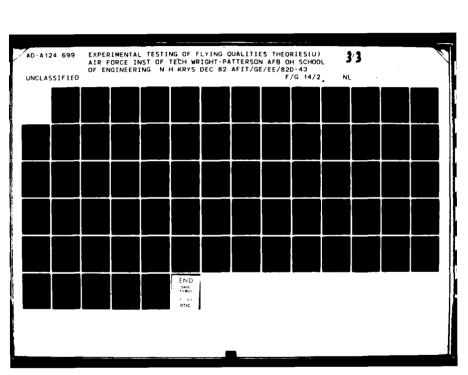
SF test 13

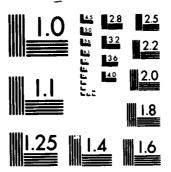
ROLL STEP FUNCTION

	Ŕ.ħ	AS VALUE O	F 1RRUK		
0.00	1.76	0.64	U • 73	હ•્ઇ€	2.01
1.03	0.76	نياد مال	U • 13	ئ • ب ≥	1
0.97	ù•98	1.63	1.4	1.00	J . 1 4
0.98	0 • > 6	1.23	1.29	1.5+	1.50
1.29	1.27	1.45	1 . +2	1.41	1.16
1.38	1.57	1.35	1.51	1.30	
1.29	1.25	1.29	1 • 29	1.54	1.5
1.56	1.55	1.40	1 • 4 2	1.41	1.00
1.38	1.54	1.54	1 • 35	1.57	1.42
1.35	1.34	1.52	1.33	1.51	1.10
1.29	1.30	1.29	1.23	1.27	1
1.20	1.28	1.30	1.27	1.20	1. 7
1.27	1.27	1.25	1 • 24	1.25	1 • 4
1.29	1.28	1.20	1 • 6 1	1.26	4 - +
1.24	1.2ь	1.65	1 • 25	1 - 24	

MEAN OF REST 1.28

TIME ON TARGET (DECS)						
6.43	1.30	2 • 4 3	5 • 4 □	4.40		
6.51	7.54	8 • 54	9.56	10.50	1	
11.94	12.93	13.43	14.91	10.94	1 1	
17.96	13.38	19.50	19.91	26.90	5.	
22.97	24.02	24.15	25 • 19	26.17	. 7.1	
25.18	29.23	30.22	31 • 25	30.21		
34.20	35.27	30.69	37 . 34	37.54	A	
39.52	40.53	40.65	41 • 01	42.63	4	
44.63	45.61	40.03	47 · 03	40.05	4	
53.74	51.74	52.77	53 • 82	54.74	- 1	
55.81	o7.78	58.83	59.03	5.6.84	. 1	
62.32	53.10	54.15	65.17	6 t • 1 2	201623	
68.15	05.17	70.17	71 - 18	72.25	71.1	
73.50	74.47	75.48	76 • 51	77.5€	10.5	
19.52	50.06	81.55	82. 9	95-61	139 - 12	





MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

SF test 14

ROLL
STEP FUNCTION

	P	MS VALUE O	F Edd Jr.		
1.57	1.57	1 - 4 4	1.11	1.11	1. 1
1.62	1.50	i • ¼ છ	1.95	1.23	1.00
1.26	1.26	1.24	1 - 14	1.11	1 - 14
1.14	1.32	1.16	1.11	1.0.	1.63
1-11	1.04	1.07	1.15	1.1.	1.13
1.0	1.09	1.06	1 • ປ່ວ	1.33	:
1.05	1.22	1.22	1.21	1 • 2 1	1. 1
1.13	1.17	1.17	1.15	1.1.	1.23
1 • 2 1	1.15	1.22	1.15	1.22	1.75
1.22	1.24	1.21	1.13	1.20	1.17
1.19	1.15	1.18	1.16	1.1:	1.1
1.15	1.17	1.15	1.17	1.1.	1.18
1.15	1.15	1.14	1.16	1.1°	1.14
1.17	1.15	1.15	1.13	1.1.	1:
1.13	1.16	1.15	1.16	1.14	1.14

MEAN OF RESE 1.10

0.55 1.51

TIAL ON	TARGET (SECE)
4 🗸 చేస్	3.31
7.40	3 • 43
13.56	14

4.51

5.41	೮ 🛮 🖒 😅	7.40	3 • 4 3	4.40	
11.51	12.54	13.56	14 • 50	11.61	1 53
17.56	13.59	19.55	عد • ثغ	21.5:	7
23.67	24.65	25.60	25. 5	21.62	. 62
29.04	50.05	31.39	• 25	53.12	10
35.00	55.22	30.04	. 7 • 12	50 - 14	. 13
40.14	41.22	43.22	43 - 33	4 + 4 1 -	61.1
45 - 09	46.04	47.14	45.12	4 (411	20.13
51.15	52.17	55.15	54 • 72	50.62	2 a . ' .)
57.24	30.26	51.23	s.0 • ∑ :	51.19	14.53
52.55	63.55	64.55	1207	· . (• ·)	* 42.5
58.67	84.0	70.07	70 • (J	73.00	1.415
73.50	75.0?	76.01	77.31	7 5.50	1.54
79.36	30.38	31.59	04 • V	20.37	٠. ~

DS test 1

ROLL SUM OF SINE WAVES FUNCTION

	RMS VALUE	OF EKROF	•		
نہ ف 🕨 ف	U • Û U	1.12	1.4	1 • 51	12
1.11	3.96	1.17	1.16	1.16	1.47
1.02	0.59	1.00	1 . 19	1.11	1.11
1.08	1.00	1.00	11	1.18	1.10
1.07	1.11	1.69	1.07	1.05	1.57
1.11	1.11	1.00	1.00	1.10	1 • 0 ć.
1.08	1.10	1.10	1.15	1.13	1.30
1.05	1.67	1.09	1.11	1.11	
1.07	1.09	1.10	1.10	1.12	1.13
1.09	1.08	1.12	1.0.1	1.10	1.5
1.10	1.11	1.13	1.09	1.10	1.15
1.11	1.10	1.11	1.10	1.13	1.1.
1.13	1.11	1.10	1.10	1.11	1.10
	1.11	1.11	1.13	1.10	1.10
1.11			1.13	1.11	1.11
1.11	1.11	1.13	1017	T # T T	. • • •

	TIME ON TA	RGET (SECS)		
0.33	1.99	2.23	3.25	3	# 6 0
ತೆ85	6 • 88	7.01	1.99	4.03	16.57
11.0ь	12.08	12.46	13.33	13.50	14.01
15.61	15.80	10.63	17.59	1: •43	1 - 4 1
20.40	21.59	22.42	23.50	23.54	34.50
ವರ∗ಶಿಪ	26.25	27.04	28.09	24.12	10.10
51.14	32.09	38.35	32 . 73	33.€3	54.40
3 ສິ • 3 ຄ	35.43	5 u • 58	57 · 12	38.25	57.13
59.94	40.93	41.62	42.22	42.67	41.74
44.73	45.13	46.16	47.18	47.67	40.00
47.58	50.71	51.71	52.50	32.98	54.42
55.02	55.28	55.58	ა6 ₊ ა8	⇒7. 37	5,55 🐇
59.86	60.47	□1.22	62.22	52.56	65.34
54.60	65.32	65.56	ນ້ອ້ • ວິວ	67.60	63.00
63.27	10.28	10.048	71 - 55	72.15	1:+10

DS test 2

HOLL
SUM OF SINE WAVES FUNCTION

RMS VALU	JE OF ERROP	₹		
1.57	1 • 1 1	1.424	1 •	1
1.04	1.17	1 - 1 1	1.00	1 - 11 7
1.11	1.1 F	1.13	1 • 0 ♂	i was
1.05	1.63	1. 17	1.64	1.00
1.05	1.03	1.03	1.05	1
1.04	1.04	0 • 95	1.03	1. 1
1.02	1.07	1 • U b	1.00	1
1.05	1.05	1.05	c 0 • 1	1 . 2%
1.04	1.63	1 • ë 7	1.02	1.
0.96	1.62	1 • 04	1.03	$1 \cdot s \cdot$
1.05	1.10	1.02	1.00	1
1.04	1.04	1.05	1.05	1.1
1.05	1 - 0 4	1.03	1 • 0 4	1.00
1.05	1 - 07	1.38	1.00	1.0?
1.06	1 • Û &	1.09	1.07	$1 \bullet \beta 7$
	1.37 1.04 1.11 1.05 1.05 1.04 1.02 1.05 1.04 0.96 1.05 1.04	1.37 1.11 1.04 1.17 1.11 1.15 1.05 1.05 1.05 1.05 1.04 1.04 1.02 1.07 1.05 1.05 1.04 1.05 1.05 1.05 1.04 1.05 1.04 1.05 1.05 1.05 1.05 1.05 1.05 1.10 1.04 1.05	1.07	1.37

	TIME ON TA	HGET (SECS)		
0.50	0.7 8	1.75	2 . 7 3	3.74	4.76
5.81	6.78	7.64	8 • 40	9.41	10.94
10.69	11.71	12.75	15.71	14.73	1 74
10.81	17.83	18.35	19. oj	20.84	21.
22.39	23.82	24.80	25.10	20.45	27.45
28.48	29.52	29 .9 2	50 • 79	31.79	3: • 29
53.50	34.19	35.22	35 • 24	57.22	45.14
39.22	40.22	41.28	42.26	43.26	4.44
45.28	45.32	47.34	48 • 36	49.41	7
ol•38	ã2.37	53.42	54.38	55.46	50 - 43
57.01	57.54	ან∙57	59.54	50.54	61.54
52.35	63.U7	54.0ំាំ	65.15	50.0u	57.15
63.18	60.68	59 •66	70.70	71.72	7: . 7
73.40	74.38	74.37	75.05	76.06	7/-10
77.91	70.41	74.16	80.18	81.16	17

DS test 3
ROLL
SUM OF SINE WAVES FUNCTION

	RMS VALUE	OF LAKOR			
2 • 4 · ·	≥ •10	2.05	3.03	1.5	44
1.33	1 • 5 □	1.54	1.1	1.11	1 •
1.27	1.23	1.25	1.08	1.18	1.14
1.17	1.22	1.14	1.06	1.10	1.15
1.20	1.13	1.07	1.11	1.07	1.54
1.09	1.08	1.10	1.11	1.05	1.03
1.11	1.14	1.10	1 • 11	1.07	1.19
1.07	1.03	1.07	1.09	1.09	1.5
1.07	1.09	1.03	1.07	1.00	1.00
1.0₺	1.06	1.05	1.03	1.06	۱۰۰۰
1.06	1.07	1.06	1.06	1.05	1.05
1.05	1.07	1.00	1 • Ú 5	1.06	1.00
1.07	1.06	1.05	1.07	1.07	1.07
1.05	1.06	1.00	1.05	1.08	1 • 0 • .
1.05	1.06	1.0€	1.ú7	1.07	1.

	TIME UN TA	RGET (SECS	.)		
0.00	1.13	2.08	5.10	4.13	-13
6.13	7.18	6.19	9.19	10.19	11.23
12.25	13.25	14.31	15.30	16.31	17.51
18.31	19.39	20.36	21 • 45	22.39	23.00
24.32	25.30	26.29	27.33	28.34	2:.15
30.39	31.42	32.39	33.45	34.31	54.57
35.68	36.72	37.48	37.92	38.93	33.91
41.02	42.02	43.02	44.03	45.06	45.07
45.81	47.82	48.63	49.87	56.83	51.3
52 • 86	53.42	54.91	55. 🕫	56 • 92	27.54
58.97	60.02	60.54	61.53	62.56	65.43
64.51	65.53	66.55	57.57	5 5∙ 50	09.45
70.47	71.46	72.10	72.67	72.75	75. 2
74.91	75.95	16.97	78.01	79.00	30.00
aD.90	32.03	32.97	M3 • 71	ყ პ∙ყ 2	54.54

DS test 4

ROLL
SUB-SINE MAYES FUNCTION.

0 • L U	0.00	1.15	1.74	€ • ₹ ?	1. 6
		1.47 ,	الاداد والكسباب	سيلناء أساس	ì •
1.02	0.79	9.91	0.76	↓•3 3	1.01
	3-46	1.00	44.	. 2.92	6 . 7 .
0.97	U • > 7	8.9 8	0.70	(· • 5)	5.00
	<u> </u>	<u> </u>			
1.02	1.00	0.57	0.90	シャラジ	0 → 7%
0.94	0.99	1-35			بساسال جالك با
J.94	0.93	0.97	3.47	9.95	n • • 7
0.95	0-44		. دُدُ مِنْكُ سِي	سيسانا لاحالا	
0.95	0.37	0.9 5	0.96	6.95	3.37
0.95	0_25	3.47	~ <u></u>	. ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ	ىلىنىدا ئ ال ىك ماد ا ئىلىد
0.98	0.96	0.97	3.91	d.95	0 . +4
6.95	<u> </u>	11.39	0.22	. ــــــــــــــــــــــــــــــــــــ	8
0.96	6.77	0.44	9. 96	0.96	Ú . · ·

(1.6)	1.464	(Helification of the Helification of the Helif	•	9.001	
1.010			34 11		11.
ـــــــــــــــــــــــــــــــــــــ	19.00	14.11	15-51	11	
17.61	13.05	19.08	20.08	21.10	22.00
23.14	24.14		25.15	27.13	22.13
29.20	50.20	30.60	31.57	3.2 • ວ ປ	33
14.62	32.62	15.04	37.=3		. 39 4 72
40.72	41.72	42.74	43.79	44.74	45.70
	77.44	48.23	49.14	41244	لل خير المالية الما
51.95	52.46	⊃3 •3₫	53.97	54.99	53.03
-7.15	٠٠١ - ١٥	علقه تلا	2919	_ 5û2.7	ul7
62.28	63.18	63.86	64 - 37	გნ•აპ	ob• '
ω7•8å .	68.55	59.92	20 • 58	71.62	12403
73.62	74.05	75.68	76 • 6d	77.7L	73.71
13.11	34.412	31.75		33-60	

DS test 5
ROLL
SUM OF SINE MAYES FUNCTION

	RMS_VAL	UE OF ERRO	E		
1.11	1.11	1 - 1 1	1.57	2.73	
	1.11	- x + /2	0.41 _		
0.97	1.67	1 • ७३′	1 • હેમ	0.93	1 1
0.99	1.02	1.00	0.10	1.09	V · Phi
0.99	1.02	1.03	1.01	9.45	1
1.09	1.06	1.02	1.04	1.05	1.21
1.02	0.95	1.04	1.02	1.00	1006
1.03	<u> </u>	1.03	1.01	0.99	1
0.99	0.92	1.01	1.00	1.04	1 3
1.02	1.42	1.06	1. 10	Lade	J
1.00	1.00	1.00	1.01	1.01	1.00
1.01	1-03	1.02	1.05	1.03	1.1
1.01	1.02	1.02	1.02	1.00	1.52
1.02	<u> </u>	1.05	1.03	1.00	
1.02	1.03	1.02	1.01	1.02	1.32

	TIAE ON TA	RGET (SECS	•		
 وو	1.29	2.01		3.94	* • 3 °
ა•05	7 - 04	8.08	9.10	10.11	11.14
 19.15	12.33	15.25	14.53	1:.31	
17.33	18.39	19.41	19.35	20.92	21.95
 22.87	23.37	24.42	25.43_	2 = . 4 0	ر د د د
27.54	23.58	29.62	30.54	31.69	52
 . 33.67	34.50	34.20	3559	. 24 و د.2	31.54
33.99	39.98	41.04	41.73	42.55	42.62
 44.52	45.04	45.19	45.73	4 <i>L</i> _59	4.,7.
49.74	5 0∙77	51.76	52.78	55.48	54.47
55.52	55.34		57.19	5:421	. Ca• /b
59.96	51.01	61.71	52.57	53.77	14.77
 65.75	56.63	66.95	67.43	5.2 .4.6	27.17
 71.05	70.61	71.63	72.40	73.37	14.40
 75.08	75.81	76.85	77.51	7 2 . 8 3	7 • • •

DS test 6

ROLL SUM DE SINE JAVES FUNCTION

المعارض والمستحدد والمستحد والمستحدد والمستحد والمستحدد والمستحد والمستحدد والمستحد والمستحدد والمستحد والمستحدد والمستحدد والمستحدد والمستحدد والمستحدد والمستحدد وال	KAR AFF	UE OF Enach	h		
1.1	1.11	$v \bullet v 1$	1.85	1.5	1.51
1.11	1.44	المالية الوشيطية المالية	1 م . تان	ت کی میلاسید ۔	1
u•97	1.03	1.03	0.5%	1.14	1.11
<u>le0</u>	1.56	0.94			J • 16
0.94	1.00	0.93	0 • ∀a	1.01	1.01
1.91	1.00	<u></u>	3	0.00	0.
1.00	0.52	J . 15	0 • Yé	0.93	9 . A. T
0.96	1079	1.01		1.00	. 1.21
J•99	0.77	1.01	1.00	0.93	J • 95
1.00	1.44	1.66	1.40	., Jagg.	2.07
0.94	0.98	0.99	U • 13	5.97	U • °
1.00	1.10	0.95	4 • 22	v+27	↓ •
3.97	0.98	1.01	1.00	u • 97	6.
3.99	0.79	0.98	9.51	3 •2.7	♥・
0.96	0.77	0.77	0.79	0.50	* •

TIME ON TARGET (SECS)

U • Q • <u>u</u>	<u>2.83</u>	1.60	2.023	3.2.4.	· •
5.61	6 • 6 O	7.25	b • ?)	+•2n	11.
11.55	12.35	12.20	14.00	المستشرف المسا	19.
17.00	10.35	19.00	20.14	21.12	22.00
23.10	24.12	دُخوند	25 2	24.60	27.
28.62	29.55	30.64	31.58	50.75	ن غ . 7.
34.73	32.24	<u> </u>	37.32	\$1.025	34400
39.43	40.47	40.77	41.79	42.37	43.70
44.82	45.56	45.94	46.24	47.97	479.0 3 4
49.97	51.01	52.02	53.04	74 · 04	55.00
<u> 3 p • 0 b</u> .	ــــــــــــــــــــــــــــــــــــــ	<u></u>	59.12	ر 15 و تا د	21.13
62.13	63.15	64.20	₽⊇ • 55	5 å • å c	⊌ 7. ∵?
	84.UB	7 u.• u.u	70 • 43	71.46 .	72.55
72.73	73.68	74.60	75 • 04	70.72	77.12
13.72	77.17	ა ⊍.7 8	61.75	_32. <u>15_</u>	5.7

DS test 7

ROLL SUM OF SINE WAVES FUNCTION

	RMS VALUE OF ERROR						
1 • • •	1.11	1.45	J . Jt	1.12	23		
1.57	1.54	1./3	1./.	1.7.	1.75		
1.74	1.75	i - 78	1.62	1.62	1 . €		
1.69	1.72	1.66	1 • 04	1.64	1 • . 7		
1.64	1.65	1.57	1.00	1.62	13		
1.7b ·	1.79	1.75	1.74	1.71	1.75		
1.74	1.76	1.73	1.79	1.70	1.7		
1.74	1.78	1.60	1.75	1.77	1.17		
1.75	1.16	1.75	1 • /1	1.73	1.74		
1.74	1.74	1.73	1./4	1.75	i./7		
1.76	1.75	1.74	1.74	1.70	1 • 7 2		
1.77	1.77	1.77	1.74	1.74	1-14		
1.76	1.75	1.73	1 - 71	1.72	1.74		
1.76	1.79	1.76	1.76	1.77	1		
1.75	1.77	1.77	1.76	1.74	1.7.		

	TIME ON TA	ARGET (SECS)		
0-45	1.19	1.9੪	2.94	3.93	••55
4.74	4.78	5.13	5.33	હ•0∂	1
n•87	7.73	ა • 3 3	7.34	1.76	10.01
10.38	10.54	11.45	12.51	12.74	1:.5
13.30	14.31	14.58	15.50	10.56	17.15
17.03	17.70	18.71	19.70	20.30	20.00
20.77	21.45	22.52	23.16	23.95	2+.13
24.42	24.48	25.20	25.73	26.39	30.44
26.93	27.27	28 •28	29.29	30.32	34.15
30.88	30.82	31.65	32 • ამ	32.54	34.43
55.57	34.05	54 • 5B	35.13	55.43	30.73
35.85	36.22	ქა •ხი	37.73	38.40	50 . Se
39.10	46.10	40.58	41.29	42.31	43.17
45.13	45.44	44.47	45.12	45.76	40.77
46.29	47.09	48.16	49.14	50.12	50.10

- DS test 8

COLL SUM OF SINE WAVES FUNCTION

	RMS VALUE	OF ERROR			
1.15	1.12	U . a 4	1 . 24	1.3.	0.29
1.48	1.30	1.37	1 • 5-	1.40	i • ·-
1.34	1.56	1.26	1.59	1.50	1.43
1.53	1.47	1.51	1.50	1.56	1. 7
1.56	1.56	1.57	1.53	1.56	1.00
1.55	1.51	1.46	1.55	1.51	1.05
1.57	1.55	1.53	1.56	1.54	1 • 54
1.54	1.54	1.52	1.54	1.54	$T \leftarrow i \mathcal{E}$
1.52	1.48	1.50	1.52	1.52	1 • 9 5
1.54	1.56	1.57	1 • pá	1.54	î • ° €
1.55	1.54	1.52	1.53	1.52	1.00
1.52	1.52	1.52	1.01	1.53	1.00
1.54	1.52	1.52	1.50	1.51	$1 \cdot 1$
1.49	1.50	1.49	1 • 56	1.50	1.00
1.49	1.48	1.48	1.48	1.45	1.90

0 4.	1.13	KGET (SECS 2.09	2.43	3.01	• 25
0.55 3.85	4.38	4 • 83	5.31	5.83	0.41
6.91	7.94	გ. ეე	→•21	9.18	ラ・ラウ
10.48	11.18	11.71	12.34	12.29	10.44
12.96	15.08	14.21	15.23	15.34	1: • . 5
16.54	17.65	18.33	18-28	16.76	$1 v \bullet v v$
19.25	19.85	19.95	21.02	21.45	21 • 13
22.49	23.54	24.53	24 - 15	≥5.39	26.45
25.87	27.88	28.09	23.62	26.94	2000
27.62	30.03	30.32	31 - 27	51.30	51.
32.69	33.70	34.47	34 - 47	35.32	35.75
36.45	37.22	37.62	57 • 98	38.23	53.15
59.18	39.17	40.82	41 • 79	413	
43.02	43.99	44.02	45.14	45.94	46.435
45.52	47.53	48.56	48.96	49.37	50.54

DS test 9

RILL SUM OF SINE WAVES FUNCTION

	RMS VALUE OF ERROR					
1.15	0 . 0 U	J • 41	£ •97	1.11	. • _ 0	
1.03	0 • a3	0.37	1.2	1.16	المام ا	
1.07	1.22	1.17	1.11	1.14	1.14	
1.08	U • 17	1.11	1.18	1.25	1.11	
1.07	1.09	1.00	1.11	1.09	1.44	
1.09	1.09	1.13	1.06	1.06	1 - 15	
1.05 1.0b	1.10	1.10	1.08	1.0€	1.10	
1.03	1.07	1.05	1.66	1.06	د . ۱ •	
1.05	1.05	1.05	1.08	1.008	1.57	
-	1.03	1.00	1.07	1.05	1.	
1.04	1.04	1.07	1.08	1.0 ≡	i su:.	
1.05	1.08	1.00	1.02	1.00	1.06	
1.06		-	1.04	1.07	1.04	
1.05	1.04	1.04	- -			
1.06	1.00	1.04	1 • ປວິ	1 • 0 C	1 - 95	
1.06	1.06	1.00	1 • 48	1.00	A # 40 to	

	TIME ON TA	RGET (SECS)		
0.90	1.29	2.23	2 • 4 5	5.44	1 4 4 4
5.25	5.99	6.15	7.19	ۥ16	• •
1.23	10.84	11.91	12.15	13.00	15.00
14.90	15.78	15.99	16.71	17.71	1 - 11
19.71	20.72	21.74	22.75	23.77	34-37
25.75	20.34	27.82	29.60	27.77	30 • ⊃
51.85	32.50	33 - 53	33 ⋅ 88	34.95	***
30.90	37.95	30.80	3ઇ•97	33.97	45.49
41.41	42.18	42.68	43.72	44.26	45.11
46.13	47.14	47.74	48 • n9	41.91	50.45
51.92	32.82	53.38	53.31	54.72	1
56.11	56.79	57.77	58 • 18	59.61	$0 \cdot 1$
61.87	62.87	53.80	64.91	65.32	500
57.38	p8.17	58.52	69 - 30	57.60	70+03
71.26	72.02	72.70	72 • 65	75.91	14. 12

NO test 10
ROLL
SUM OF SINE WAVES FUNCTION

	RAS VALUE OF ERROR						
1.1 :	1.77	1.44	1.47	1.0.	: • 1		
1.11	1.30	1.17	1 • . 1	1.06	1.4		
1.19	1.11	ۥ99	1.04	1 • 1 4	1.01		
$c 0 \bullet 1$	1.05	1.03	0 • 93	0•96	$1 \cdot v 1$		
0.97	1.02	1.00	1 • 01	0.99	1		
0.98 .	1 • ú 0	0.99	0 • 11	U•93	J. 4		
3.97	0.97	3.9₺	0.43	0.98	u • · ∙ 7		
0.99	0.98	1.01	0.97	0.97	5		
0.94	0 t . 0	0.95	0 • 37	0.94	U • ² ↔		
0.94	0.75	86.0	0.09	36.6	O . 4		
U.97	0.97	0.93	0.36	U•77	5 . 35		
0.96	0.95	0.35	0.92	0.96	1. 12		
0.96	0.57	0.95	D • 94	û•96	5.75		
0.94	0.95	ٕ9E	0.97	5.97	∪ - :4		
0.96	0.95	0.95	v = 4	0.25	J . · •		

MAN OF RMS= 0.96

	TIME ON TA	RGET (SECS)		
0.94	1.14	2.13	3.16	4.00	: 3
3.45	6.51	n •94	7.93	5.99	9.4
10.98	11.79	15.00	14.00	1 % . 6 6	1 - 100
17.01	10.03	19.05	20.03	21.05	ن د د د ک
23.12	24.10	25.10	26.09	27.12	2 0
29.09	50.10	30. 93	31.42	32.84	5 '• ĵ
34.85	35.84	30.85	37 • მ0	೨೭•88	55
40.54	41.52	42.54	43.52	44.53	45.35
46.57	47.52	48.61	49.79	50.32	31.12
52.09	53.11	53.74	51 • 77	59.79	35.18
57•81	53.22	59.23	50 • 26	51.26	52.32
63.23	64.52	65.13	a5•70	21.071	5/1/1
60.70	64.72	70.83	71 - 73	72.75	12.16
74.77	75.80	76.60	77 • 27	7 5 • 3 1	79.00
d0.33	81.58	82.54	83 - 34	84.43	35.41

DS test 11

RILL SUM OF SINE WAVES FUNCTION

	NMS VALUE OF ENROR					
ម•ជ≎	1.13	4.44	0.1	1.	• 4 5	
0.75	1.64	9.50	↓ • ↑ *	1.000	1 - 11	
1.07	ひ・フロ	りゃりち	V • 96	0.3∃		
0.99	1.02	0.97	9.45	1.01	J 🔒 👊	
3.99	1.00	0.91	9.74	₫•99	L 7	
0.96 ·	1.04	0.97	J•⇒7	ひ・ラバ		
1.00	0.99	1 - 04	0 • 78	1.00	1 . 11 .	
J • 47	3ۥ0	リ・フィ	ਹ•ਖੜ	0.97		
0.9 8	0•98	0.95	1 • 00	3 . ***	J. 🕶	
0.93	J • ₹7	0.90	3. 19	b • ₹ 5	5 . 1 I	
1.00	0 • ∮8	0 • 98	មិ∝ាំខ	1.44		
1.00	J•97	0. ∀5	9. 7	ପ୍•ୁଖର		
0.98	0.98	0.98	0 - 96	5 •9 ≥	J. • 7	
0.99	0.46	U • 97	₫ • ₹3	4.37	J + ++	
0.97	0.97	0.98	8.75	ម•ាខ	J. A.	

MHAN OF RHS= 0.98

	TIME ON TA	RGET (SECS	•		
1.00	1.90	2.40	3.50	4.44	. 4 5
J • 15	6.60	7.600	8.06	9.21	* · · · ·
11.26	12.24	15.29	14.53	15.29	1 . 9
17.33	18.54	19.33	20.39	23.74	1.
22.64	25.59	24.50	25.64	25.54	_'. 7
23.03	28.78	29.00	≠ 50 • u3	31.4U	30 . 42
33.40	54.43	50-47	36.47	37.53	• • •
39.14	39.45	41.02	41.73	45.85	44.
45.03	45.37	46.16	47.13	4%.13	• •
50.22	51.26	52.22	53.16	34.02	29.01
55.52	5u • 58	57.53	58.09	ວ ປ•ວິຊ	
51.27	o2 • 32	ú3•30	54.97	81 • 4 د	
06.82	57.53	55.86	69.45	70.55	12.7
7.2.85	73.00	74.67	75.67	75.58	17.00
78.73	77.72	50.72	31.30	52.79	ερ. • ∀U

DS test 12

RULE SUM OF SINE WAVES FUNCTION

	RMS VALU	E DF EKKU:	₹		
1.5	1.5)	1 • 4 4	1 . * .	1.11	. 1 -
1-1-	1.11	J . J .:	1.	1.01	$z \cdot 1$
1.25	1.05	1.67	U • →2	0.97	1. 1
1.02	1.02	1.03	0 • 110	1.01	
0.94	1.00	1.05	0.12	1.01	7
0.98	0.94	0.93	0 • 93	U.96	in 🛊 👍
U•91	0.95	0.54	0 . 1.	J • 97	U • •
U.95	0.98	0.94	0.94	ŭ.94	.
0.92	0.70	6.96	3. 14	5.45	4 بان
0.95	0.44	6.95	0 • JS	J • 17 4	L.
0.95	0.91	0.93	0.12	J • 50	J . ' '
0.90	0.74	0.12	0.06	0.75	∪ . ந
0.95	0.95	0.92	0.74	3.52	2 • · · •
0.43	0.75	0.95	Ú . 14	0.9 4	5.12
0.93	0.72	J.93	0.94	0.75	U • 1.

	TIME ON TA	RGET USECS	•		
0.5 *	0.65	1.54	2 • 65	3. 5 ⋅	14/4
5.40	u • 41	7.44	8.45	9.55	10.47
11.50	12.51	13.51	14.54	15.35	15.00
17.45	18.46	19.48	20.49.	21.45	2.00
23.52	24.57	25.∙58	20.57	27.60	23.00
27.52	30.63	31.02	52.70	33.67	5 + 4 7 3
35.72	36.74	37.77	38 • 83	5 m • 5 1	5 1 . + 5
40.87	41.89	42.92	43.54	44.70	41.4
40.489	47.59	40.97	50.02	01.04	12.6
55.07	54.02	55 . 0∺	56.12	57.11	50.17
59.37	59.43	սն•39	51.43	32.48	13.47
64.46	65.48	66.52	67 . 53	53.51	51.05
70.58	71.56	12.02	73.32	74.61	7. •
7 ნ ∙ 58	77.17	78.10	79.29	30.26	1.17
81,29	45.50	34 - 34	45 - 34	20.25	. 7

DS test 13 HOLL SUM OF SINE WAVES FUNCTION

	RMS VALUE	- JF EKKUK			
1.1	⊍•7 5	1.4.	5.77	1.31	. 11
1-11	1.10	0.000	0 • 3 •	1.0€	و يال
1.07	0.98	1.08	3.75	1.01	□ • +1
1.05	0.95	0.47	0.75	U • 73	J. 9
0.99	1.07	ù •93	0.96	1.05	1.05
0.91 .	0.94	0.95	0 • 95	1.03	U • 15
0.95	0.95	0.97	0.31	0.35	U 🕳 .º 4
0.91	0.45	0.44	3.75	ٕ97	3.52
0.92	0.93	0.95	0.91	0.94	t. 4
0.94	0.43	u •95	0 • ±3	ù•93	3.03
0.95	0.54	0.71	0 • 58	0.91	3 🗸 🖰
0.95	0.92	0.93	0 • 93	0.94	ن . ن
0.94	0.92	J.75	0 • 95	0.94	J. +2
0.93	4 د ۵	0.92	Ú • 45	6.94	. 4 و د
0.95	0.34	0.94	0 . 12	6.93	

HANG OF RMS= 0.94

	TIME ON TA	ROLT (SECS)		
0.08	1.19	2.13	5.20	4.21	• 1 3
6 • 23	7.24	8 • 25	9.25	10.23	11.51
12.30	13.54	14.00	14.55	10.05	1
17.85	13.88	19.91	20 • ⋴₿	21.33	ر 🕹 کے
25.33	24.35	25.34	26.37	27.44	å: • • • 0
29.42	30.45	31.52	32 • 45	33.49	39 € <i>2</i>
35.45	36.49	57.54	38 · 54	37.54	رڙر ۽ ڏ ٻ
41.61	42.61	43.44	44 . 67	45.54	4 % . 3
47.64	40.06	44.66	50 - 75	91.69	2 15
55.76	54.78	55. 7 □	55·78	57.81	J 🕠 🕶 💆
57.81	ა0•87	51.03	ස2 • පජ	53 . 47	a * • 3
65.66	56.13	67.65	60 · 68	62.70	16. 7
71.71	72.73	73.70	74.72	75.77	10.10
77.80	7៦.៩0	79.83	80 • ಆ7	31.33	5 D 🐷 🔧 🕖
35.91	34.92	85.89	85 - 12	გ7•მნ	50 · 15

MK test 1
RILL
SUM OF SIME WAVES FUNCTION

	RAS VALUE OF EFROR					
1.1.	1.56	2.62	1.47	1.30	7	
1.57	1.52	1.05	1.49	1.20	1.7	
1.34	1.42	1 • 37	1.35	1.29		
1.50	1.38	1.41	1.51	1.51	1 • • 5	
1.33	1.34	1.30	1.51	1.32	1	
1.50 .	1.31	1.28	1.50	1.50	1 * : I	
1.50	1.55	1.34	1.33	1.37	1.	
1.57	1.40	1.59	1.58	1.41	1.17	
1.57	1.43	1.44	1.43	1.44	1 1	
1.65	1.70	1.67	1 . 59	1.67	l · B	
1.66	1.68	1.69	1 • 57	1.68	1	
1.67	1.08	1.67	1.58	1.67	1. 5	
1.67	1.68	1.71	1.70	1.67	1. 7	
1.70	1.75	1.75	1.73	1.72	7 - 13	
1.72	1.71	1.72	1.76	1.81	1.7	

	TIME ON TA	RGET (SECS)		
0.61	0 • ♂♂	1.25	1 • 25	2.20	• 1
2.98	3.99	⇒.01	6.33	7.05	1.71
4.40	8.51	y . 08	10.55	11.65	1
12.59 .	13.08	14.01	14 • 35	15.21	13. š
17.31	17.81	13.28	19.49	20.33	24.54
21.63	22.28	22.52	23.55	24.58	25.0
20.93	26.50	26.59	27 • 20	27.22	21.
27.07	28.13	29.15	30.18	31.15	30
52.67	32.70	35.22	34.04	34.63	44 🕶 :
34.57	34.32	35.15	35 • ∂3	51090	: • • 3
33 .87	38.88	39.35	39.44	40.25	40.
40.84	41.52	42.14	42.17	+2.17	42.77
45.54	43.74	43.95	45.03	45.64	4 7
46.76	46.86	47.82	48 • 37	4 2 • 8 1	·, 0 • · -
50.31	51.86	52 . 27	52 - 25	5 22	28.

ROLL SUM OF SINE WAVES FUNCTION

	KH2 AAFAF	JE ERRUK			
1 • • •	1 • ti 0	1 • 2 5	1.7,	1.51	
1.11	1.0	1.3	1.17	1.16	1.11
1.15	1.15	1.11	1.21	1.29	1 - 05
1.55	1.51	1.08	1 - 52	1.27	L • 50
1.44	1.44	1.46	1 . + /	1.44	1.47
1.48 .	1.49	1.47	1 • 45	1.45	4.95
1.41	1.43	1.44	1.42	1 • 4 1	1.47
1.42	1 - 41	1.39	1.39	1.59	1.50
1.41	1.38	1.36	1.37	1.37	1.41
1.37	1.37	1.33	1.59	1.3€	1 - 7
1.38	1.38	1.38	1.58	1.37	1 7
1 • 3 d	1.37	1 • 4 1	1 • 5¢	1.57	1.57
1.58	1.56	1.58	1.58	1.57	1.18
1.38	1.53	1.34	1.50	1.37	1 + 1 5
1.36	1.35	1.54	1.55	1.54	1.5

0.54	1 • 1 4	2.19	3 • 20	4.23	٠.45
5.43	6.45	7.59	4 • 51	ઇ•9ા	1
10.25	10.98	11.95	12.45	12.91	1:.1 =
14.25	14.93	15.33	15 • చేర	1 n • 9 8	17.00
17.48	17.94	18.94	13.98	20.18	20.15
21.19	21.48	21.92	22 . 34	23.52	6 T + 1 T
24.80	25.77	26∙78	27.64	2 (• 32	2 5
2 9 • 13	50.07	31.00	32.09	33.03	37.42
34.14	34.37	35.37	35 • ≥0	34.632	: 7.00
37.85	38 • B8	30.97	39 • 57	40.21	والمناسبة
40.88	41.74	42.76	43.17	44-74	H 1 → +4
45.47	45.71	46.37	46.12	47.91	4 . 5
43.86	45.79	50.78	51 • 51	o 2 • 12	· · · · 1
53.13	od.78	54.73	ઇ5.1સ	55.11	11-12
57.72	50.21	54.22	60.69	6∂•0a	50.4

MK test 3

HOLE SUM OF SINE WAVES FUNCTION

	RMS VALU	E OF EXRUR			
3.00	1.11	1.43	U • 🤈 🖡	1.4U	1-11
1.1	リ・プロ	1.17	1.00	1.11	1.00
1.15	1.11	1.11	1.37	1.34	1 • • 5
1.11	1.11	1.16	1.13	1.11	1 - 4 5
1.05	1.13	1.15	1.09	1.11	1.11
1.11	1.22	1.00	1.09	1.11	1 • 1:00
1.04	1.12	1.11	1.08	1.00	1 - 12
1.11	1.12	1.10	1.12	1.12	1 - 11
1.11	1.13	1.13	1.12	1.09	1.18
1.14	1.12	1.13	1.10	1.15	1.1
1.16	1.16	1.13	1.10	1.14	1. ')
1.20	1.19	1.20	1.21	1.21	$1 \cdot 1$
1.21	1.21	1.19	1.19	1.20	1 • U
1.21	1.31	1.26	1.21	1.20	1 1
1.20	1.20	1.21	1.19	1.21	1 -

	TIAC ON TA	RGET (SECS)		
0.44	0.84	1.55	2.3₺	ن• 4 l	4.5
5.39	6.48	7.46	5.01	̕9 ti	•
10.80	11.76	12.50	15.59	14.01	14.00
15.54	16.31	10.39	17.53	13.40	1 1 1
20.15	21.22	21.52	22.52	23.54	2 4 4 4
25.59	26.09	27.03	28 • 05	29.13	13.17
_	31.37	32.17	53.10	34.05	55.
30.68	32.38	35.93	37.49	38.41	33.
34.93	40.78	41.62	42.37	4 H 8	43.00
40.42	= · ·	45.08	45 • Y.3	40.78	47. 3
44.56	45.14	47.64	48 • 07	43.74	4 15
47.62	41.58		52.48	51.61	53. 5
49.71	4 ن • 0 ق	51.74		57.83	2 3 •
54.62	55.67	jo•67	57.75		
oJ•53	60.54	61.29	61.41	62.47	65.44 ≤
64.47	65.47	96.48	67 ∙ 52	57.65	~? • · · *

MK test 4

RULL
SUM OF SINE WAVES FUNCTION

	RMS VALUE OF ERROR					
1.7	1.11	0.00	0.7.	1.11	. J. C	
1-11	1.11	1.1/	1 • • 6	1 • < 1	ل '' د د	
1.54	1.15	1.15	1 • 21	1.17	1.11	
1.11	1.14	1.15	1 • 13	1.16	1.414	
1.15	1.11	1.17	1 • 13	1.15	1.13	
1.11 .	1.15	1.12	1.11	1.11	1.05	
1.14	1.14	1.14	1.14	1.11	1.11	
1 • 8 á	1.12	1.13	1.11	1.12	1.12	
1.10	1.09	1.11	1.35	1.13	1.17	
1.13	1.15	1.09	1.15	1 - 1 1	1.10	
1.15	1 • 1 4	1.15	1.13	1.15	1 - 1 4	
1.12	1.15	1.13	1 • 11	1.12	1.44	
1.12	1.12	1.12	1 • 14	1.14	1.14	
1.13	1.13	1.12	1 • 11	1.1	المتأسب	
1 • 0 7	1.13	1.11	1.12	1.13	1.1.	

	TIME ON TA	RGET (SECS	.)		
0.70	1.80	2.7€	2.93	3.61	والمراج والمراج
5.68	5.73	14 · 3 to	5 • Ju	7.40	1.
<pre>>.01</pre>	10.01	10.55	11 • ° b	12.24	1: • 1
14.24	15.26	16.631	17.53	19.33	1 . 14
18.96	17.76	20.37	21 • 39	23.03	;° - • , ⊲
24.87	25.88	25.07	27.58	23.54	2
29.97	30 • 77	32.04	53 · J5	35.75	5
34.98	35.33	36.23	37.15	33.17	33.42
59.92	4J• 9 8	41.94	42 - 46	42.54	43.09
44.59	45.52	46.01	47.52	40.63	4 . 3
48.83	+9•82	58 ⋅ C c	51.51	52.38	3. • . •
54.41	55.42	ა ნ •38	57 • 38	57.67) · • • • •
59.42	5U•48	61.54	61.54	£ & . 5 €	3.5.92
64.50	55.55	06.53	65 • 03	57.86	13.5 4 2.5
39 .91	70.72	71.96	72.18	73.90	$I_{\rm color} \sim 20$

MK test 5

ROLL SUM OF SINE WAVES FUNCTION

	HMS VALUE OF EHROR					
3.23	2.73	1.61	1.55	100	. 1.	
1.7:	1.7	1.57	1.43	1 • 4 5	1. 3	
1.41	-1 - 36	1.57	1 • 50	1.29	1.15	
1.30	1.29	1.26	1.29	1.29	1.	
1.23	1.27	1.20	1.27	1.25	1. 19	
1.26 .	1.24	1.25	1.25	1.28	1	
1.24	1.25	1.27	1.24	1.25	1	
1.21	1.24	1.25	1.31	1.20	1 3	
1.20	1.22	1.22	1.22	1.23	1 1	
1.23	1.19	1.21	1 • 13	1.20	1 🚅 🥖	
1.20	1.19	1.18	$1 \bullet 1$	1.18	1-19	
1.19	1.18	1.20	1.15	1.13	i • 4 l	
1.17	1.19	1.19	1.13	1.11	1.1	
1.18	1.16	1.17	1.17	1.1:	1 • 1 :	
1.17	1.16	1.16	1.17	$1 \bullet 1 \oplus$	1.14	

	TIME ON TA	RGET (SECS)		
0 • 0 t.	0.14	1.14	2.16	5.21	O 1
>•05	05 و ن	7.04	7. 26	5.14	• 1.1
10.14	11.18	12.18	12.31	13.34	1 :
14.70	15.73	16.69	17.74	17.95	18.00
14.55	20.58	21.59	22.60	23.60	24.33
24.43	25.10	25.13	27.14	27.68	23.5
29.00	50.00	31.05	32.03	32.54	13.24
33.82	34.90	35.88	36 • 55	37.00	37 w . u
3 1.07	40.05	41.02	42.J6	46.44	45.17
45.88	44.15	45.19	46 • 18	40.35	47.17
43.27	47 - 58	50.41	51.42	52.44	56.42
94.34	ວ່ວ•11	55.97	57.02	57.54	27.72
50.71	59.74	ь0.77	61.75	52.78	30016
64.52	55.50	66.55	67.15	67.35	00.00
54.07	39.67	7 ú • ú 7	70 • 87	71.+1	7' • 1.'

MK test 6

ROLL SUM OF SINE WAVES FUNCTION

	Ri	4S VALUE 01	F ERKJM		
0.00	2.25	1.70	1 • 48	1 • D &	1.17
1.33	1.18	1.23	1.52	1.20	1 - 4
1.27	1.19	1.25	1.21	1.14	1 3
1.17	1.24	1.15	1.10	1.11	1.1
	1.13	1.11	1.11	1.13	1.15
1.16	1.11	1.15	1.11	1.16	1.11
1.09	1.11	1.10	1 • ប្ន	1.08	1.37
1.10		1.07	1.38	1.00	1.05
1.07	1.07	1.05	1.10	1.00	1.07
1.08	1.09		1.05	1.07	1.35
1.07	1.09	1.05	1.37	1.04	1 + 34
1.07	1.06	1.07		1.00	1.14
1.05	1.06	1.06	1.03	1.0b	i.)
1.05	1.05	1.06	1.04	1.03	1 • 2 4
1.06	1.05	1.05	1.35		1.15
1.05	1.06	1.05	1.57	1.05	• • •

TIME ON TARGET (SECS)								
0.95	0.98	1.63	2.40	3.65	to a talk			
3.64	6 • 4 5	b•8U	7.55	5.685	1.5			
10.61	11-40	12.25	13.24	14.25	19.40%			
16.23	16.45	1 d • 01	18.99	20.01	بالانتان			
22.02	23.05	23.57	24.10	25.00	r_{2} . 12			
27.12	28.17	29.14	30 - 14	51.08	3. • 2.3			
35.17	34.15	35.10	46.70	57.20	24. • 22			
39.23	40.22	41.24	12.26	43.23	44.25			
44.94	45.61	46.57	47.51	40.61	4 🐪 👶			
50.66	51.67	52.67	93 • 59	54.65	20.00			
26.67	57.66	აყ•74	59.72	SU.71	1.75			
62.71	63.72	64.73	65.76	55.75	57.77			
58.80	69.81	70.80	71.23	12.21	71.27			
75.63	74.62	75.63	76 • 52	77.62	7 .02			
79.63	30.61	31.7U	82.47	35.71	39.71,			

ML test 7

RULL SUM OF SINE WAVES FUNCTION

	HMS VALL	JE OF ERROI	٠,		
3.00	1.75	1.7	1.47	1.1.	1
1.5)	1.57	1 • • 1	$1 \bullet I^{\circ}$	1.55	. 1
1.90	1.85	1.85	1 • So	1.43	1 7
1.85	1.76	1.96	1.19	1.95	1.
2.01	1.93	1.42	1.58	1.92	1 . 2
1.86 ·	1.91	2.05	2.02	2.00	17
1.99	2.02	2.00	1・リブ	1.9 c	1 + c
1.95	1.93	2.01	2 • J3	2 ⋅ 0 ≥	• ?
2.05	2.03	2.07	2.01	2.02	7. C
1.96	2.00	2.00	2 • #3	2.02	1.02
2.02	2.02	2.01	1.99	1.94	1
1.98	2.00	2.06	2.15	2.03	* 5 *
2.02	2.01	2.62	2 • u 1	۱) ل و د.	1 · 3
1.99	1.79	2.07	2 • ∪3	2 • 0 7	1.7
2.06	2.05	2.05	2 • úp	2.005	1.00

	TIME ON TA	RGET (SECS)		
0.58	0.73	1.11	1.99	2.55	5 🐧 🖓 🤫
5.50	5.60	3.96	4.46	4.45	4.42
4.46	5.45	5.57	6.09	5.05	• *
7.96	7.36	B.23	8 • 25	··• 2 6	10.15
10.14	10.60	10.93	11.5	11.65	12.70
12.89	13.28	13.25	13.99	14.35	10.54
15.79	15.77	15.25		17.46	17.05
18.90	19.38	19.58	1 . 73	23.51	29. :
20.77	21.14	21.55	21.37	22.03	12 🕳 . 😘
22.45	22.68	23.02	23.67	23.73	94
24.55	24.74	25.23	25.48	?5•35	
27.94	20.00	27.99	28.72	2 1.92	34. 4
31.40	31.77	31.77	32.34	32.95	: . · •
34.55	35.22	35.25	35.27	527	on. • H
37.34	37.33	31.78	38.29	58.38	5

MK test 8

ROLL
SUM OF SINE WAVES FUNCTION

	RMS VALU	JE OF EKKOI	ĸ		
1.600	0.13	1.11	1.1	1 • 2 3	• _ J
1.00	1.06	1.7	1. 1	1.57	1 - "
1.77	1.03	1.72	1. 0	1.72	1.71
1.76	1.80	1.76	1.78	1.71	7.12
1.72	1.75	1.77	1.77	1.77	1.74
1.89	1.82	1.55	1.73	1.3%	1.00
1.85	1.85	1.06	1.05	1.35	1. 4
1.95	1.94	1.92	1.30	1.91	1.73
1.94	1.92	1.93	1.91	1.92	1 4
1.95	1.95	1.91	1.40	1.90	1 - 10
1.87	1.08	1.69	1.37	1.36	1000
1.84	1.86	1.84	1.04	1.05	1 - 3
1.83	1.62	1.82	1.81	1.82	11
1.83	4.53	1.34	1.53	1.03	1. 2
1.85	1.32	1.81	1.81	1.80	$i \leftarrow \pm i k$

	TIME ON TA	RGET (SECS			
0.23	1.15	1.55	2.49	5.41	• 6 1
4.00	4 - 44	5.03	5.46	€ 6 €	5 4 1 4
5.31	6.71	7 •5 U	7 • ∀3	うゅうさ	• 1 J
9.41	y.59	10.51	11.51	11.85	$1 <_{\bullet}, \dots$
12.71	13.01	13.10	14.01	14.93	$1 \cdot \dots \cdot 1$
15.28	15.31	16.78	17.01	16.09	1 4 5
18.75	13.94	19.45	19.75	23.4%	و و ا
20.95	21.27	22.15	22.75	23.0:	,, * • \ <u>*</u> ±
23.62	24.03	24.44	25.45	26.23	1. · · · ·
26.63	27.02	28.03	25 • 07	2 - • 1 m	
30.07	30.68	30.92	31. ∋0	52.00	5 . 7
35.13	33.07	34.12	35.12	35.64	50 · 35
30.17	37.02	57.05	38 • U2	3 5 • 7 0	
39.43	39.58	39.60	39.62	40.05	40.00
40.42	41.52	42.06	43 - 34	4 1.7 m	45. 3

AME test 9

RULL
SUM OF SINE WAVES FUNCTION

	KMS VAL	UE OF ERRO	₹		
1.15	1.11	1.11	1.77	1.11	
1.03	1.11	1.1/	1.15	1.20	1 1
1.15	1.18	1.07	1.18	1.23	1.17
1.27	1.24	1.21	1.20	1.24	1.
1.25	1.27	1.25	1.27	1.16	1
1.21	1.25	1.22	1.50	1.32	1.51
1.34	1.37	1.57	1.48	1.45	1-+3
1.42	1.44	1.42	1 • 48	1.47	1. • •
1.48	1.45	1.45	1.46	1.43	1. + 7
1.45	1.44	1.44	1 • 48	1.48	1 7
1.47	1.46	1.43	1 • 47	1.47	1.05
1.45	1.47	1.47	1.53	1.31	1 . 1
1.50	1.51	1.53	1 • D0	1.51	1.1
1.51	1.51	1.51	1.00	1 • 4 2	1 •
1.49	1.49	1.50	1.49	1.48	1 - + 1

1.00	1.95	2.98	3.08	3.93	:. 13
5.93	6.65	o • 85	7.45	3.45	1.
10.55	10.78	11.83	11.96	18.33	15.54
14.31	15.38	15.50	15.08	1 1 3 1	17. 5
17.41	18.46	19.31	20.19	20.51	34.4
22.54	23.45	24.07	24.12	24.70	41 . 43
25.89	26.12	26.00	26.su	27.52	· · · • · • • • • • • • • • • • • • • •
29.3d	50.47	51.37	31.32	31.09	50 - 14
35.15	55.87	34.38	34 • 80	55.35	3 50 •
36.35	36.80	31.27	37 • 57	31.32	38.0
59.37	40.38	40.55	41.00	41.44	41.7
42.53	42.59	43.46	•	44.40	44.42
40.45	45.54	45.74	46.62	46.60	47 4
40.00	43.37	46.76	49.55	20.33	31.39
51.67	52.48	52.56	53.62	54.41	59.91

NY test 10

YULL
SUM OF SINE WAVES FUNCTION

	RMS VALUE OF ERROR						
2.24	1.11	1.7	1.47	U	• .		
1.3.	1.30	1.50	1.21	1.16	1 4		
1.23	1.18	1.10	1.21	1.20	1.17		
1.16	1.16	1.15	1.13	1.15	1.20		
1.29	1.21	1.24	1.02	1.27	1.1		
1.18 .	1 • 21	1.22	1.27	1.11	$z \cdot z \cdot 1$		
1.24	1.26	1.22	1 • 26	1.51	1.6		
1.31	1.27	1.26	1.29	1.30	1.54		
1.55	1.33	1 • 3 3	1.52	1.33	1 - 31		
1.30	1.29	1.28	1.29	1.28	1.451		
1.52	1.51	1.32	1 • 31	1.33	1.51		
1.30	1.29	1.28	1.29	1.20	1 . 1 7		
1.33	1.34	1.35	1.53	1.31	1.57		
1.51	1.31	1.32	1.31	1.30	1.71		
1.50	1.30	1.50	1.30	1.28	1.30		

MEAN OF RES= 0.96

	TIME ON TA	RGET (SECS)		
0.66	0.91	1.74	2.13	2•3.	
4.85	5.88	6.91	7.48	· • 7 1	·• . 3
9.8€	10.91	11.94	12.55	10.68	19. 4
15.71	16.75	17.15	17 • 3 €	10.23	1 1
10.96	14.46	20.41	20 • ან	21.6€	,' • ':'
23.57	24.19	24.53	24 - 38	20.32	
27.89	28.90	29.92	29.98	30.63	31.20
31.04	32.07	33.07	33.20	33.59	* * • · · · · · · · · · · · · · · · · ·
54.67	35.69	30.37	57 · 58	30.39	3 1. 13
40.22	41.23	42.28	43.26	44.21	44 - 11
44.31	45.32	46.24	47.22	44.22	9 . 1
49.89	50•36	51.74	51.78	53.01	
53.25	53.26	54.12	55 • 14	50.17	
58.17	59.96	50.09	61 - 13	61.52	0
53.20	64.20	55·02	55 • 48	śh•5∂	.7. J

MM test 1.13
ROLL
SUM OF SINE WAVES FUNCTION

	KMS VALU	JE OF ERROI	K		
1 • 1 7	1.92	1.5	.19	1.43	/3
1-1.	1.24	1 - 1 /	1 • 16	1.14.	9.45
1-19	1.32	1.25	1 . 17	1.20)
1.19	1.16	1.21	1.11	1.13	
1.17	1.17	1.17	1.37	1.11	1-14
1.10 .	1.10	1.23	1.17	1 • 1 9	1.17
1.14	1.15	1.15	1.11	1.17	1.11
1.15	1.08	1 -12	1.12	1.1.	1.11
1.10	1.14	1.12	1.12	1.12	1.11
1.11	1.12	1 • 1 1	1.10	1.10	1.10
1.10	1.09	1.15	1.12	1.15	1.1.
1.12	1.14	1.1.	1.12	1.14	1.12
1.12	1.11	1.12	1.11	1.11	1
1.11	1.10	1.12	1.11	1.14	1.12
1.14	1.13	1.12	1.14	4.14	1.1:

	TIME ON TA	ARGET (SECS	:		
10.01	0.91	1.91	2.53	5.55	1.03
$0.0 \bullet 0.0$	0 • 33	7.54	8.10	" • U.3	
9.51	9.54	10.44	11.43	13.58	
13.89	14.09	15.50	15.69	17.88	
17.91	20.88	21.69	21.27	22.02	
23.78	24.50	25.27	25.14	20.70	. 7
28.04	28.87	23.57	30.55	31.60	52. 7
35.20	54.28	35.≥8	30.28	37.30	2.
37.19	39.37	47.38	41.39	434	4-• 1
43.69	44.07	45.72	45.75	47.74	4 . 1 %
47.24	50.26	⊃U•54	51.04	01.12	71.74
52 .7 7	53.19	34.78	oo 79	56.7e	57. S
53.86	59.52	06.40	61.42	52.47	
54.00	54.98	55.0s	65.02	35.10	10 2 4 4
66.63	57.23	67.83	68 • 7s	5 J • 1 U	1

MK test 12 ROLL SUM OF SINE WAVES FUNCTION

	RMS VALU	IE OF ERROI	≺		
1 •	1 • 3 a	$0 \bullet J1$	1.55	11	. •
1.1.	1 • 1 1	1.03	1.55	1 • 1 -	1.15
1.30	1.15	1.15	1.17	1.07	1 - 1 1
1 • 0 3	1.05	1.000	1 • 93	1.003	11
1.06	1.02	1.13	1.13	1 • 1 %	1.1,
1.13	1.17	1.17	1.19	1.15	1 - 0
1.19	1.22	1.22	1.20	1.17	$1 \cdot \cdot \cdot 1$
1.21	1.19	1.17	1.19	1.15	1.:.
1.10	1.15	1.17	1.14	1.1%	1.15
1.10	1.17	1.10	1.18	1.13	1
د 1 • 1	1.10	$c1 \cdot 1$	1.17	1.18	1 - 1 7
1.17	1 • 1 7	1.15	1.15	1.15	1 - 14
1.16	1.14	1.17	1.15	1.15	1.10
1.15	1.14	1.14	1.14	1.12	1.i·
1.14	1.13	1 - 1 4	1.13	1.14	1

	TIME ON TA	ROLT (SECS)		
0.31	1.31	2.30	2.53	3.2%	6.623
5.24	6. 28	7.26	ਖ∙ੇਤ	''•36	1 . 1
11.35	12.33	13.20	14 . 35	19.000	1 . "
16.55	16.69	10.00	18.49	1 1.99	21. 2
22.05	23.02	23.51	23 • 52	24.20	75 ·
25.29	25.57	27.19	27 • 58	23.65	: • 1
29.22	27.00	36.22	51. 16	32.14	51.10
34.20	35.19	ან•1ა	37 • ∂2	30.26	• •
43.24	41.28	41.653	42.36	41.57	4 1
45.20	45.20	45.93	45+12	45.72	-1.1,
45.17	49.31	3 J • 5 4	5 • · 5	51.63	J 7
53,67	24.41	op.32	150 € 56	57.29	$x \sim 1$
59.22	a0.12	50.47	6.0 • 4.2	51.30	2.
55.40	54.41	41 • ط	55 • 4. ²	3/.1×	. /
50.55	69.17	73.17	71 • 25	12.22	7 4 . 3

MK test 13

ROLL SUM OF SINE WAVES FUNCTION

	KM3	S VALUE U	IF ERKUK		
1.15	1.57	1 • 58	1.29	1.00	11
1.12	1.25	シェラ む	1.17	1.11	1.37
1.07	1.15	1 • 0 0	1.15	1.05	1.02
1.05	1.06	1.00	1.61	1.01	1.59
1.04	1.07	1.03	1.51	1.05	1.07
1.05	1.02	1 • 0 1	1.00	1.00	1.03
1.00 .	1.00	1.02	1.01	1.01	4.14
1.02	1.01	1.02	0.17	1.01	ال . • ت
1.0C	0.99	1 - 0 2	1.01	0.75	1 2
1.04	0.99	1 • 0 0	1.33	1.01	1.12
1.06	1.30	1.31	0 • 95	3.99	
1-31	1.00	1.61	1 • 00	1.04	غالانا
1.0s	1.02	1.01	1.03	1.03	1.00
1.02	1.01	1.03	1.01	1.01	
1.02	1.01	1 • 0 1	1.52	1.03	1.00

TIME ON TARGET (SECS)								
0.5H	1.08	2 . € 0	3.51	4 • 4 3				
0.65	7.68	ಚ • ಬ5	9.04	10.65	11. "			
12.75	13.71	14.71	15.74	16.38	17.36			
18.41	19.41	20.39	21.42	22.00	2 . 12			
24.08	25.12	26.12	27.12	28.15	21.15			
3J.1c	51.17	32.14	33.17	34.10	3000			
30.24	37.20	36.25	39.27	40.24	915			
42.20	43.27	44.31	45 • 22	44.32	• • • •			
43.34	49.34	⊃U•33	51.33	52.52	. •			
54.58	35. 38	56.41	57 • ≥8	57.93				
57・97	61.01	52.05	63.35	53.23	5.001			
65.22	66.23	67. 28	68 • 26	525	t 1 • □			
79.22	71.23	72.23	73 • 23	73.33	19.4			
75.83	70.05	17.05	78. 32	79.80	7			
31.87	32 • 87	85.91	84 - 21	35.30	50.405			

MK test 14

ROLL SUM OF SINE WAVES FUNCTION

		RMS VALUE O	F ERHUR		
2.77	1.57	1.12	1.25	1.28	25
1.05	1.04	1.05	1.11	1.16	1.1
1.07	1.03	1.08	0.96	1.05	1 . 5 .
0.79	0.96	1.03	1.31	1.01	. J
1-04	1.02	1.03	1.01	3.47	1.00
1.02	1.00	1.ûl	1.01	0.9 3	1.02
1.02	0.95	1.01	1.00	1.01	1.00
0.96	0.99	1.01	0.37	0.99	ت و له ل
1.00	1.00	0.99	1.00	∂. 99	1.09
0.90	1.01	1.01	0. 10	0.99	و د د د
1.01	1.02	1.00	J. 96	1.02	1.00
1.00	1.00	1.00	û • 49	1.01	1.05
ひゃうケ	1.01	0.99	1.01	U•97	1.00
8.97	1.01	1.00	1.33	1.02	1.00
1.00	1.30	1.01	1 • 32	1.01	J 9

TIME ON TARGET (SECS)								
0 • ೨៦	1.58	2.50	3.56	4.60	3 د ٠ د			
6.61	7.50	3.03	9 • 58	10.63	11.55			
12.56	13.68	14.71	15.71	16.7c	17.71			
16.70	19.25	23.29	21.28	22.28	2			
24.30	25.33	26.52	27.55	20.37	20.27			
30.37	31.37	32.36	33.49	34.35	J .42			
36.39	37.40	34.43	39.43	43.45	41.43			
42.47	43.46	44.51	45.43	40.56	47.04			
40.55	44.52	50.54	51.56	၁၉၈၆၃	نا د د د			
54.57	55.62	56.61	57.56	5 61	11.51			
59.71	60.67	61.71	62.66	53.73	20012			
65.72	66.50	67.47	c6.43	£3.53	10.02			
71.51	72.53	73.52	74.57	75.57	7 1			
77.60	78.52	79.22	30.22	31.23	5 . 1.7			
83.12	83.50	84.45	85 • 49	១ b • 5 C	17.1			

MM test 1

HOLL SIM DE SIVE WAVES FUVETION

	+	MS VALUE D	F Exx m	_	
4 6 .	1.59	1.05	1.47	1.41	• • 4
1.5	1.47	1.48	1.52	1.11	1.464
1 - 25	1.5b	1 • 51	1.05	1 • 2 •	. • 5
1 • 54 1 • 22	1.19	1.33	$1 \bullet \neq 7$	1 • 2	
1.23	1.23	1.24	1 • 2Ŭ	1 • 2 €	10.5
1.1.	1.16	1.19	1.1.	$1 \bullet 1$	•
1.20	1.22	1.2.	1.21	1 - 1 1	1 • 4 *
1.24	1.3	1.21	1 • 15	1 • 4 •	. • 4
1.25	1 • 21	1.25	1 . 22	1.34	1 - 1 5
1.023	1.25	1.23	1 • 25	1 • 2 4	• •
1.20	1.25	1.24	1.25	1.27	1 a U
1.20	1 - 24	1.23	$1 \cdot J1$	1 . 20	
1.45	1 • 24	1.27	1 • - 3	1 - 2 -	1 • 12
1 • 4	1.3	1.25	د, ۱۰	**,5	1.4.14
15	1.22	1.23	1.22	4 • □ ♂	1 + 15

4: AN OF RESE 1.24

11M. ON TARBET 1.8001								
J • 34	1.34	1.55	1.71	7.7. 7.54	· · · ·			
4 • 4 3 5 • 2 3	4.56 9.21	16.25	11.22	12.42° 17.20				
10.39	14.91 19.08	10.95 20.14	1.13	22.17	• 4			
23.67 23.25	24.67 38.27	25.12 25.27	25.70	103	. <u>1</u>			
51.53	51.00 34.19	51.20	20 • 63 20 • 12	3 4 • 12 5 2 • 4 4				
40.37 44.52	41.32	42.09 40.00	47.54	4 / • 2 /	v • ₹			
41.83	50.52 54.44	91.95 99.45	12 • 1 10 • 15	ებ⊕ს# ე ″⊕21t	να•. δ 			
53.72 57.43	99.49 50.00	51.04 33.28	(2.00 √1.00	57.60% 57.65%	4 <u></u>			

MM test 2

ADEL SOM OF SINE WAVES FUNCTION

	-	MS VALUE D	F (33.7.13		
		1.44	1.11	1.51	
• 77	1 • 11	0.95	1.27	1.0::	200
1.11	1.54	1.07	1.07	1.00	1.11
1.15	1.33	1.25	1.09	1.05	∂€
1.00	1.05	1.00	1.03	1.0	1.1
1.600	1.09	1.07	1.30	1.9.	
1.000	1.05	1.00	1.37	1.37	1
1.000	1.00	-	1.07	1.34	1 - 14
1.00	1.05	1.03	1.04	1.67	1.05
1.12	1.10	1.10	1.07	1.09	A •
1.07	1.05	1.09	1.07	1.03	
1.03	1.07	1.00		1.37	1.0
1.06	1.37	1.00	l • up	1.00	. • 3 N
1.07	1.07	1.07	1.00	1.00	
1.07	1.07	1.07	1 • 37	1.00	1 7
1.03	1.07	1.00	1.07	1 0 2	. • • •

ABAN OF REST 1.07

TIME ON TARGET (SECS)								
A 11	1.29	2.51	2.0	4.4.4	4 4 44			
0 • 50 6 €	5.49	7.43	3 • 24	W . 4 W	12.5			
5.50	12.50	13.66	14.50	10.55	¥ 1.0			
11.63	18.65	19.70	20.76	21.51	• • • 0			
1/.55	22.43	23.33	24.54	2 1 1 1 1	. 7			
22.45	23.42	24.44	د 4 • ٥٠ د	31.40	2. • 44			
27•53 55•45	34.47	50.14	35 • 22	57.1				
59•73 59•25	40.27	41.27	42.08	97.425	46.0			
44.2:	45.33	46.32	47 . 22	47.42	1			
43.32	49.58	o 0 • 39	51 • 54	52,21	51.17			
99.00 94.23	33.26	⊃ 6•20	-1-21	24.07	• 21			
54.25	01.02	ن ک ب ف د	, ১৯০৪	ى ك• ئەر د	. 7			
50.00 50.05	65 o z 7	et oul	57 · 55	20.65	. 70			
70.67	71.71	72.71	12.14	70.20	7 '3			
7 (-3)	70.20	11.55	15.35	7 🤊 • J u				

MM test 3

ROLL 304 OF SIVE WAVES FUNCTION

h.				
1.56	1.11	1 • 11		, , (
3 • 3 8	0.98	1 - 11	2.47	. 1
J • 48	J • 31	1 • 11	u •™7	. • 2 .
	1.30	1.5	ت فی ل	
	1.02	1.01	∪ • c² :	• **
	1.00	J . 119	1.00	1.4
	1.00	0 • 49	0.77	5
		1.00	1.0%	1 1
	=	1.01	1.01	5. 😼
		1 • 10	1.01	2260
			1.0.	1
			1.01	1
			1.5	
				i - '
		-		1
1.03	1.02	4 • 7 · .		
1.01				
1	IME ON TAR			
2.01	ა•u1	ن • • •		5 1 2 4 5 4 5 4 5 4 5 4 5 6 5 6 6 6 6 6 6 6 6
	1.56 0.38 0.78 1.05 1.04 1.00 0.39 1.02 1.00 1.02 1.00 1.05 1.00 1.05	1.56 1.11 3.38 8.98 0.98 J.31 1.05 1.00 1.04 1.02 1.00 1.00 0.39 1.00 1.02 0.99 1.00 1.01 1.02 1.00 1.02 1.00 1.03 1.00 1.03 1.00 1.03 1.00 1.05 1.01 1.03 1.01 1.03	1.56	1.56

TIME ON TARGET CON						
0.95	2.01	1 ن•ن	 ↓ €	: • 0 =	٠ ٩	
7.00	o • 11	9.08	3	10.41	lla et	
12.4%	15.00	14.45	10.5	10.04	11.	
18.00	19.55	20.57	21.58	20•50	* • • · · *	
24.59	25.05	25.55	21.34	20.05		
50.65	31.47	32.50	53.47	54.56	4	
36.03	37.54	30.57	39 • : 2	46.666		
42.64	43.00	44.66	45.32	46.00	900	
	41.08	DU • 12	51.12	5. • 4	• . 1	
4 3 • 07	22.14	50.18	51.21	50.024	• • • • •	
54.16	00.58	01•3¢	62.52	83.435	• • 1	
úu•27		57•I5	5 • † 3	c •41	1	
65.55	υδ•υ7 20 0 •	73.25	13.08	14.1		
/1.40	72.25	75 • £5 75 • ⊌8	7 2 • /1	30.40	1.74	
7:1.57	11.5		35 • 32	35.34	1.17	
ちょうせい	83.31	ರ ५ • ೨ U	3 3 • 32	<i>35</i> • 5 ,		

MM test 4

HULL SINE WAVES FUNCTION

	h	MS VALUE O	r Same Sa		
150	1.50	1.12	1 • • 7	4 • 61.1	1 - 1 1
1.11	1.64	しゅうし	U • (೨	1 • '	
0.97	0.94	1.07	0 • 142	U • ∀ ₹	1 • 0 1
0.95	9.70	1.00	1.05	. * • × · .	·. • · · ·
u . 97	1.02	0.73	1.51	1.0	الم در م
1.00	0. 16	しゅりお	1 • ∪ →	U • 4.7	1.675.25
U • 75	1.02	0.55	U . 15	و چال	3.17
0.99	0.99	U • 96	0 • 45	6.97	1 • 0 0
6.95	0.94	0.49	U • 27	3.72	. • 41
3.94	3.77	0.71	1.73	1.00	1
0.97	1.00	t.¹b	1 • • 0	1.607	1.00
1.60	1.60		1.51	1 • 0 .	1.31
1.62	1.01	1.02	* • • •	1001	
1.01	1.01	1-01	0 • 17	1.5	! .
1 • 6 1	0.59	1.01	1 • JU	U • ',''	1 - 41
EAT OF RMS	: û•99				
	i	THE ON TAR	GET (SEES	,	
ひゃりひ	1.98	2.00	충출생성	: • ∪ ٺ	•
1.33	7.24	8.50	きゅうじ	10.1	11.00

TEAT OF KINS = 0.99

TIME ON TARGET (SEED)							
U . 9 U	1.78	5.00	5 . 58	1.000	•		
1.03	7.74	8.50	9.05	10.1	11.50		
12.59	13.65	14.58	15.00	1 (• 0.1)	17.5		
1 > • 64	19.75	20.75	21.17	26.73	1000		
24.78	25.62	20.00	27.65	20.07			
30.30	31.20	52.54	33.33	34 • ≥ ?			
32.32	51.57	30.42	3 d • 4 4	4 1 4 1	· 1 • 4 7		
42.45	43.07	44.63	+1 . C+	46.16	+ 1 - 14		
98.17	49.18	56.19	11.20	52.25	•		
54.26	35.24	20.27	27 ⋅ 53	50.00	1.00€		
2.3.0 00	51.14	52.10	62.71	65.628	1. M 🔸 🚉 🐧		
p5•56 p5•55	56 • 36	67·37	6,5 € 33	50.07	> • ≤8		
70.5d	71.61	72.61	15.67	74.0.	S. 6223		
	77.08	78.70	79.73	33.75	1 • 3 ♂		
76.68 52.77	33.00	84.32	ช ົ • ±ີ້ວ	30027	1.51		

MM test 5

WHAT OF SINE MAYES FUNCTION

POM OIL STAP 4					
	кМ	IS VALUE OF	= CHRON		1 0
0.00	0.79	0.91	1 - 25	ម•សភ	
	1.04	1.23	1.11	1.1.	1 - 110
1.11		2.03	1.07	1 • 0 • •	1.01
1.02	1.72	0.97	1. 38	0.16	1.04
0.72	1.05		1.07	1.0:	1.03
ひゅうり	1.04	1.05		1.05	1.31
1.0≥	1.00	1.03	1.04	1.02	3.97
0 • 9 ซ	1.00	0.99	0.77	1.00	1.00
1.00	1.00	1.01	0 • ५६		1.33
1.00	U•39	1.01	1 • 110	1.15	1.03
	1.00	1.01	1.55	1.05	
1.02	1.33	1.05	1 - 35	1.0%	1.15
1.0+		1.03	1.33	1.04	$T \bullet \gamma_{ij}$
1.03	1.04	1.04	1.05	1.05	4
1.01	1.63		1.65	1.0:	1 m
1.05	1.03	1.00	1.03	1.02	1.31
1.03	1.02	1.63	1.03		
ALAN OF KES	1.05				
	!	TIME ON THE	KGET (SECS))	્રા
0.05	1.49	3.00	3 • 45	D • U ⊃	
0.90	8 - 06	4 • U ti	10.11	11-11	11.

		LIME ON TAR	GET (SECS)		
0.96 7.15 15.15 17.25 20.52 51.42 57.20	1.49 8.06 14.18 20.26 26.34 32.45 38.20	FIME ON TAR 3.00 9.00 15.17 21.28 27.38 35.30 37.80	3.98 10.11 15.21 22.52 23.37 54.15 40.22	5.03 11.11 17.20 23.32 23.34 30.14 41.26 43.37	2.03 1.01 12.05 24.32 50.43 50.12 4.00
45.20 45.03 54.67 57.20 59.50 70.41 76.50 51.60	44.28 43.65 55.72 57.26 65.32 71.48 77.55 32.98	45.53 50.64 56.72 50.33 66.40 72.50 78.20 83.69	45.01 51.63 57.19 61.23 67.41 73.01 73.62 84.70	52.65 57.48 52.65 53.42 74.57 7.87 82.84	31.37 32.49 32.02 37.45 77.65

MM test 6

ROLL SUM OF SINE WAVES FUNCTION

	ĸ	MS VALUE 0	F IKA K		
1.92	1.57	0.91	1.35	1.10	0.54
1.05	1-11	Ŭ•98	1.03	1 • J U	1.1
1.07	U . 139	1.05	1.54	1.01	J • 13
5.5 4	0.40	1.03	1 • ∂ Ŭ	1.01	17
1.02	1.04	1 • 0 0	Ü • 73	1.33	7
1.05	1 • U O	0.98	3.99	J.47	1.51
1.02	ひ・フタ	1.07	0.93	() • · · · ≥	0.00
1.05	1.00	0.95	0 • 4 3	1.30	1.30
0.54	8.47	0.93	1.01	3.71	. • M.D.
0.95	0 • ५ ৪	1.00	1 • 66	1.0%	
0.94	0.98	1.03	0.70	1.01	J 🕶 (4)
1.00	1.60	0.99	1 • 0 3	ن ن ۽ د	1.06
0.90	0.49	0.98	1.02	1 • J J	1.00
0.99	1.01	1 • 0 0	1 • J 0	1.00	الانت وال
0.90	64.0	U • 99	1.00	3.97	1.00

TIME ON TARGET COLON						
9.96	2.00	5.Jl	ر ^ن ب 4		J 🕶 🕽 🤧	
7 - 10	3-11	J • 68	16.69	11.11	11.09	
15.19	14.15	15.19	15. 1	17.21	18.03	
19.20	20.24	21.20	22.52	23.38	. 4.50	
25.33	25.73	2: •7J	21.72	2 + . 74	15	
50.75	51.77	50.15	23.002	44.0£		
5.003	37.89	ಎ೮•೮7	37.037	40.52	41.16	
42.89	43.34	4 , . 61	45.1	41.591	+ * + 91	
4フ・しさ	ភបិត្សិត	31.Jg	* 2	o tol	21.1.	
55.12	ુ5 • છકે	26.91	1. 54	057	يخ ولا 📦 د و	
80.93	62.01	(2.97	63.53	54.7	J. 15	
50.01	57.57	38•68	10 • 10	7 D • 7 🗆	12.13	
72.71	73.78	74.75	75.4U	75.61	17.13	
10.22	19.20	5 0. 26	31.27	36.67	: • 3 U	
84.27	ಕ್ರಕ್ತಿತ್ತ	56.54	87 · 36	38.3e	. 4 . 79	

MM test 7

ROLL SUM OF SINE WAVES FUNCTIE.

1.50	1.77	MS VALUE U	F 18606 1.75	1.07	1.
0.59	1.30	9 • 9 8	1.02	1.7	1 •
1.07	1.20	1.10	1 • 44	1.20	. •
1.17	1.56	1.00	1 - 11	1-1/	
1.19	1.25	1.14	1.22	1.15	! •
1.10	1.19	1.19	1.1t	1.1"	1 .
1.15	1.17	1.18	1.10	1.15	1.
1.12	1.17	1.16	1.10	1.11	
1.13	1.15	1.15	1.1J	1.15	
1.15	1.14	1.15	1.16	1.17	i .
1.14	1.14	1.15	1.10	1.1/	1.
1.15	1.17	1.10	1.16	1.14	1
1.15	1.15	1.14	1 - 14	1.1	
1.14	1.14	1.14	1.15	1.13	ì
1.15	1.10	1.12	1.13	1 • 1 1	1
JF KMS=	1.17	•			

4 :

	1	TIME ON TAR	SET (SECS)		
.) 44	1.28	1.29	1.	•	. i
0.34	5.95	t, • 4 d	7. 19	s 🕳 😏 🗁	• t 🗇
4•51		12.15	12.93	13.51	1.4.
10.71	11.71	17.38	18 • 50	13.64	
15.31	16.33		21.75	21.75	,
20.53	20.33	20.75		20.90	1 .75
24.87	25.84	26.68	27.96	5:.15	4.13
30.44	31.65	51.Qii	25.12		46.72
30.13	35.13	57.22	38.19	37.23	
41.20	42.29	43.25	44 . 23	44.29	• • •
	+6.ul	47.61	48 • 54	40.000	• • • • 7
43.54	51.38	52.21	52.06	50.04	m • 2m
50.33		5/.61	55 · 63	51.01	្មស្ន
55.54	56.57		62.55	5:4.33	· • * *
51.05	51.82	a2•31 2•63	68 • 45	57.45	10.41
65.3℃	20.40	67.41		71034	1
71.47	72.36	12.58	73.38	(T ● +, G	. •

MM test 8

ROLL SUM OF SINE WAVES FUNCTION

	i ·	MS VALUE OF	F ERROR		
0.00	1.37	0.91	1 • 24	1.11	1.16
1.11	1.24	1.45	1.11	1.21	1.00
1.11	1.07	0.59	1.11	1.11	1.11
1.08	1.05	1.00	1 • 병원	しゅうべ	1.01
1.04	1.04	1.02	1.07	1.07	1.07
1.07	1.09	1.00	1.00	1 • € 3	1.51
1.06	1.08	1.08	1.07	1.05	1.7
1.00	1.05	1.03	1.06	1.00	1.02
1.05	1.11	1.05	1.34	1 • U O	1.07
1.07	1.00	1.00	1.05	1 • C :	1.07
1.04	1.04	1.00	1.00	1 • 0 1	1.34
1.05	1.07	1.10	1.05	1.04	1.04
1.05	1.05	1.05	1.00	1.00	i • 6 ts
c0.1	1.04	1.05	1 • 0 5	1.05	1.04
1.00	1.44	1.00	1 • 15	1.04	1.05
ALAN OF HASE	1.06				
		TIME ON TAR			•
0.90	1.38	2.76	3 • 75	4 • ± 1	• 4.3
u • 81	7.65	0.85	₹• 23 d	10.90	.1.50
12.70	13.10	14.09	15.59	10.15	17.18
18.15	19.20	20.21	21.13	22.22	15.26
24.24	24.39	25.14	25 • ₹3	20.17	1/.10
28.20	29.22	5 L • 2 ≟	31 • 27	3 1.23	4.0
54.22	35.24	jt • 45	કુંક • વહે	57 • SC	• 5.2
34.35	40.32	41.55	42.37	40.30	44 . 5 %
43.25	45.52	46.51	47.53	45.55	9.74.18
50.57	51.56	52.62	25.57	54.61	7
8 ئا م د ر	57.61	ეგ•ენ	১৪•৪১	೨ % ₀ ४ ₺	
51.90	10.50	53.93	し4 • つち	55.61	• 1
97.65	oB • 23	69.07	70.16	71.16	77.10
75.17	74.20	15.21	70 • 36	77.20	1. • 17
73.88	79.70	30.70	3 1 • <i>l</i> 3	82.51	- 4 2

MM test 9

HOLL SUM OF SINE WAVES FUNCTIO:

		KMS VALJE (OF EXX 19		
1.12	1.77	1.11	1 • 4 7	1.71	1. 7
1.11	1.04	1.17	1.11	1.00	01
1.11	0.94	1.07	1.07	i a U c	1.01
1.05	1.65	1.03	1.000	1.J1	· . /
1.04	0.95	J • 75	1.5	1.01	1
1.02	1.11	J • 98	0.97	i • 0 1	
1.00	1.02	1.00	3.98	1.01	
1.00	0.49	U • 7 G	و, و 🐞 ن	1.00	1.55
1.00	0.96	1.01	0.17	1 • 0 0	
J.95	0.96	0.99	0.79	1 • 0 ù	
0.45	0.78	1.00	1.00	J.99	3 4 4 4
0.54	1.01	0.91	1.00	0.10	1.30
1.05	1.61	1.00	1.03	1.003	J U
1.61	1.01	1.00	1.02	1.02	1.00
1.00	1.01	1.01	1 • 02	1.01	3 .
1tAN OF RES	= 1.00				
		TIME UN TAI	ROET (SEC.))	
0.50	1.49	2.50	3 • 50	ન • ડે હ	• • • •
6.36	7.40	ს • ⊅ ნ	9.41	10.45	.1.4
12.48	13.48	14.51	15.51	16.54	11.
1 m . 6. b	14 59	20.45	1.1 - 1.2	29.59	7

TIME ON TANGET (SECS)								
0.50	1.29	2.50	3 • 50	7 • j c				
6.38	7.40	მ • ⊅ ნ	9.41	10.45	.1.4			
12.48	13.48	14.51	15.51	16.54	11.4.1			
16.60	14.59	20.65	21.00	22.5 €	. 7			
24.65	25.52	26.53	27.54	28.55	• • • • • • • • • • • • • • • • • • •			
აშ•57	31.00	32.62	ာ်သံ•မဂ	34.50	10.12			
36.67	57.70	36 0€9	39.72	40.73	4 /2			
42.77	43.74	4 + • 81	40 • 64	46.83	41.88			
48.63	47.37	50.71	51 . 12	52•91	Sec. 3.2			
54.96	55.18	55.90	57•¢1	5 01	. 12			
uܕ07	L1-11	62.17	ပုဒ္ခံ 🕶 🗸 🖰 😘	04.12	٠13			
ob • 17	57.17	50.10	69 • 1s	70.17	110			
71.00	71.95	72.10	13.21	74.22	11.020			
76.25	77.27	73.26	73.51	80.28	1.16			
45	4 (24	المناج المناج	HD = 411) c p c +, b c	7			

MM test 10

WOLL SING WAVES FUNCTION

1.15	1.17 1.17 1.15	1.17 1.17 1.15 1.14 1.15 1.15 1.69 1.14	1.15 1.15 1.14 1.14	1 • 1 · 1 · 1 · 1 · 1 · 1 · 1 · 1 · 1 ·	1.
------	----------------------	--	------------------------------	---	----

MEAN OF KYS= 1-20

	1	145 DV TAN	3, T (SECS)		, ,
0 - :	U•⊬1.	1.09	2.21	J • U :	1.1
0•55 5•0≎	5.76	L . 74	7 • 1.1	•	1
10.70	10.71	11.59	12.03	1	
10.70	10.49	11.bb	18.03	19.50	•
20.94	21.08	27.13	25. 15	ان کا ہے ۔ ایک ہو ہے جاتا ہے۔	
20.64	26.72	21.75	28.75	2 ° • 3 ° ·	
31.07	31.09	32.90	33.24	4 3 • 2 c	• 1.5
50.30	51.57	30.55	53.30	4	Sec. 2.14
41.04	46.00	45.71	14 44 a 15 44	. u . 71	1.1.4.
41,641	47.06	43.67	%9 • 54 54 • 54	55.57	1.0
52.57	52.57	53.51		54.604	1
57.17	50.17	57.15	53 • tu	36.43	7 · (1)
٠ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ	u3 • 58	94.58 70.61	21 • n2	72.05	73.47
53.50	ရွ်မှ ၁၀	70.51	77.61	70.653	77.43
7 5 5.7.	15.57	76.662			

MM test 11

MULE SUM OF SINE WAVES FUNCTION

	11	MS VALUE O	F ERR⊅K		
1.58	1.93	0.91	1 • 2 +	J • 25 C	!)
1.11	0.76	1.17	U • 17	1.3.	1.10
0.87	1.15	1.11	1 • j7	1 • 5 4	
1.11	1.05	1.11	1.13	1.54	x + 114
1.02	1.04	Ü • 🖖 🧠	1.01	1.6	1.01
U - 4 5	1.04	1 • 6 /	1 . 62	9 . 4 7	1
1.06	1.06	1.02	1.04	1.01	1.27
1.03	1.02	1.00	1.00	1.00	1.00
1 • Ú 4	1.06	1.05	1.4	1.01	1 • 11.
1.04	1.04	1.03	1.54	1.03	1.5
1.01	1.02	1.63	1004	1.54	4.653
1.03	1.02	1.33	1. jš	1.0.	\$ • 6 s.
1.05	1.05	1.05	1.03	1.01	ا " أن ما د
i • J +	1.04	1.05	1 • 64	1.5:	
1.65	1.04	1.0:	1.02	1.0.	4
LAN OF KMS=	1.04				
	ı	The OR TAR	J. T (SEES)		
0.93	1.74	2.75	8 a 44 m	1	. 1

45

FIME OR TANGET (SEES)							
0.93	1.74	2.75	3. 45	1.00	• 1		
7.01	0.05	1.05	10.65	11.11	. ل • ١		
13.11	13.73	14.54	15.41	1 + 4			
13.46	19.49	20.55	.: 1 · . 1		4		
24.54	20.57	20.27	21.00	1 to 1 to 1 to 1	•		
50.72	31.65	32.60	33.20	33.54	• • 17		
35.34	30.39	57.43	54. IU	57.4.	47.14		
41.43	42.49	43.40	44.40	44.79	45.12		
46.72	47.72	40.74	49.73	ગળ•7ડ	(4		
52.75	55.74	34.13	⇒5 • 34	55.52	7.		
54.91	59.91	υ0•9 <u>1</u>	s l •52	64.5	• 4 0		
54.50	65.43	Ü6.47	65 - 36	67.50			
59.27	70.28	71.50	72.05	7:050	1 + + 27		
75.37	76.57	17.40	73.41	7 / • 7 1	1.14		
3 C . 7 E	31.55	52.57	لايد ماکر	34.654	5		

MM test 12

SIM OF SINE WAVES FUICTION

	k.	45 VALUE U	F { 3 4 1 K		
1.12	1.12	じゃしょ	4.60	1 - 1 1	11
1.11	1.44	1.17	1.00	1 • C u	• • •
0.97	U • 58	1.41	1.04	1.30	! • J 1
0.99	1.63	1.03	1.00	\$ • ≠ *	3. 14
1 • 0 .	1.02	1.41	1.00	1.05	$1 \cdot \bullet \downarrow 1$
1.04	1.00	i • C C	1.02	1.01	1.000
1.05	1.00	1.34	1.52	U • 1	6435
1.03	1.06	1.03	1 • .2	1.00	
1.03	1.02	1.65	1 - 55	1 • 0 ↔	1
1.34	1.34	1.02	$I \bullet $ ^{n}I	1 . 3 -	1.4
1.02	1.02	ن با م ۱	1.05	1.00	1.50
1.69	1.63	1.(1	1.0	1.09	1.35
1.62	1.01	1.02	2.00	1 • 3	
1.02	1.03	4	J 🕳 🕶	1.5	. • • •
1.01	1.01	1.02	1.50	1.02	1 • 0 1

4. AN OF KYS= 1.02

TIME ON TARGET (SECS)								
3.90	1.98	2 • U u	3. 40	5.03	- 1			
/ • 1 ù	d • 11	9.11	10.13	11.13	1 1			
15.15	14.00	14.45	15.45	10.47	11.10			
10.23	19.25	20.25	21.603	27.53				
24.17	24.00	2: •37	26.0	27				
23.34	30.34	31.56	42 . 5 5	သို့သိန္ 🚶 🗸	·• • (*)			
35.07	53.74	3 13	:1.73	30.10				
40.77	41.H3	42.435	45.61	44.47	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1			
45.91	47.25	40.21	41.15	50.11	1			
53.025	23.60	54.31	55 • 3 2	36.50	7.004			
51.020	37.31	5 b + 3 t	61.59	53. \$3				
54.45	99.45	£6.48	.7.47	5	. 1			
70.52	11.27	72.32	72.82	73.33	14.02			
10.05	70.00	77.85	10.11	7 - 11	1.0			
4.5.03 4.1.8.7	32.03	a2.91	83.72	34.45	7			

MM test 13

RILL SUA OF SINE WAVES FUNCTION

		r\	MS VALUE O	OF EXRUN		
	1.11	1.77	1.11	Ü • ≯5	1.52	1.11
	1 • 1 1	1.04	0.91	0.95	0.94	1.00
	1.11	0 - 94	1.07	1.00	10.01	9.7
	1.95	0.93	1.30	1 • 00	U • F	. :
	0.05	3.47	1.36	1.00	6.74	0.11
	1.00	0.96	u • 5 7	3.7	1.01	
	1.00	1.02	しゅジラ	0.91	0.9€	1.78
	0.76	0.97	0.96	U . 71	J + 19 17	€ • • 1.
	0.9 8	ひゃがお	0.47	0.47	1.03	يون نواند دون نواند
	0.97	0.78	34.0	0 . अंड	H•4,	7
	U . 97	0.98	0.97	Ú . 20	6.97	
	0.97	3.49	() • ∀ →	0.17	0.46	.97
	りゃりむ	0.17	0.97	0.98	0.90	0
	0.91	0.37	3.45	0 • 45	er • (4 e)	1
	J • 9 3	0.16	U•47	0.47	G · ·	3.90
i An	UF 3M3=	ย•9ส				
		ī	HAT NO LMI	GET CHECS:)	
	0.94	1.99	2.99	4.00	5-30	2.03
	7.05		9.69	10.11	11.11	13.14

		AT NO LMIT	ROLL CHECS)	
9-94	1.99	2.99	4.00	3 - 3 -	4 . 3 3
7.05	4.05	4.69	10.11	11.11	13.10
15.1n	14.15	15.15	15.13	17.14	1 .21
19.25	20.25	21.30	22 - 30	20.23	. 4 . 4 .
25.35	?6.54	21.29	25 • 57	39.51	· 0 . 4 _
31.42	32.43	33.41	54 • 45	50.40	ليد' سي ر
37.53	3 ₫ • 54	37.53	44.54	41.57	- 1
45.61	44.12	45.50	46 • 134	47.33	/1
41.55	51.71	J1.72	52.13	35.57	9
35.58	Jo • 51	57.63	78 · 37	j 7 • ú +	1 C . 10
21.70	62.71	53.71	64.72	50.00	/ .
67•71	48.15	69.73	10.76	11.71	" .70
73.31	74.85	15.85	16.35	77.35	1
79.91	පිට • පිට	81.93	32 • 2o	55.34	S 7
53.91	30.47	ರಚ.02	ay • J5	14.07	-1.13

EM test 14

NOLL SUM OF SINE WAVES FUNCTION

		RMS VALUE (OF ERROR		
1.15	0.79	Ű •64	1 - 74	1.22	1.11
0.42	1.04	J.76	1. 13	0.50	2 • 1
1.02	0.98	0.95	↓ • 96	1.56	• 7 :
U. 95	1.02	1.03	0 • 11	J. 90	2
J.97	1.02	1 • ú 0	0 • ∀3	3.17	J • ***
1.02	1.02	U • 9 ti	0.97	ઈ • ∀€	• 12
0.95	ひょうち	ر لا ◘ ال	0.45	U • 13 =	. • • • • •
Ŭ• ⁹ 6	0•4€	3.98	û•47	U + 39 th	
0.93	0 • → 7	0.57	น์ 🕶 🗷 🖰	0.95	
0.93	0.94	1.36	5 • 47	ピ・フラ	
U•95	0.96	J. 90	J. 10	リ・ラー	ر، ` ، ل
0.96	0.10	U • J.	U . 75	0.00	u • ° t.
0.95	0 - 96	3.47	D • → /	0.94	J • • •
3.70	Ü • 9 €	0.00	U • 11	• • 1	▲ 3.1
4.40	41 * 1542	(1 → **)	3.31	r • • • 1	• 11.
MEAN OF KMS=	: 0.9₺				
0.04	9 (TIME ON TAR			
0 • 9 5	1.94	2.98	4.01	tv•0 c	• = 7
7.05	3.09	9.11	10.11	11.16	11
13.14	14.19	15.19	15.25	17.25 25.32	1 • →
19•23 25•34	20.26 26.37	21.\$2 27.35	22.56 25.42		• • •
31.42	20.37 52.47	33.45	20 • 42 34 • 47	29.40 35.50	. • • .
37.55	58.38 58.38	59.45 59.57	40.35	3 (• 3 J 4 1 • 3 Y	4
43.61	44.59	45.00	40 • 30 45 • 00	47.64	4 1 4 10
49.73	50.71	51.73	52.70	54.79	· • 11
55.79	56.52	57.83	53.23	ラジ・ウェ	
61.86	62.90	⊌ 3 • 9 3	53 • 2 5 54 • 2 0	55.17	t to end to
68.00	67.02	70.05	71.05	72.02	15. 6
74.07	75.11	75.03	77.11	73.12	1.5
80.16	81.18	82.17	83.24	34.21	•
86-21	87.27	58•2b	59 • 30	90.33	ì • • •
00.21	01021	33025	07 • JU	7 U • J	1.00

RL test 1

HOLL SUM OF SINE JAVES FUNCTION

	r.	MS VALUE 0	F EKKJR		
1.15	G.78	0.91	1.11	1.32	5 • 1
1.33	1.47	1.17	1.00	1.50	. • • • • • • • • • • • • • • • • • • •
1.34	1.39	1.25	1.30	1.40	1 • 4 I
1.32	1.31	1.57	1.4	1.35	1 • -1-
1.42	1.40	1.33	1.50	1.54	1.15
1.32	1.50	1.35	1 • : 5	1.50	1.54
1.57	1.31	1.55	1.34	1.31	. •
1.50	1.35	1,30	1 • 32_	1,39	* * * * * * * * * * * * * * * * * * *
1.57	1.36	1.54	1.54	1.30	1 - 74
1.55	1.33	1.34	1.55	1.57	2 • 5°
1.38	1.57	1.38	1.37	1.38	1 • 2 9
1.58	1.37	1.30	1.35	1.37	1.57
1.37	1.56	1.57	1 • এ৪	1.30	$1 \cdot 2^{H}$
1.55	1.57	1.57	1.37	1.37	1.1
1.35	1.35	1.36	1.35	1.31	1.0%

1.00	1.46	2 e à 4	3.16	≯• 1 ³	⊶ , 71
4.85	5.94	7.01	/ • · J	7 • 7 •	° • ∠ 4
8.23	8.86	9.91	10.71	11.0~	11 • t
12.54	13.35	13.59	14.3.	14.00	10.41
15.01	16.p5	17.63	17.35	1 • ***	7
20.03	21.03	22.02	22 . 52	22.76	
24.19	25.22	25.07		27.54	
28.79	29.00	30.85	31 • 24	51.50	
33.35	34 • 3.7	♦५∙3 2	3 5 . 64	ે ્ર∳ઇ જ	1.)
37.72	38.72	39.03	40.07	40.17	9-1 × 4.7
41.90	42.14	43.51	43.74	45.37	4
44.81	45.86	46.79	46.75	47.57	4 . 14
45.67	49.12	42.87	50 · 18.	.20.51	· ! . i
51.78	52.81	53.82	54 - 19	54.73	* ' • 4
26.46	57.32	58.24	59.29	うりゃっく	• 4.5

RL test 2

ROLL SINE WAVES EUNCTION

	KMS	VALUE OF	rRR IN		
1.57	1.77	1.44	0.97	1.31	1.19
1.10	1.04	0.91	0 • • • .	1.54	1. 2 2
1.02	1.11	1.11	1.11	1.21	1.17
1.17	1.14	1.15	1.00	1.23	. 33
1.13	1.15	1.19	1.15	1.07	1 • 1 ~
1.16	1.16	1.19	1 - 14	1.14	1.17
1.17	1.10	1.17	1 • 2 U	1 - 12 0	1 • 1 **
1.10	1.18	1.17	1.10	1.1	1.15
1.17	1.15	1.14	1 • 17	1.14	1.14
1.14	1.14	1.14	1.12	1.17	1.15
1.14	1.16	1.17	1.17	1.17	1 • 1 0
1.17	1.16	1.16	1.10	1.10	1 • 1 ·
1.16	1.16	1.18	1.14	1.17	1.15
1.17	1.18	1.18	1-17	1.16	1.17
1.17	1.16	1.15	1.13	1.15	. • 17

4: Ale OF RMS= 1.15

		and the second s			
		TIME ON TAI	KOLT (SECS)	
0.94	1.39	2.16	3.10		• 1
6.21	6.51	7.53	8 • 54	M • W 5	13.01
11.58	12.51	12.96	15.28	14.31	11 • 11
16.54	16.80	17.80	18.83	14.11	. 1 . J to
21.12	21,47	21,97	23.02	23.95	· • 11 5
26.03	21.03	27.38	28 • 34	25.01	10.10
31.14	31.79	32.04	32.49	35.20	14.4
30.03	35.27	30.24	37 • ab	3 e • 2 7	. 4.
40.32	41.52	41.91	42.77	4 5. 3 4	7
46.03	46.38	43.01	48.67	4 4	+ • + 4
50.64	ع ۵۰ د ۵۰	51,62	52.72	51.64	1.1.24
55.22	56.19	56.68	56.∙82	57.51	
59.67	60.29		bl . 54	£ 6 € 5 H	2 to 12
64.13	64.71	65.41	o o • 15	67.00	7 • • 7
69.00	59 . 67	69.87	76 • 83	71.47	7. 1 · · ·

RL test 3

HOLL SUM OF SIGE WAVES FUNCTION

	K	MS VALUE O	F ERROR		
1.95	1.57	1.12	1.47	1.51	1 • 2 0
1.19	1.25	_1.17	1 • 22	1 • (2.5)	1.16
1.15	1.26	1.11	1 • ປ છ	1 - 1 4	1.1/
1.11	1.05	1.19	1.14	1.1:	1 - 1 %
1.15	1.15	1.13	1.15	1.20	1.15
1.15	1.11	1.13	1 - 11	1.14	1.11
1.14	1.14	1.13	1-14	1.15	1.12
1.12	1,15	1.10	1.15	1.15	1.13
1.14	1.16	1.15	1.17	1.16	1.16
1.20	1,17	1.16	1.18	1.17	1.16
1.18	1.17	1.15	1.15	1.15	1.14
1.17	1.17	1.16	1.17	1.19	1.16
1.17	1.17	1.17	1.17	1.20	1.19
1.18	1.18	1.13	1.10	1.1:	1.10
1.19	1.19	1.18	1.15	1.21	11

114N OF RMS= 1.16

		TIME UN TAI	RGET CHECK)	
0.44	1.58	Legi-	2.91	2.4	٠٠٠ الم
4.71	5.76	6.59	7.10	1.50	5 🗸 🗸
9.51	10.65	11.53	12.15	12.50	11.75
14.66	15.66	16.41	16.59	1/.13	1 -16
14.18	20.20	20.29	20.73	21.57	• • • •
23.54	24.57	25.65	26.04	21.75	1. 1.
23,40	29.53	30.05	30.00	51.1"	•
32.52	53.48	34.45	35 • 52	30.000	· • ****
57.50	38,53	\$5.27	39.1.4	34.83	4 . 15
41.17	41.98	43.04	44.46	44.35	91.11
46.12	47.08	48.14	49 • 43	40000	. 17
50.72	51.74	52.53	52.73	53.40	. 4 · · · · · · · · · · · · · · · · · ·
77.22	26.23	76.31	96 • 4c .	57.42	• `4
58.98	59.98	61.03	01.75	62.45	• 11
63.50	64.61	65.15	65.61	62.677	1

RL test 4
RULL
JUN OF SINE WAVES FUNCTION

	ĸ	MS VALUE 0	F LRRCR		
1.13	0.00	1.45	1.1	0.70	1.52
0.94	1.04	0.58	1 • 1,1	1 • Jr	1.6
1.07	1.07	1.03	1.15	1.04	1.11
1.05	1.02	1.00	1.16	4.18	1.16
1.10	1.15	1.19	1.15	1.13	1.10
1.16	1.21	1.18	1.19	1.27	1.17
1.17	1.21	1.15	1.11	1.15	1 - 1 6
1.17	1.15	1 • 1 v	1 • 21	1.23	ı • 🤭 (ı
1.23	1.20	1.19	1.21	1.21	1.21
1.14	1.22	1.20	1.19	1.15	1.20
1.20	1.22	1.18	1.19	1.20	22
1.21	1.20	1.21	1.70	1.17	1 • 0 1
1.21	1.20	1.20	1 • 2 u	1.20	1 • 1 4
1.18	1.20	1.18	1.20	1.20	1.1 1
1.16	1.19	1.10	1 - 1:	1.17	1.15

0.96	2.01	5.00	4 • 0 3	*- • U 1	1.
6.65	7.71	3.66	8 • 14	2.660	15.51
11.58	12.63	13.64	13 • 👵 5	14.51	10000
16.0៦	17.10	10.14	18 • € 9	10.95	14.44
20.06	21.09	22.09	22.57	21.55	4.02
24.44	25.44	26.02	20.49	57.45	
29.50	30.55	31.54	:2 • 1 j	32.60	(• • • f
34.52	35.52	36.12	36 • ≥0	30.95	1.5
58.94	59.59	43.5℃	41.65	41.57	" · 1
43.11	44.06	45.12	45.59	41 .U?	ن ∔ ن
47.9₫	48.31	49.32	41.70	1 6 • 52	. • * . *
51.73	52.74	53.07	53.61	34.33	• 7
56.34	57.31	50.09	58 • 13	94.70	1.01
61.02	62.06	63.00	1.3.57	64.00	ખું 1 ત
6 v • 0 1	57.03	67.72	od • 21	64.77	. 73

RL test 5

RULL SUM OF SINE WAVES FUNCTION

	į.	MS VALUE U	FLEKKUR		
1.11	0.00	1.12	ن د • 0	မ 🕳 🕏 🖂	1.1
1.55	0.96	J •98	1.11	1.•9 t	ي المن المن ا
1.15	1.11	0.99	1.13	1.00	2.74
1.08	1.05	1.00	1 • U 9	1.11	1.66
0.94	1.05	1.09	1 • u 7	1.13	1.13
1.11	1.00	1.09	1・リソ	1.11	1.11
1.05	1.12	1.00	1 • 11	1.12	1.12
1.15	1.12	1.11	1.09	1.11	1.15
1.13	1.12	1.10	1.10	1.15	1.15
1.13	1.17	1.16	1.12	1.1:	1.14
1.13	1.14	1 - 18	1.16	1.16	1.15
1.14	1.15	1.13	1 • 14	1.15	1.1:
1.15	1.13	1.15	1.13	1.15	1.17
1.15	1.15	1.17	1 • 1 •	1.13	1.16
1.17	1.14	1.15	1.17	1.10	1.17

	- :	TIME ON TAI	RGET (SECS)	
0.81	1.85	2.81	3 · de	4.7t	49 · 10 h
5.91	6.89	7.91	8.94	9.91	10.12
11.21	12.28	13.21	14.00	14.36	1 . * *
16.39	17.18	18.25	19.20	20.19	20.19
21.52	22.29	23.32	24 - 50	24.37	. 11
25.90	20.92	27.33	20.57	20.87	
30.63	31.38	52.42	35.43	55.95	• • • • •
35.48	36.52	37.02	38 - 62	54.03	412
40.23	41.19	42.19	42.32	42.23	• 1
44.24	45.28	46.00	47.13	45.05	% 3 d 2
49.22	49.58	50.49	51.52	50.001	. 17
5:.27	54.27	55.31	55 • 9 7	56.67	47.33
55.02	59.04	_ b 0 • 0 7	L1.UB	61.35	1.
62.48	63.55	64.56	u5.40	១៦.•06	. • • •
66.63	67.23	68 ∙2 8	69 • 28	70.31	" Fig. 15 ha

RL test 6
RULL
SUM OF SINE WAYES FUNCTION

	к	MS VALUE O	F ERROR		
1.15	1.37	1.44	1.4/	1.2 /	' • t. 4
0.94	1.24	1.11	1.17	1.3:	1.00
1.62	0.98	1.11	1.00	1.51	1.3.
1.00	1.02	,1 • 0 b	1.05	1.01	1.654
1.04	1.05	1.07	1.07	1 • U 5	1.17
1.09	1.09	1.08	1 • 0.3	1.0%	1.10
1.07	1.10	1.02	1.16	1.ÚŁ	1.14
1.12	1.10	1.04	1.37	.1,11	1.16
1.09	1.10	1.07	1.09	1 • 0 c	1.05
1.11	1.12	1.09	1.08	1.09	1 - 37
1.09	1.11	1.13	1 • 09	1.05	1.11
1.14	1.10	1.09	1 • 10	1.10	1. 3
1.10	1.12	1.14	1.10	1.11	1.12
1.11	1.12	1.19	10.12	1.19	1
1.11	1.12	1.10	1.12	1.11	1.12

TIME ON TARGET (SECS)								
0.15	1.11	£ 0 0	3.09.	4 • 1 4	.1.			
6.2 0	7.26	8 • 28	9.24	16.24	10000			
11.66	12.06	15.00	14 • 65	15.71	i .71			
17.71	18.54	19.41	20 • +1	21.40	• 4 3			
22.98	23.43	24.40	47	24.21	v 🗸 5 5			
27.42	28.37	25.39	30.40	31.42	4 4 %			
\$2.75	33.50	34.50	an • ⊃2	3 € • 5 %	.77			
37.77	38.82	39.83	40 • 30	41.07	4 47			
43.13	45.47	44.72	45.12	4 tr • tr 4	.7 7			
43.32	49.31	50.37	51.32	52.32	· · · 1			
53.54	53.79	54.7x	55.75	56.12	7			
57.92	58.91	54.92	€0 • 39	61.95	1 .4 26			
63.41	63.95	<u>0</u> 4 • 6 ²	15.11	68.12				
67.61	68.47	υ9.5U	70.52	71.53	1. 10			
73-04	73.87	74.52	75.55	76.5	77-01			

HOLL
JUM OF SINE WAVES FUNCTION

RL test 7

	H	MS VALUE U	F ERROR		
2.74	2.25	1.70	1.47	1.50	1.45
1.40	1.63	1.70	1.61	1.42	1.47
1.54	1.49	1.52	1.50	1.4.	1.53
1.45	1.47	1.68	1.64	1.69	1. 6
1 ∙6 წ	1.69	1.67	1.64	1.00	1.64
1.60	1.63	1.63	1.51	1.59	1.50
1.70	1.06	1.66	1.53	1.64	1 - :- 1
1.61_	1.65	1.65	1.61	1.64	1 • • · · u
1.60	1.60	1.61	1.62	1.59	1.55
1.59	1.60	1.64	1.64	1.0€	1 - 6-4
1.64	1.64	1.65	1.53	1.62	1.62
1.62	1.59	1.62	1 • : 1	1.62	15
1.66	1.65	1.66	1.65	1.64	1.54
1.62	1.62	1.03	1 • 62	1 .tes	1.53
1.65	1.65	1.63	1.64	1.64	2 . 6 4

		TIME ON TAR	C T CECSI)	
0.00_	0.81	1.75	2 • 75	3.01	4.54
5.29	5.46	5.8:	6.25	7.95	7 • 9 3 T
9.09	9.59	4.61	10 • 73	11.31	11.70
12.46	12.96	12.95	13 • HO	14.51	14.03
15.03	15.24	16.24	17.13	1 4 . 1 5	1 . 1
19.21	19.53	19.76	20 • 40	21.53	91.40
21.92	22.68	23.65	24 - 60	9 t • 5 h	7
26.82	26.87	27.40	13.13	23.13	33.14
30.22	34.08	31.04	31 · 83	50.09	1.15
33.70	34.05	33.99	35 • 32	31.67	
\$5.65	57.14	35.13	39.17	46.15	4 1 4 4 4
41.09	41.57	41.65	42.35	4 5 . 4 .	44.44
43.83	44.08	45.14	40 • 17	41.00	4/01,4
48.22	48.21	4 5 • 81	49 • 61	50.59	1.14
51.18	51.63	52.33	F 2 _ 1,1}	54.49	4 4

RL test 8

RCLL SUM OF SINE WAVES FUNCTION

	R	MS VALUE O	F ERRUR		
0.00	2.10	1.11	1.57	1.52	1.J2
1.19	1.24	1.17	1.58	1.21	1.45
1.41	1.49	1.55	1 • 4 4	1.95	1.40
1.44	1.47	1 • 48	1.52	1.45	1.47
1.49	1.41	1.39	1.41	1.41	1.50
1.35	1.42	1.40	1.41	1.50	1.1
1.39	1.38	1.39	1 • • 1	1.35	1 4
1.48	1.49	1.47	1.45	1.50	1.45
1.48	1.53	1.48	1.48	1.50	1 • : 0
1.53	1.51	1.51	1.51	1.50	1 . 4 . *
1.48	1.50	1.50	1 • 46	1.40	1.40
1.49	1.49	1.51	1 • 40	1.49	1.45
1.47	1.46	1.49	1 • • 9	1.46	1 - + C
1.47	1.46	1.48	1.90	1.4 %	1 • 4 7
1.46	1.46	1.47	1.46	1.45	1.17

TIME ON TARGET (SECS)								
0.98	1.00	2.06	3 🗸 🐣	4.11	• . 1			
5.61	6.10	6.28	7.09	0 • U 14	• •			
8.88	9.14	9.35	10.00	11.04	11.			
11.78	12.09	15.10	14.11	14.89	1 4 3			
15.91	16.34	16.90	17.43	10.4	1			
19.55	20.26	20.62	21.19	27.00	7			
23.44	23.93	24.45	74.49	24.41	• •			
25•0ช	25.52	25.60	26.54	20.00	. 1			
28.47	28.75	29.14	30 . 04	31.04	. 1			
31.67	32.12	32.93	33 • 6 ≈	34.39	69.14			
36.54	36.63	37.63	38 - 55	54.65	7			
40.63	40.67	41.72	42 • 45	45.74	9:5.57			
44.98	45.66	46.06	47.64	47.50	4 4			
48.61	49-11	49.47	50.52	51.56	1.01			
52.53	55-57	53.36	4 - 1 1	55-17	* 1 - 1 - 1 - 1			

RL test 9

RCLL
SUM OF SINE WAVES FUNCTION

	•	RMS VALUE	OF ERROR		
1	•9b 1•3	7 1.12	0.70	1.20	1.20
1 .	• 39 1 • 1	1.28	1.11	1.25	4
1	•27 1.1	1 1.51	4.81	1.14	1.20
1.	.22 1.2	4 1,21	1 • 23	1.23	1 - 54
1	.51 1.2	5 1.33	1.31	1.29	1.40
1.	•46 1•4	5 1.46	1.46	1.41	1.43
1	•40 1.4	2 1.40	1 • 58	1.41	i • 4 d
	. 39 1.4	4 1 22	1.49	2.41	1.41
1	•41 1.4	2 1.30	1.41	1.41	4.41
1	.39 1.3	8 1.41	1.42	1.47	1.45
1.	.42 1.4	2 1.41	1.41	1.35	1 - 4 4
1	.45 1,.4	3, 1.42	1 • 44	1.43	1.40
1.	-46 1.4	4 1.44	1.44	1.44	1.43
13	44 1.4	3 1.40	1 - 42	1.64	. 4 -
1	.44 1.4	4 1.43	1.43	1.46	• • •

		TIME UN TAI	RGET CSECS)	
0.41	0.96	<u> </u>	<u></u> 2•99	* • 2 (•
4.36	5.39	6.41	7.41	5.01	€ € 4 €
9.68	10.86	11.65	12.28	12.70	15.35
13.75	14.31	15.33	15.75	1 6 • 2 ₺	10.51
17.58	17.78	18.28	19.19	19.79	15.79
20.09	20.75	21.77	22 • 78	23.08	. 9.38
25.09	25.65	26.02	27 • UZ	27.1	. S. 92
28.58	29.04	30.04	36.45	31.2.	1. 5
32.24	. 34.67	33,65	53.98	34.4	7
36.15	30.19	57.24	37.52	57.77	10000
39,82	40.23	41.27	42.51	4 5 . 0 1	4 . 2
43.94	44.58	45.59	46.22	40.57	· . · 7 ·
47.66	48.71	49 eka	5ŷ•33	20.42	**** 17 L
51.94	52·68	53.37	53 • 9≥	o 5.98	24.02
55.61	56.18	57.17	57 • 54	57.54	* * * ?

RL test 10

ROLL
SUM OF SINE WAVES FUNCTION

	k	MS VALUE O)F		
1.13	2.10	1.00	1 • 47	1.50	1.45
1.39	1.24	1.20	1.4.51	1.39	. • • • •
1.27	1.26	1.10	1.21	1.23	1.14
1.25	131	1.13	1.15	1.13	1.15
1.17	1.15	1.15	1.18	1.13	1.16
1.14	1.16	1.16	1.12	1.17	1.05
1.19	1.18	1.19	1.21	1.22	1.15
1.19	1.20	1.14	1.18	1.20	: • 1 - 1
1.17	1.17	1.15	1.13	1.15	1.1
1.18	1.17	1.16	1.15	1.17	
1.20	1.19	1.13	1.17	1.17	1.17
1.15	1.16	1.17	1.15	1.17	17
1.15	1.15	1.16	1.16	1.14	1.13
1.16	1.15	1.14	1.16	1.6	1.15
1.10	1.14	1.16	1.1	1-14	4

MEAN OF K/S= 1.18

1	TME	13 NI	TARGET	(SECS)
	1 1 17 1 7	UIN	4 A K () 1	(311.5)

0.81	1.16	1.06	1 • 1	7. 6 to 8	6.43
4.43	5.41	b • 46	7.43	0	• 51
9.33	10.28	11.08	11.95	12.00€	1
14.68	15.68	15.68	17.55	10.50	1 - 4
19.84	20.79	21.15	21.50	27.54	
24.63	25.68	26.64	26.53	26.095	
28.45	29,45	50.1c	30 • 40	31.31	4.5%
33.07	34.68	35.07	35 • 76	36.82	1.18
53.02	39.52	40.85	41	4	47.77
44.26	45.48	40.37	47.08	47.70	4 5 g 1 st
48.76	49.81	50 •54	51 - 42	51.5:	• • 7
53.53	54.58	55.44	56 • 17	See. St	2/042
50.30	59.42	60.32	_ 60 • 51	1.1.50	
63.32	64.03	65.01	65.53	bb.46	1. 4. 4. 40
68.52	64.42	70.21	73 . 56	71.00	· 7

RL test 11

ROLL
SUM OF SINE WAVES FUNCTION

	к	MS VALUE O	F EKR IR		
2.76	1.92	1.70	1.47	1.57	1.20
1.45	1.30	1.43	1.16	1.0	
1.34	1.51	1.37	1.27	1.29	1
1.25	1.26	1.16	1.15	1.1:	1.26
1.17	1.23	1.17	1.22	1.1%	1.14
1.15	1.16	1 + 1 7	1.19	1.1/	17
1.17	1.21	1.19	1 - 10	1.17	1.17
1.15	1.18	1.17	1.15	1.11	1.7
1.19	1.19	1.19	1.18	1.15	1.00
1.18	1.17	1.16	1.15	1.21	1.1.
1.18	1.19	1.10	1 - 17	1.13	1.1:
1.18	117	1.19	1.15	1 • 1:	1.1
1.20	1.16	1.14	1.17	1.20	1
1.19	1.19	1.21	1.19	1.1	1.1
1.1)	1.18	1.18	1.18	1.1.	

1EAN OF KMS= 1.20

0.19	1.25	11Mt UN TA	51	4.23	. 01
5.15	b • 16	7.24	7.45	e • 3 €	4.
9.94	10.93	11.09	12.00	15.55	14.14
15.34	16.09	17.06	18.37	19.10	27.15
20.46	21.39	22.34	23.40	23.3	. 4.
25.39	26.39	26.59	27.55	28.55	25.75
29.27	30.27	31.25	32 • 50	33.30	
35.32	36.05	37.04	37.74	37.92	4.5
58.47	39.29	4 <u>૫,•</u> ૩૫	41.53	43.50	4 47
45.87	44.30	45.18	46.19	47.22	47.15
47.89	48.39	49.38	50 • 25	50.50	~ 1 . ϵ_{C}
52.67	53.63	54.12	55.12	56.65	· 1 • 2 · 1
57.31	50.32	59.32	60 • 41	့ သပ်ခြင်းပါ	1.
62.55	62.55	62.91	∪3 • 36	63.83	· 4 • t. ti
65.50	66.35	67.37	نفت بديد	ALCOHOL: The second	F

RL test 12

RULL SUM OF SINE WAVES FUNCTION

	Ri	MS VALUETO	F ERKIR		
1.14	1.57	1.10	U • > 7	ម•ស្ភ	1.11
1.05	0.96	0.58	1.05	1.05	1.1.
1.02	0.98	1.03	0 • 36	1 • 0 4	3 - 28
ب 0 و 1	1.08	1.03	1 • 0.5		1.31
1.02	1.09	1.04	0 +	1.00	1.27
1.05	1.07	1.09	1.07	1.65	
1 • 0 b	1.Ú6	1.06	0. 19	1.04	1.37
1.04	1.06	1.05		1,1,•0f	
1.11	1.04	1.05	1 - 0.5	J.95	1.33
1.03	1.00	1.05	1.03	1 . 0 .	1
1.04	1.05	1.03	1 • 0 ±	1.00	
1.02	1.31	1.03	1.02	4.61	1.62
1.03	1.62	1.02	1.32	1.02	5
1.01	1.03	1.05	1.35	1.02	1
1.03	1.05	1.04	. 1.05	1.04	5

TIME UN TARGET (ÇCCE)								
0.81	1.98	2.61	3.64	4 • 60	• 45.5			
6.66	7.69	8 • 49	9•:0	10.00	. 1. 1. 3			
11.85	12.68	13.81	14.5	1 b • 655	ί. 🗸 ί			
17.61	18.35	19.58	20.57	21.54				
23.59	23.87	24,•52	25 • 90	24.€75	7 🚅 🤨 🕶			
28.92	29.52	29.95	30 • 74	31.57	1			
33.49	34.99	35.98	-7-1:2	.\$ 0 00				
40.05	41.05	42.04	43.64	44.00	11			
46.13	47.12	48,•09	49.12	50.35	* 1 . 3 %			
52.03	52.61	53.62	៦4 • ១៦	D: •64	• 19 8			
57.07	<u>58•6</u> 8	57.72	n0 • 12	61.7.	. 13			
65.73	b4.56	65.60	56 • 57	31.5a	3.5 .			
69.15	59.33	<u> 70.67</u> .	71 • ab	7: •37	7:003			
7+.92	75.52	16.05	77 . JE	70.00	7 . 36			
79.68	30.40	aŭ•97	S1 • 21	85.00	· · • i U			

RL test 13

HOLL SUM OF SINE WAYES FUNCTION .

	4.1	4S VALUE OF	1 R K . H		
1.50	1.34	1 • 4 4	1.57	1.12	1.11
1.14	1.2.17	. 1.11	1.1	1.01	3
1.15	1.15	1.11	1.7	٠٠ ل 🕳 1	1.14
1 • 0 •	1.05	1.10	1 • 1 1	1.11	1-11
1 • 0 1.	1 • 1 1	1.69	1 • 100	1.J	1.13
1.11	1 • 1 1	1.12	1 • 13	1.0.	
1.12	1.12	1.05	1.16	1.12	1
1.19			1 • 11	4.1.	1 + 1 0
1.05	1 • 1 û	1.09	1 - 33	U.S	
1.00	1.10	1.09	1 • 11	1 • 1 1	(+
1.0 +	1.09	1.10	1 • 08	1.0 .	1.10
1.09	1.09	1.11	1.07	1.00	1 - 1
1.00	1.08	1.11	1.00	4.00	
1.01	1. L. V.	1.03	1 • (7	$1 \bullet 5$	1. J. J
1.08	1.07	1.05	1 • 3 5	د ن د ن	. • . ?

MIAN OF KMS= 1.09

		TIM: UN TAI	ROLL CIECS)	
0.43	1.41	Leye	2.75		• • •
ა∙78	6.51	7.53	8.55	2 4	1
11.15	12.13	12.74	13.00	1 4 . 4 *	• • • • • •
16.49	17.25	17.03	20.43	10000	
21.29	22.43	22.70	43.45	20.00	14 🙀 5 7
20•68	26.44	21.33	25 • 20	2 - 634	. 4.2
30.24	<u>51.06</u>	32.08	\$2.49	33.54	· . 2
55.45	36.49	36.92	37 · nc	პე•აი	5 D . 5 m
43.87	41.39	42.37	45.1	4 1 . 0 (~ ~ • 57
40.60	46.41	47.48	45 • 43	49.40	Ů • + 1.
51.46	22.12	52.77	. 55.44	54.42	11 1 4 A 1
5ე• წ2	56.39	57.33	70.32	59.33	• 5 1
: 1. ± 27	<u> </u>	. 2.2.697	44. 35	50. 0€	·· • 4.1
67.03	58.€b	こう・リロ	70 • J/	71.3%	7
72.98	73+25	74.25	75 • 2	15	. 7 . 1 7

RL test 14

ROLE SUM OF SINE WAYES FUNCTION

	ĸ	MS VALUE O	F ERFOR		
1.12	1.57	1.71	1.24	1.5 /	1.60
1.11	1.29	1.05	1.21	1.50	6
1.15	1.11	1.07	1.04	1.14	1.30
1.14	1 • 0 p	1.13	1.60	1.11	t • oʻ≠
0.94	1.34	1.02	1.37	1 • Ú ·	• ** 5
1.05	1.07	1.67	1.36	1.06	1.04
1.06	1.06	1.03	1.09	0.113	1.11
1.00	1.03	La li L	L 20 € 1155	1.00	<u>انوال</u> و لم
0.77	1.02	1.05	1 • 04.	1.64	1 1 1 4
1.01	1.43	1.00	1 • 1	1.0%	1
1.05	1.04	0.49	1.03	1.05	13
1.04	1.02	1.00	1.31	1.91	1
1.51	1.05	1.04	1.03	1.32	1.02
1.01	1.04	1.00	1 • • •	1.32	
1.03	1.05	0. 98	i • • •	رُ ن • ن	1.02

#L4N OF RMS= 1.05

		_	
TIME	ri N	TARGET	(5)(0)

				•	
 0.95		1.46	2, 49	ا (دروان	40 2
4.95	5.94	6.96	7. ∋3	H . ** t	,
10.98	12,00	13.01	14 • ti 1	1 ~ • 0 4	10.0
16.23	17.06	18.04	19.05	ن 1 • 1 ت	19
22.1v.	25.14	2414	25.12	w w e taut	. 7
21.60	20.21	24.23	30.24	31.00	· 🔥 🕹
33.12	ځا و لا کــــــ	31.Q9	35.34	37.10	
39.13	40.10	41.12	42.15	40.12	4. 4.2
44.L6	45.54.	46.00	47.7	ಆವ.50	9
49.80	50.87	51.91	52 • c8	55.85	11.0 4
. 25.62	50.42	27.04	ಬರ•೮೮	5° • 0 €	
61.09	04.03	o2.63	63.55	64.65	• t. t.
. 66.a8	57_52	68.422		70.23	1
71.72	72.77	/3•∂ნ	74.75	75.76	7 . 73
77.77	78.75	19.40	<i>i</i> ≤0 • ↓3	51.32	•

SF test 1

SUM OF SINE WAVES FUNCTION

	RMSTVALT	DE TOFTERROR	ξ	···		-
2.47	2.22	1.659	1.74	1.00	. • / 0	
 1.75	1.92	5 -15	2.34	- 1777	. ;	
1.92	1.98	1 - 20	$1 \cdot j \hat{n}$	1.78	. • :	
1.31	1-88-	1.89	1.36	1.77	: • i ·	
1.85 .	1.55	1.03	1.55	1.75	. · · ·	
 1.81	1.82	-1-81		1.77	1 • (•	-
1.00	1.82	1.82	1 • 7 :	1.75	• ' /	
 1.77	1.77	1.83	45.	7.	1 • 17	
1.83	1.54	1.33	1.50	1 • 8 3	•	
1.80	1.77	1-\$3	1 • 7 5	1.34	1.	
1.35	1.03	1.02	1.73	1.78		
 1.79	-1-79	176		1.81	. • 1	
1.84	1.85	1.81	1 • 32	1.61		
 1.00	1 ead	17			1. 4	
1.59	1 • 69	1.68	1 🕶 ಚರ	1.50		

v.21 -	U.bi		- · · · · · · · · · · · · · · · · · · ·	TT 5 • ∠ H	1.51
4 • 4 0		4 • 6 5		t. • 3 t/	•
			9 -•-04	– 1 u • û d−− –	10.+1
10.81	10.84	11.29	12 • 35	12.41	12.
15.01		14.03 —	·14.31 · · · ·	14.65 ··	1
15.06	15.51	16.51	17.51	18.11	1 . 1 .
18.75	- i7.09	- 19.20	20 - 25	21.25	- 21.
21.75		22.13		23•७7	
- ين و و ا					27.17
20.29	28.78	20.78	20.15	ವ ⊹•ಕರಿ	2 😽 7
29.78	27.92	·うひ。サマー・・	51.~yu-	- 33.48	22. 1
33.39	33.69	34.07	34 • 04	54.07	34.50
44.39 -	- 5年• ラ5	- ქი. 9 ე	~35 • 15	37.39	3-1-
30.34	30.64	35.52	55 • 14	30.10	5 1 .

SF test 2

RULE SUM OF SINE WAVESTFUNCTION

	RMS VALU	E JE ERKOR			_
2.04	2.93	3•33	÷ • J.	1 • 1	1.70
 7-77-	1.77	1-75	1 . 73	1 1 1 45 7 1 1	1.53
1.27	1.65	1.5%	1.00	1.4	1.73
	1.55	- T.62	1	1.7	1. 3
1.45	1.49	1.52	1 - 4	1 • 4 7	1 • • 7
 1.45	-1-99	" 1 "•55 """	1.55	1.51	1.50
1.47	1.55	1.50	1.10	1.57	1
 	1-1-	1.5/		175E	7 1.75 TT
1.33	7 د م 1	1.50	1	1.52	1.
 -	1:- 56	··· + 55- ···	1 . 74	1 • D 4	1.00
1.5+	1.54	1.05	1	1.51	$1 \cdot 1$
 	1.51	t-5u	~ <u>~ 1</u> .	* 1.5U	- 1.47
1.50	1.50	1.51	$1 \cdot 1$	1.50	1 • n · i
 1.49			1.71	1.51	1.00
1.49	1.51	1.50	$1 \leftarrow -1$	1.50	1 . +1

	TIAE ON TA	RGET (BECS			2.13
v • v 1			1 • 4 J 4 • 1 ÷	2.01 7:	75
5.04 					
11.65	12.04	12.16	12, 9	10.50	14.55 13.15
15.53		15 •15 15 •15 15 •15	1/4/3	11.1. 26.7	21.1
18.78 21.55	18.85	- 22.JU	- 12.42	27.40	00.12
23.60	25.72	24.02	24.32	21.31	ପିଥା•ାରିଟ ଦଳ ଫୁଟ•ୁସ୍ପ ଅଟି
25-82	25-79		<u>2</u> 1.55 	5 - 30 U	55.45
კყ.დმ ქ4.52°°	ან.14 - ახ.2Մ	35.46	35.14	· 6 • 9 ·	57.55
50.52	30.94	39.29	31.	46.45	41.02 45.67
41.92	91.51	44.77	42.10	90.97 91.22	41.65
44.54	44.38	44 a 11 	- 45.15 °		· · - 4 17 • 17 ! -

SF test 3

ROLL
SUM OF SINE WAVES FUNCTION

	RMS VALU	E DE ERRO	,		
u • U L	0.7c	O • tr •		∵ •	1.25
 1.76	1.46	1.53	1.71	1.46	1.95
1.36	1.32	1.51	1 - 1 >	الله • ما	1.55
1.41	1.33	1.34	1. 2	1.21	1.41
1.43 .	1.42	1.50	1.50	1.2:	1.7
1.55	1.58	1.57	1.14	1.56	1.40
1.44	1.44	1.59	i • /	1.40	1
 1.41	11	- 1.40 ···	1.17	1.42	1.57
1.41	1.41	1.40	1.41	4.41	1.41
 -1.41	1-41	1.40	1 • '4	1.43	1.50
1.42	1.40	1.57	i.	i • 4 u	1.41
1.45	1.40	1.4.	1.441	1.41	1.42
1.45	1.42	1 • 4 1	1 5	1.43	1.1
 1.40		1 .37	1.50	1.3	1.4%
1.39	1.59	1.30	$1 \bullet : \mathcal{D}$	47	1 • 54

	4 1.51		·· · · 3 • r 1	5.001	. • 3
4.33	4.46	5.41	5 • 4 1	54	7.1.
		7.83	y .y	• ₩ • ₽ ₩°	- 10 · 15
10.23	10.68	11.53	11. +	1	$1 \leq \bullet \neq 1$
13.05	15-45	······································	13.10	15.30	10.00
16.81	17.34	15.35	13. 30	1 44	13
19.99	21.02	~~ ~~ 22.02 · · · ·	25.34	25.44	22.77
24.37	24.58	24.79	24.57	23.83	26. • # 1
··· 25 • 55				~ ''ለ₩•ቑሕ' ''	10.17
30 •∠8	31.25	32.30	33.34	24.00	54.53
34.67	35.45	35.43	21.42	53.18	3000
30.49	39.34	40.38	41 · 23	42.09	42.17
- 42.7E		45.87	44.44	45.44	45.74
4 n • 3 u	47.53	48.37	48 - 14	4 2 . 77	3 J • ∪ J

SF test 4

RULE SINE WAVESTFUNCTION

		KYS TVAL	JE OF ERRI	₹		
	Jack	0.30	وا الأ⇔ال	1 7	t.7.	1 • 1 U
•• •• ••	1.13	1.35		1.1	1.11	~~ 1. 20~~~~
	1.13	1.42	1.37	: 🗸 • 7	1.23	1 • 1 7
	1.19	1.24	1.16	1.15	1.03	1.1
	1.15	1.11	1.11	1.15	1.15	1 • 1 =
	1.21	1.14	1-12	1.12	. 1.•0.	1 • 1 .
	1.14	1.15	1.1:	$1 \bullet 1^{-1}$	1.15	1.17
	1.08		1.1	11-6		1.12
	1.04	1.UR	1.00	1 • i 3	1.12	1.12
	1.10	1.10	1.12	····1·•11	1.12	1-10
	1.12	1.11	1.10	1.12	1.13	1.1.
	1.19	1-17	Y • 12:	- 1 • 1 ·	1.17	1.17
	1.17	1.17	1.19	1 • 2 5	1.13	1.15
	1.17	1-16	1.50	minima domini	j.#.3.p	······ 1 · · · · ·
	1.21	1.13	1.20	1.17	1.17	1 + 1 :

	1.05		4kGET (SECS 2•5~		ं व्यक्तिक व्यक्ति	* * * * * * * * * * * * * * * * * * *
	ŭ 3	0.61	7.1j	7 • 40	21	4. 1
	-10.25	10.60			~~ ~~ } (* • 6 4 °	113771
	14.75	15.43	16.31	17.4.28	17.63	10.54
	17.45	20.59	21.57	22.15	120.33	25.27
	25.00	24.43	25.33	26.34	25.65	27.5%
-	21.62	25.12	·····	- 29.00 ·	38.99	31.71
	36.93	35.97	34.94	55.17	35.65	57.57
-	38 . 45	-38 · 8 2		40.75	~ # T• Z5 ~	420074 "
	43.27	43.37	44.51	74 . 72	45.24	45.60
	45.31	45.55	45 295	·····47•727 ···	· · · · 36 / · · ·	48.38
	4 2 5	47.24	o 0 • 0 o	50 • ∉ 7	51.93	52.52
	52.74	23.39	" ೨೨.೮5 "	54.47	55.65	35.2
	51.21	37.86	57.36	9 5 • 34	មួ 🚜 និង	ns to 🕳 😚 😅
		m % . 4 M		្រក ក្នុង «ប្រៀ	24.46	55. 11

SF test 5

VOLE
JUM OF SINE WAVESTRUNCTIONS TO THE TOTAL TO THE TRANSPORTED TO THE TOTAL TO THE TOTAL TOTAL TO THE TRANSPORTED TO THE TOTAL TOTAL TO THE TRANSPORTED TO THE TOTAL TOTAL TOTAL TOTAL TO THE TRANSPORTED TO THE TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL TO THE TOTAL TOTA

		RMSTVALUE	OF ERROI	· ·		
	3	_ • = 1	2.23	1 - 19	• °	. • ** · •
	2.10	2 • 45		2.15	2.75	1 3 • 5 · · · · · · ·
	2.21	2 • 20	19	2.55	. • 3 9	· 1
•	2.05	2.14	2.09	2.1,	C 1 . "	2.15
	2.11	2.00	2.05	2.55	2° • Ú 4	~ • U 4
	2.01	2.05	72.03	2. 10	1.94	2 . 12.4
	1.98	1.97	1.90	1 • 19	1.000	2.00
	2.65	2.13	-2.15	5 • 1.1	"" 1:12	1 12 • U 1 1 1
	2.07	2.36	2.05	2.11	2.04	$z \bullet \mathcal{C}$.
-	2.01	~2.03 ~~~	~ 2 0 0 5 ° °	* 2.J2	2.00	2.001
	2 . 04	೭.05	2.03	•	€.02	± • 3 €
	2.04	2.03	72405 77	4 •	2.02	2.15
	2.10	2.10	2.15	2 + 3 4	√.12	a • 1 ·
	2.14	2015	2.14	7.12	~~ ~~ 1 4 ~~	72:12
	2.13	2.11	2.04	2 • 39	2.03	2 • 3 •

MMAN OF RMS: 2.03

	TIME ON TA	RGET (SECT			
0.1:	1.05	1.95	2 . C	2 6 5 T	5.11
5.436	3.40	4.54	1	70.00	• • 1
5.16-	t-8t		t.:3		1
ラ・1 パ	3.26	9 · c 9	9.00	* • * *	10.00
10.54 "	··· 11.55 ···	11.75	12. 3	1.5000	13.30
14.01	14.56	15.58	15.01	17.0	17.00
19.46	17.41	1.941	19. 5	23.50	23.57
26.72	20.72	21.27	22.03	20.15	25.14
	25.89		2 4	7 2 m • 5 y = 7	25.12
26.45	26.50	27.27	28.13	.* • 1:	23.50
29.35	-29-84		13 1 . 78	30.21	32.44
32.60	33.15	33.72	34.45	44.33	34.16
24.91	35.38	**************************************	35 . 10	37.24	57.20
57.55	37.74	34 · 83	5 9 . ∞8	1004	40.2
91.17	···	92.11 -	45.1	99.11	44.17

SF test 6

HOLE
SUM OF SINE WAVESTFUNCTION TO THE TOTAL THE TOTAL TO THE TOTAL TOTAL TO THE TO

•		RMSTVAL				
	: • · J	ج . 0 م	1.60	1 - 7	1.7	. • 1
	1.65	1.52	1.70	1. 1	1.54	1.64
	1.54	1.76	1.72	1.71	1.64	1.600
	T:57 T	T-61	T.68	" 1 • 6 3	1.50	1.53
	1.61	1.07	1.57	2 6 5 4	1.60	1.5%
*	1.51	1.60	7.55	1 4 69	1.52	1.60
	1.61	1.01	1.01	1.5	1.5"	1.00
	1.558	1755	1-55	-1. (3)	1.50	1.500
	1.01	1.09	1.558	1	1 • 0 €	1 • 1040
• .	1.55	PC-1	7.63	1.1	1.69	1.5 / ~ ~
	1.50	1.56	1.50	1.:7	1 • 5 h	1.7
	1.55	-1.57	শা ন্ত ত	1.50	1.50	1.500
	i • • 1	1.51	1.51	1 • • 3	1	1 . 4 .
•	1.49		1.47	1. -50	1.43	1:44
	1.45	1.47	1.48	1 • 45	1.44	1.70

0.46	1.19	1-88-	1 . 15	2.5	2.00
4.20	4.56	4.58	5 🗸 🕫	n • 5 4	7.24
	7 		·= -9 • 53 ·=	1が・カン ・	11.35
11.91	12.31	12.58	13.1	10.484	14 - 74
14.45	14.88 ***	- 15.76	16.05	17.56	17: • 75
19.11	19.41	19.86	19.50	20.73	21.74
21.71	22.58	23.68 ···	25.03	26.92	70.00A
20.40	20.85	20.68	27 • 3 c	27.57	27.00
	28.77	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	∵ 3U•J7	50.75	51.52
32.57	52.92	32.90	აპ • 🗀 🕆	34.30	35.30
35.87	პ ნ∙ 88	27.55	57.59	347	56.07
40.24	40.05	41.66	42. 19	43.71	44.00
44.59	43.52	46 eb1	47.17	भ ५ • छ छ	49.13
56.65	24-04	51.22	51.35	51.9c	58.65
··· 55 • 5·1 ··· ···				ייי מיד • לכ	さん・ラー・

SF test 7

KOLL SUM OF SIGE WAVES FUNCTION -----

		KYS TVAL	リピージアーと それりゃ		*		
	5	£ •73	2.24	3.50	2.1.	1.13	
	:: 	2.19	2.49	2.44	Z.55	9	
	.i • b u	2.77	2.63	2.00	2.65€	2.4	
	∵2.50	2.55	2.51	2.51	2.52	2.63	
	2.51 .	2.77	2.71	2 • /1		2.5	
	2.55 20	2.77	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	- 2.15	"d • 3 4	1 • > U	-
	2.75	2.78	2.75	2.51	2.36	2.79	
				2. r1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	· > • • • •	
	2.37	2.06	2.65	2 •∪	2.80	$2 \bullet Im$	
	2.73	2.75		- 2.76	2.77	- 2 · 7 ·	
	2.79	2.76	2.76	2.1-	2.72	2.72	
-	2.71	~2.71	2.71	2.1.9	'• 5४ °	2.70	
	2.80	2.35	2.63	2 • .1	• 51	3 • 8 €	
	-2.79		 -	2.15		12.15	
	2.75	2.74	2.73	2.71	7.71	2.7.	

T I	M =	ON	T	ARG.	· T	100	

	1 2 11 2 0 10 1 7		• •			
0 • U 1 =			- ··· 1 .68	2.06	2000	
2.75	2.76	2.76	3 • ∪ 1	* • 4 I		
		- 5 .88	—— 5 • ১৪ —	· · · • • • • • •	7.15	
7.ob	7.68	3.03	8 🗸 ə 3	d •30	1.26	
3.31	ყ •38	· 7 • 15 · · ·	7.17	10.14	10.75	
10.94	10.76	10.94	11.43	11.58	11./1	
11.75 -	" 12.18"	-12.10	· 12.10	12.41	15.35	
13.53	13.61	13.61	13.00	11.493	14.01	
14.59	14-, 70		15·78	16.50	15.76	-
15.90	17.29	17.51	17.55	17.65	17.5.	
"17.99 ···	19.03	19:79	19.1	20.97	20.74	
21.34	21.29	22.03	22.50	298	22.036	
23.25	23.22	- 25.53 -	24.05	24.35	24.70	
೭೪೦೮೨	25.08	25.69	26.12	26.43	25.75	
	27.00		څر و اج	29.40	34.43	

SF test 8

ROLL SUM OF SINEMANESMEUNCHIUNMAN M

		*			
4 • 2 7	z • 95	6.95	2.50	2 € 6. •	• 4 3
 2.54	72.46	2.41	2 1	2.31	2.24
2.2	2.40	2.53	2.	2.37	2.54
 2.26	7.2.28	2.57	2.55	3 • 2 8	2.70
2.29	2.29	2.50	2 • : 2	2.29	2.51
 2.32	5.58	2.28	1 1 2 . 30 1	7.41	2.4
2.42	2.44	2.44	2.40	2 • 3 :1	2.50
 ~~ 35	2.57	2.57		7 2 3 3 3 7 7 7 7	2.30
2.51	2.36	2.41	2.41	2.039	2.4
 72•3s 1 ""	7 2 - 34 7 7	2.36	7.34	2.53	2.52
2.50	2.37	2.37	2 • 55	2.54	2.33
 2.54	- 2°• 35 ···	2-31	~~2 • 5 C	2.29	2.50
2.2	2.33	2.52	2 • 54	2.33	2.43
	2.32	2.33	2.52	2.31	1 2 3 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
2.29	2.34	2 • 3 t	2.56	2.34	2.34

MFAN OF RMS=2.34

	TIME ON TH	ARGET (SECS	.)		
0.05	່ "ປ•2ສ່າ		0.54	1.31	2.14
2.91	3 • 0 5	3.36	3.00	5.55	4.71
4.74		cu	~~ ~5 • 75 ~~	-7.91	7.50
7.55	7 • ७७	8.01	8•33	3.53	3 • 54
8.37	~ ታ. 26~	y-18	9.14	10.84	10.81
11.26	11.81	11.99	121	12.10	12. 5
12.55	- 12.61 -	···· =1:5:• tr5 ··· ···	13. 41	14.21	16.01
10.30	15.30	15.81	15.71	17.50	1 4-34
18.50	15.66	10.70	- ~ ty 22	20.09	20.18
20.45	20.92	21.32	21.54	22.57	22.7
22.89	25.15	23 -18	24.05	23.08	25.19
25.04	25.97	26.30	26.15	≥1.00°	27.33
27.74	27.70	27.95	21.91	27.97	28 · 47
25.53	28.80	29.27	29 . 7	2.9 . 37	:0.7
319-64-4		31.03	٠ ا و الحاد	32.62	32.75

SF test 9

ROLL
SUM OF SINE WAVES FUNCTION

	RMSTVALI	JE OF ERRO	(
0.0	0 1.7%	0.31	1.77	1.0	1.54
1.57	1.42	1.52	1.72	1.63	1167
1.71	1.73	1.70	1 • 49	1.57	1 • : 4
1.61	1.65	1.78	~~1 • / ô	1.79	1.71
1.04	. 1.69	1.74	1 • ∪ 9	1.69	4 • • • • •
- 1.72	1.68	1.68	1.17	1.75	1.74
1.70	1.68	1.65	1.69	1.70	1.07
1.6by	1.64	1.70	1.77	1.70-	1. t
1.60	1.55	1.67	1 - 4	1.67	1 • • 7
1.66	1.006	1-72		1.72	1.72
1.7ú	1.71	1.70	1.71	1.50	1.47
1.71		1.72	1.72		1.71
1.79	1.59	1.69	1.71	1.71	1.57
		1.67		-1 •- <i>t</i> -1-	1-71
1.71	1.72	1.73	1.73	1.71	1.73

	TIME ON TAR	RGET (SECS)			
ឋ∍ម៦ា	· · · · · · · · · · · · · · · · · · ·	1.45	1.78	13	7.440
3.75	4.51	4.75	4.73	5 • 1 ·s	". • 'D
 	7.11	7.25	··-8•39	: - 3 - 4 U	フェラミニー
9.03	10.19	10.21	10.00	11.91	1.1.1
13.95 -	14.75	14.71	7 15 - 18	15.58	16.11 "
16.39	17.28	17.39	17. এট	1 1 • 1 5	19.11
 20.10	21.17	21 •42	fil.52	22.52	23.48
23.40	24.07	24.07	34 . 15	23.37	20.34
 21-34	28.38	28.72	~~ ## # J 5~~ ~	T 50€08 T	1150.TW 11
30.70	31.15	31.19	31.75	36.44	38.00€
33.52	- 53-99	54 - 57	35.59	36.50	57.30
35.03	38.Ú3	5 a • 50	38.79	54.17	40.11
41.18	41.55	41.91	42 • 35	43.03	43.57
44.12	44.58	44.99	45.01	40.95	40.40
 4 6			98 - 1.7	· 44,94 ·	50-52

SF test 10

٠.

HOLL SOM OF STRE WAVES FUNCTIONS ----

the state of the s	RMSTVALUE	CONTRACT			
2.47	5 • 7 U	5.≥9		. • 1.4	• •• •
2.51	2.36	7.19	A . L	77.11	2.0;
1.93	1.93	1.00	i • . J	1.050	1.73
1.71	···1.70	1.64	1	1.39	1.52
1.63	1.60	1.66	1	1.07	1.00
1.62	-1.51	~1.62~~~	1.	1.5/	1.7
1.54	1.59	1.57	1.49	1.50	1.
1 544-	-1-45				
1.40	1.44	1.44	1.43	1.4.	1.45
1.40	1.42	1 ~4 U	1.17	1.50	· -
1.51	1.51	1.50	1.49	1.40	1
1.47	1.47		-1.45	1.44	1 • •
1 • 44	1.46	1.44	1.44	1 • 4 4 1 • 4 4	1 • 0 %
1.45	-1-42	-1-4-1	1.41	1.44	1 . 4
1.40	1.42	1.41	1.71	1.41	1.40

MUAN OF RUS= 1.54

TIME ON TARGET (SECS) 0.25 - 0.35 - 0.34 - 1.05 - 1.57 3.50 - 3.28 - 3.70 - 4.01 - 0.55 7.50 - 0.33 - 9.35 - 10.34 - 11.38 13.45 - 13.95 - 14.76 - 14.97 - 12.50 15.65 - 17.20 - 17.20 - 17.40

15.75 15.85 --- -17.20 ---- 17.61--17.75 19.75 20.53 21.58 21.72 22.15 23.42 24.30 25.84 - - 25.99 - - - 27.62 - - 28.03 24.04 30.04 31.02 32.12 32.54 33.40 34.12 34. 10 ··· ·35 • +3-----35 • -28--39.87 40.04 41.23 41.52 41.45 41.63 42.00 92.02 - 43.45 - - - 49.44 45.43 47.49 45-67 43.78 49.20 50.14 D1.14 52.14 32.62 53.79 53.91 ~~ 54 · 71 35.6h 00.55 57.33 **⊃**3•34 34.08 50 **.** 34 31.12 52.15 198000 17 - 17 - 17 - 1800 - 1 56.56°

12.40

SF test 11

KOLL SUM OF SINE WAVES FUNCTION

		RMST VALUET OF LEROR					
	2.53	1.37	1.44	. • ≤	1.11	1.51	
	1.39	1.57	1-ee	1 • .5	1.54	1.41	
	1.45	1.45	1.46	1.56	1.57	1.00	
	1.51	1.49	1.53	1.54	1.50	1.52	
	1.44 .	1.45	1.47	1.44	1.46	1 • 4 1	
	1.45	17, 39	T1-33	1.46	1.54	1.41	
	1.39	1.57	1.42	1 - 42	1.41	1.49	
	1.45			-1. * / / /	` ~i~ 3∀```	1.33	
	1.57	1 • 40	1.35	1 • Dis	1.57	1.46	
	1.41	1.39 ···	1 • 5€·	1.56	1	1.55	
	1.35	1.35	1.36	. • 55	1.32	1.54	
**	1.35	1.54	1-34	1.50	1.36	1.54	
	1.36	1.36	1.38	1.57	1.5	1.17	
	1.35			1 : 54	1.35	1.54	
	1.33	1.54	1.38	1.12	1.35	1.54	

	TIME ON TARE	FET (SLOS)
. / 4	1.51	2.15
) 5	5 • 56	:. • 6 l

U = / 4	1.51	5.12	> • 1 ° ·	4 • 4	1 • 1
4.75	3 • 56	:. • 6 l	7 5	* • to 5	* • · · *
	11.11		11. «1	11.91	12.14
12.51	13.48	14.54	15.55	19.91	15.75
17:49	18:11	15.85	19.03	22.10	20.32
21.23	22.28	23.24	23 . 😘	24.15	25.14
25.42	26.03	725.02	15.00	27.12	17.14
28.17	29.19	30.12	1.03	51.30	37.55
	54 - 52	34.85	544	··· 55.12	35 • 4 / T
36.12	37.12	38.12	33.04	40.61	41.5
42.05	42.28	43.17	····44 • 18 ···	45.13	4 11
46.00	47.02	40.04	48.41	1 1 1 7 4	+ 5 € 62
44.52	49.799 -	50.54	51.43	52.55	* 2 . * *
50.02	54.18	55.02	Ja • 15	១ខ•៩៩	71. 4
		b U • U?****	· 01 • 25 ···	0.001	126 - 7

SF test 12

RULL SUM OFFISINE WAVESTFUNCTION

*	TRMSTVALU	E" DE ERKOR			
3.3.	1.15	2.73			1.0
2.02	1.65	1.75	$1 \bullet \cdot \circ \circ$	1.55	14
1.57	1.57	1.60	1 /	1.52	1 • 4 "
1.42	1.43	1 • 4 T	1 • 4 4	1.57	1.55
1.39	1.41	1.59	1 • 1to	1 • 4 ∂	1.00
1.55	11.55 · ·	1.35	1.71	1.34	1.54
1.23	1.36	1.33	1.05	1.30	1.31
1.28	1-26	1.30	-1.07	" 1.25" "	1.024
1.27	1.24	1.24	1.24	1.24	1.25
1.24	7125	1.•24	11.72	1.24	1.22
1.23	1.21	1.24	1.23	1.23	1.25
1.24	1:25	1 •25-···	1.24	1.024	1.22
1.22		1.22	1 • .'1	1.25	$1 \bullet 1 ?$
1.21		1.25	- 1.1	1.21	11 • 1111
1.21	1.22	1.23	$1 \cdot < 1$	1 • 2 ü	1.71

50.07

54022

TIME ON TARGET (SECS) 0.08 m · · · · 0.51 · · · · · 1.38 · · · · · 2.39 4 - 35 3.58 5•∂8 6.51 7.75 9.75 5.39 ~•ਰ1 15.85 14.31 15.35 17.0 1 • 🖭 19.00 ~20.64~~~ 21.39 ~ 22.40 20.25 ~ 35.43 24.17 20.13 25.80 26.80 27.02 24.77 22.54 157.54 33.52 ~~dd.06~~~~~dd.65~~ 27.62 -31.50 3 .55 34.60 35.03 **ა**ս•63 27.75 39.00 ~4 4 • t) ~·~ 44.45 ----- 4 û • 48 ---41.43 45.42 46.42 44.51 47.4% 44.47 49.72 ---50.61--- --51.52----520 57 55.44 55.27 55.99 54.27 56 • 14 .01 51.60

61.71

L6. "1

1 ا د د د

37.2d

りきょりし

50.01

13.00

- 51.03 - - 51.32 -

ნხ∙*∂***ხ** ნხ∙30

SF test 13

RULL SUM OF SINE WAVES FUNCTION ()

	RMS VALUE	OF ERRO	Š.		
5.1	5.82	2.43		. •	. 41
	2.10	77.10	1 • 2	71 • 11 · ·	1 - 1 -
1.74	1.75	1.5.	1.	i . t. +	1
1.55	1.53	1.54	1 • 2	1.52	1 • 55
1.57	1.45	1.65	1.	1.02	
1.55	1.54	1.50	1.51	1.5%	1.5
1.47	1.47	1.46	1 • •	ì • •	1.44
			···· 1 • 4 ·	44	1.495
1.44	1.42	1 - 4 4	$1 \cdot \cdot 1$	1.41	1.4
1.41	· · · 1 • 4 U	1.40	1	1.41	1.5
1.57	1.39	1.50	. •	1.37	1 • 4.
1.54	1.57	1.35	1 - 54	1.5%	1 • 1 2 1
1.45	1.36	1.35	1 • 1	1.34	1 • 1 1
1.54		1-51	···· 1 • 5 5	1.5	1.1
1.35	1.53	1.33	1 . 15	1.54	. •

Meyd OF RUSE 1.45

	TIME UN TAI	POLT (SECS)		
C • U 4	0.88	್೮⊛೪೮	1.1		• • "
4.25	5.68	₽ • Q ;;	i • 3	• (• .
10.35	··		15.1	1 4 - 1-4	1.
10.25	17.29	17.91	13.0		1 1 🕶 😺
1 1.81	20.21	20.92	J1 . 3	1. • 2. 4	J 17
273	24.78	23.81		1.11	. (• "
20.57	29.55	30.28	* A • * * * * * * * * * * * * * * * * *	11.32	1.14
33.52	34.54	30.22			57.
- 38.00	38% 58		40 • 11 i	41.17	47. • 1 / 7
ويوري	43.59	44.21	44 🗸 : 👌	4	45.01
41.62	48.57	99.19	49.45	7 J • 32	51. c
52.01	53.92	54.94	55. 11	51.49	30
51.52	58.37	59.39	50.0	5 1 • 5 tz	11 1 · 4
53•45	64.35	64.77	134 . 18	, ~ • ⁽) ii	3000
67.0t		····5	್∵ೀರೆ•1ರ್ ⊤	57.17	20.01 °

SF Lest 14

DUM OF SINE WAVES FUNCTION

	0.00	JETOFTERROI	₹ 5.47×	1.0	11
1.55	1:18	1.17	1.43	1.11	1.23
1.07	4	1.14	1.10	1.11	1.17
1.07	1.09	1.09	1.86	1.00	1.14
1.03	1.10	1.07	1.1x	-1:03	1.10
1 • 0 ₫	1.05	1.07	1.11	1.10	1.0
1.09	1.11	1.15 1.10		1.07	11:
1.10 1.11	1.10	1.12	1.15	1.11 1.11	1.11
1.12	1.15	1.11	1.11	1.12	1.1.

0.45	1.98	RGET (SECS ~ 2.65%	2.07	5 • 114.	1 • 1
4 4	p. 59	7.05	7.		15.11
tu•H7	-t-t-++t	-12.00		1 • 0 **	20.11
10.55	10.55	17.60	23.17	24.24	35 • 27
21.12		20.24°°°	25. 3	54.09	53 • * *
20.23	27.28 32.77	33.37	34.04	37.000	င်းကုန⊌ "ု
51.92	38.12	39.10	40.04	91.1 →	41.41
37.27	4.5.0.74 	45.07		45.28	45.20 91.75
41.24	48.27	49.27		30.72	45.77
52.78°	53.25	53.57		ლო•11 ნი•მი	• •
داورو	37.34	ည်စ်စ⊈င်	50 · 14 01 · 11	52.11	. 5 s "t"
- 50.14	50.32	60.75	07.07	60. JU	a 4 •
64.32	55.87 71.55			75.38	74.41

<u>Vita</u>

Nathan H. Krys was born November 17, 1947 in Munich, West Germany. His family immigrated to the United States on January 6, 1950 and settled in New York City. He graduated from Brooklyn Technical High School in 1965, and later attended the Academy of Aeronautics in Queens, New York. There he received an Associate Degree in Electronic Technology in January of 1968. After a short employment with Western Electric, he enlisted in the Air Force in November of 1968 and was later assigned to Forbes AFB, Kansas. He met and later married the former Leslie J. O'Reilly, of Topeka, Kansas, on November 28, 1971. Selected for the Airman Education and Commissioning Program, he attended the University of Wyoming where he received a Bachelor of Science degree in Electrical Engineering in June of 1974. After completion of Officer Training School, he received his commission in September of 1974. He later completed navigator training school at Mather AFB, California and received his wings in May of 1975. During subsequent flying assignments he flew C-141's at McGuire AFB, WC-130's at Anderson AFB, and HC-130's at McClellan AFB. In June of 1981 he entered the School of Engineering, Air Force Institute of Technology.

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19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Longitudinal simulation
Man-in-the-loop simulation
Flying qualities
Ground-based simulator

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

An analog computer simulation was used to model the roll dynamics of the generic aircraft which had been evaluated on the variable stability NT-33A aircraft. Sum of sine waves and random step functions were used as the two different command signals. The purpose of this study was to determine what effect the nature of the command signal had on the pilot rating of the

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task simulation.

The experiments consisted of fourteen different tests for each command signal. Five pilots, with varied flying experience, were instructed to follow the command signal in a pursuit flying task. The system time delay was varied from 0.1 to 0.8 seconds. The highest frequency component of the input signal was 2.54 radians/second. The subjects used a control stick while looking at an oscilloscope displaying the command signal and the subject's response. RMS error, time on target, and the Cooper-Harper rating scale were used as performance measures.

The experiments showed that the subjects considered the sum of sine waves task closer to an actual flyingtask. In addition, as the time delay was decreased, the subjects preferred K/s-

like dynamics.

END

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